

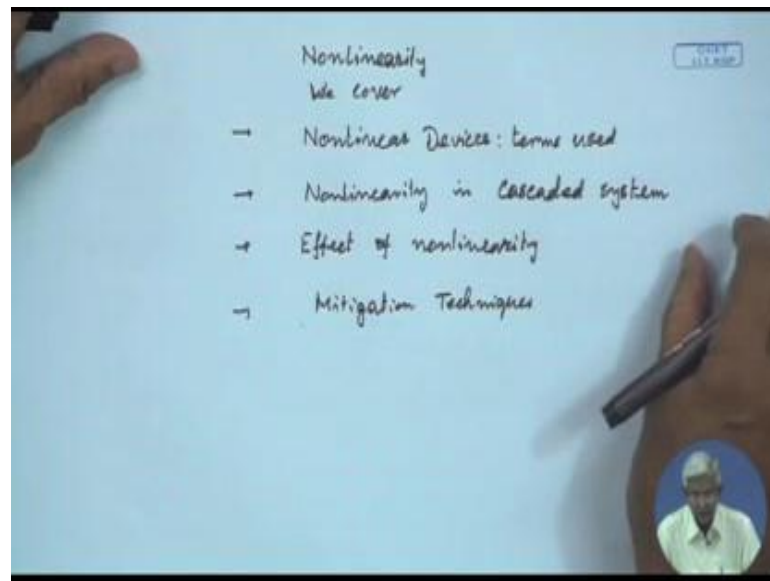
Satellite Communication Systems
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Lecture – 31
Nonlinearity I

Welcome. We have discussed about the orbit space segment, the link budget, the propagation effect, ground segment and then we talked about a network system and that multiple access, different types of multiple accesses. Now, we will try to talk about certain issues we face in this type of communication which is wireless and which is a long delay and which has a probability of error is quite high. Now, let us see the first part that is it is a long distance repeater; the satellites are quite high in the sky. So, the power that is required from satellite to ground to receive properly with good sensitivity, we need to transmit large power from satellite and similarly from the ground to satellite.

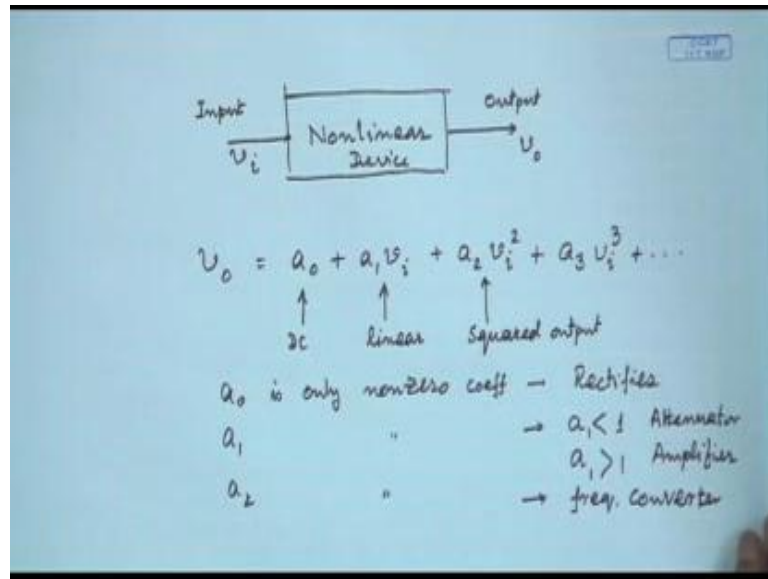
So, once we try to transmit larger power we have to look at the power amplifier and a take maximum power out of it. Now, any device when we try to take maximum out of it, it goes into non-linear. So, as we know that any amplifier at a very low input level there is no yes even if you do not give an input there be certain thermal noise. So, there is non-linearity at the very low level. Similarly, when you go to higher level there will be again certain distortion that is limiting by the power supply to that amplifier. Now, it is not only amplifier there are many devices which generates and proves non-linearity. In fact, almost all practical devices active devices they show non-linearity and non-linear characteristics.

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So, we will see how this non-linearity can affect our communication system. So, our topic is non-linear and what we cover is and this is topic is what we will cover the non-linear devices certain terms, we use terms used those terms define what type of non-linearity it is and then we will talk about non-linearity not only single device when the cascade non-linearity in cascaded system when they put one after another and of course, we will see the effect of non-linearity and very briefly we touch upon the mitigation technique is the general form and there will be mix of this while we discussed. So, let us take a non-linear device and let us say the device is non-linear.

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It has an input, let us say we gave a voltage input V_i and it goes to the output and it gives a voltage V_o . Now, in general, a generalized form of non-linear expression that V_o output can be modeled as a Taylor series. So, it can be written this way simply a_0 is a coefficient, then $a_1 V_i$, then $a_2 V_i^2$, then $a_3 V_i^3$, like that we can continue and depending on the coefficient values that non-linearity can be generated. So, this is a very, very general term.

So, out of that we can define that this is a DC term if we give a DC input and this is a linear term and this is a linear output. This could be this is a squared output like that. Now, if we say that all other coefficients are 0 and only a_0 is a non-zero coefficient, then the device is a rectifier. Similarly, if a_1 is a non-zero coefficient, then the device, if a_1 is less than 1, then output will be less than the input. So, it is an attenuator and if a_1 is greater than 1, then it is an amplifier. This is how it is expressed.

Similarly, if a_2 is the only non-zero coefficient, it is generating higher and higher frequency. It is a frequency converter. So, that is how, based on the Taylor series model, we can define, based on the coefficient, what type of system it is, but in practice these things occur together. So, several of the coefficients may be non-zero in practice, but this is an ideal modeling situation.

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$$v_i = V \cos \omega_0 t$$

$$v_o = a_0 + a_1 V \cos \omega_0 t + a_2 (V \cos \omega_0 t)^2 + a_3 \dots$$

$$= \left(a_0 + \frac{a_2 V^2}{2} \right) + \left(a_1 V + \frac{3}{4} a_3 V^3 \right) \cos \omega_0 t$$

$$+ \frac{a_2 V^2}{2} \cos 2\omega_0 t + \frac{a_3 V^3}{4} \cos 3\omega_0 t$$

$$G = \frac{v_o}{v_i} = \frac{a_1 V + \frac{3}{4} a_3 V^3}{V} = a_1 + \frac{3}{4} a_3 V^2$$

gain compression

Let us try to give input let us say V_i is $V \cos \omega_0 t$ you want frequency and a voltage. So, this is input now how V_o will be written V_o will have DC component that is a 0 then will have the linear component $\omega_0 t$ then will have a square component then it will have a cube component like that. Now, if we take this cosine square cosine cube this term and use certain trigonometric identity and separate out that single frequency component and DC component and higher other frequency component.

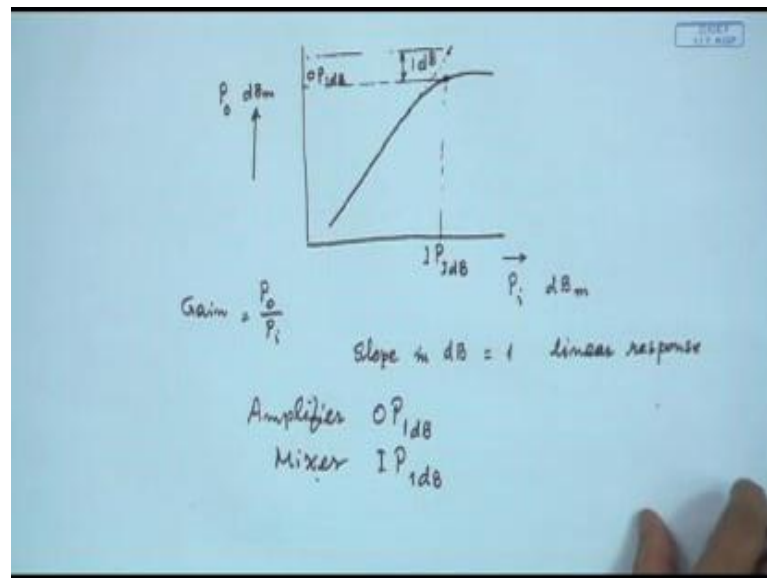
We can group them like this that $a_0 + \frac{a_2 V^2}{2}$ that will be our DC component then $a_1 V + \frac{3}{4} a_3 V^3$ that is a fundamental component, but is with this coefficient cube then $\frac{a_2 V^2}{2} \cos 2\omega_0 t$ that is double frequency component it will have step of coefficient then $\frac{a_3 V^3}{4} \cos 3\omega_0 t$ another higher order component of frequency with a different coefficient.

So, in these let us assume that this is amplifier. So, we will take the fundamental component and what is amplifier gain the gain is V_o by V_i . So, this coefficient that is $a_1 + \frac{3}{4} a_3 V^2$ now here a 1 and a 3 that generally practically this a 3 is many times opposite sign of a 1. So, in that case it will grow linearly, but after sometime it will

deviate from linearity it will look like briefly it will go straight and then deviate from linearity this is V and this is V out V in I can call, so that capital b as we increase.

So, this is actually what is happening gain compression, I can call it a gain also this is gain I can plot gain if I plot then gain will goes linearly and then it will try to deviate from linearity. So, it is called gain compression. So, this is one of the major effects of non-linearity that gain will go linearly and after sometime it will saturate.

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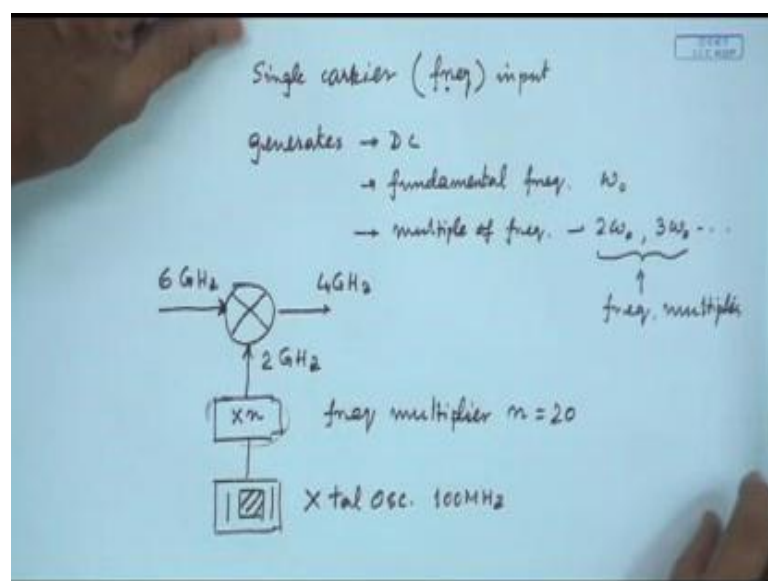
Let us see what happens if we try to draw this characteristics in power what happens in power. So, let us call this P_i in dB, dB m let us call and then this is P_o out and dB m. Now, once is plotted in terms of power it is linear slope and then it deviates from the linearity. So, when it deviates from the linearity this could have been the linear situation and when it is 1 dB down from here to here, let us call this is 1 dB down this point is defined by the device suppliers or manufactures that at this point we start getting the non-linearity or it is getting into saturation.

So, this point from the input side it is defined as input power of 1 dB compression point. Similarly, this is called output power 1 dB compression point 1 dB getting compressed. Therefore, it is away from linearity it is compressed and it is going away in the non-

linearity direction, now this gain of this amplifier of course, power gain is a ratio of p out by p in and this slope when we do it in dB it is 1 that is, it is a linear response and when the p out start from deviating the linear response we get into saturation and when it is away from the 1 dB of linearity is called 1 dB compression. Now, these is a define in terms of either input for 1 dB compression point or output 1 dB compression point, if it is referred to input is called input 1 dB compression point $i p$ 1 dB or output 1 dB compression point which is $o p$ 1 dB have it in here.

Generally, that in practice the higher 1 of this is specified in case of amplifier in case of amplifier output 1 dB compression point is higher than input on compression because the gain is multiplied to that and let us say a lossy device called mixer which is a non-linear where the input 1 dB compression point is higher. So, in case of mixer input 1 dB compression point is referred. So, when simply 1 dB compression point it says then we have to check whether it is referred to input or it is referred to output, but generally we will be talking about amplifier of course, will sometime come to mixer will always refer it we can say 1 dB compression point as $o p$ 1 dB or $i p$ 1 dB compression point. Now, let us see that what happens with a single carrier input to non-linear device that is single carrier means single frequency.

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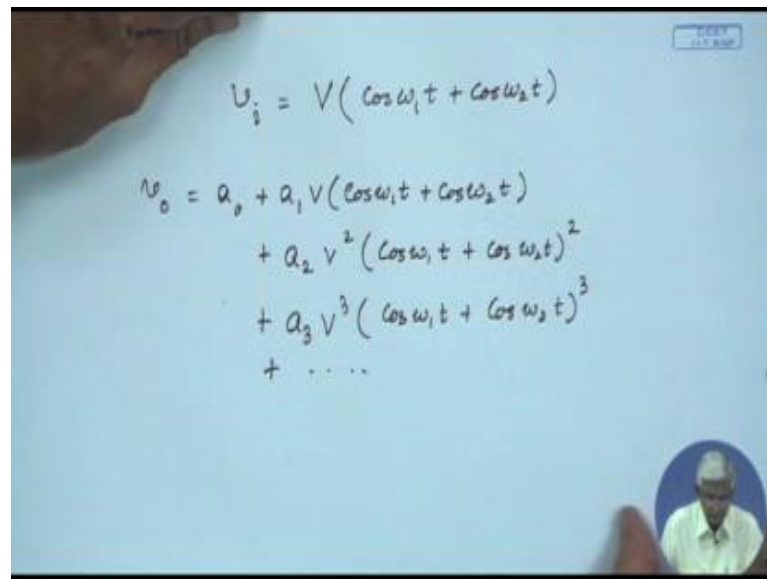


It generates, we have seen that it generates a DC component it generates a fundamental frequency which is ω_0 , it generates a multiple of frequency which is $2\omega_0$ or $3\omega_0$ like that. So, these characteristics of multiple frequency multiple of the fundamental frequency is used in frequency multiplier like this we have at satellite we get input in 6 gigahertz, let us say uplink which is gone to the satellite and after $1/n$ it has come to a down converter which is nothing, but a mixer and then a local oscillator and that local oscillator contains a crystal oscillator which is generally this is crystal oscillator, which is generally of the order of 100 megahertz and to get output of 4 gigahertz which should be the downlink after this down conversion I need to give 2 gigahertz here.

So, this is 100 megahertz has to be multiplied and brought to 2 gigahertz. So, this frequency multiplier is n equal to in this case 20. So, you get a 2 gigahertz. So, this is 1 of the place where this non-linearity is used it using mixer also that for single frequency when it is going up through a non-linear device, we get this multiple of the input frequency which is in times of input frequency and there may be when here it is simplified and shown it in 1 stage it may not be taken as 20, it may be multiple stages and in between amplifier may come, but this is the concept of the frequency multiplier.

Now, let us go in to the amplifier. In amplifier, generally in satellite communication we have seen last period multiple access multiple carriers are coming. So, let us take a simplified case of 2 carriers input.

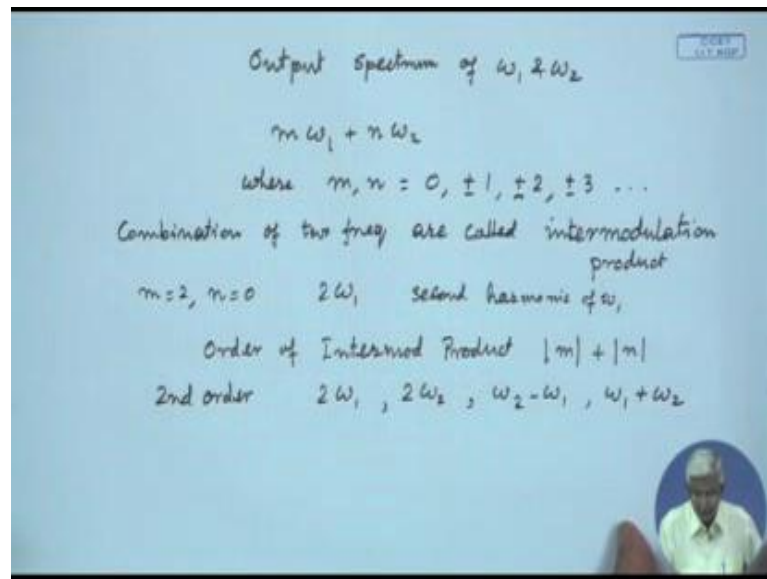
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$$U_i = V(\cos \omega_1 t + \cos \omega_2 t)$$
$$V_o = a_0 + a_1 V(\cos \omega_1 t + \cos \omega_2 t) + a_2 V^2 (\cos \omega_1 t + \cos \omega_2 t)^2 + a_3 V^3 (\cos \omega_1 t + \cos \omega_2 t)^3 + \dots$$

So, 2 carriers input is let us say V and that case and both carriers have same amplitude. So, $V \cos \omega_1 t$ and $\cos \omega_2 t$ both have this same amplitude V , this is for simplified calculation, in a actual case it may be most of the time it will be $V_1 \cos \omega_1 t$ or an $V_2 \cos \omega_2 t$ each amplitude may be different depending on the input what is being supplied by different carriers.

So, the V output will be in the case by Taylor's series. If you go a $0 + 1 V \cos \omega_1 t + \cos \omega_2 t$ then a $2 V^2 \cos \omega_1 t + \cos \omega_2 t$ whole square then a $3 V^3 \cos \omega_1 t + \cos \omega_2 t$ cube like that it will continue. Now, if you simplify this square terms and cube terms and then use certain trigonometric identity then you will find that in addition to the fundamental components ω_1 and ω_2 you are getting the higher order components like $2\omega_1$, $3\omega_1$ like $2\omega_2$, $3\omega_2$ and also you will get $\omega_1 + \omega_2$ $\omega_2 - \omega_1$ or $2\omega_1$. So, like that there will be lot other frequencies which are generated other than fundamentals all those frequencies are called inter modulation product the let us let us try to do it mathematically.

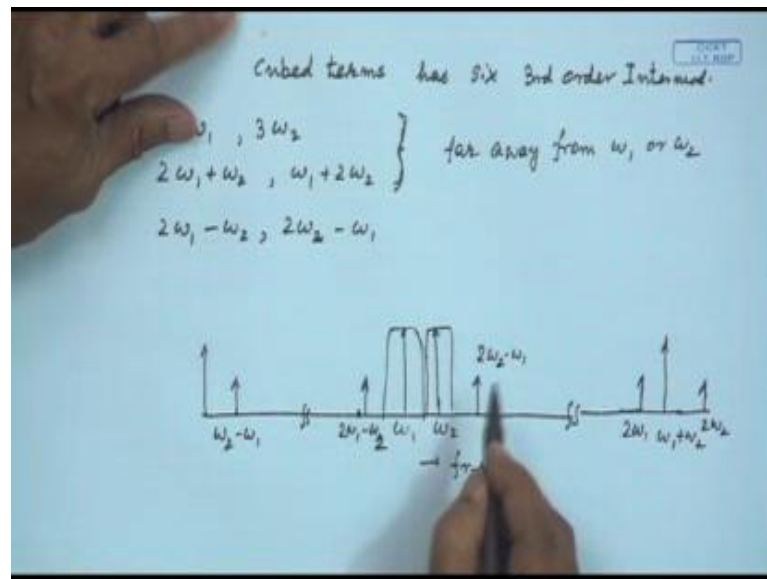
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Let me show you that is that output spectrum of ω_1 and ω_2 will in the form of $m\omega_1 + n\omega_2$ where m and n could be 0 plus minus 1 plus minus 2 plus minus 3 like that this combination of 2 frequency are called either you can call in this case we call them inter modulation. This term I have used earlier that we are not defined it is inter modulation product. So, let us say m is equal to 2 and n is equal to 0 then what will you get $2\omega_1$ which is second harmonic of ω_1 . So, we can say there is a order of m and n .

So, the order is defined order of inter mod product we can define as mod of m and plus mod of n . So, we can see the second order components are $2\omega_1, 2\omega_2, \omega_2 - \omega_1$ then $\omega_1 + \omega_2$ like that, any terms now when this ω_1 and ω_2 when they are closely spaced then the multiplication or addition subtraction terms would be far away from the fundamental frequency ω_1 and ω_2 . Now, similarly we can see in the cubed term has 6 third orders inter mod.

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It is $3\omega_1, 3\omega_2, 2\omega_1 + \omega_2, \omega_1 + 2\omega_2, 2\omega_1 - \omega_2, 2\omega_2 - \omega_1$. Now, these 4 first $3\omega_1, 3\omega_2, 2\omega_1 + \omega_2, \omega_1 + 2\omega_2$ class ω_1, ω_2 plus $2\omega_1 + \omega_2, \omega_1 + 2\omega_2$, you can look at from this you can make out they will be far away from the fundamental or ω_1, ω_2 , but these terms $2\omega_1 - \omega_2$ and $2\omega_2 - \omega_1$ if ω_1 and ω_2 are closer the difference also becomes smaller. So, there will be coming very near and they may fall within the transformer and with modulation, if it is pure carrier then they will be away by $\omega_1 - \omega_2$ but if they have modulation then some of these frequencies will fall within the filter bandwidth of a ω_1 and ω_2 .

Let us try to draw a simplified diagram, let us say this is the frequency and here somewhere I have close them together, this is ω_1 and ω_2 . So, $\omega_2 - \omega_1$ will be here very near to DC, but $2\omega_1 - \omega_2$ will be coming very near similarly $2\omega_2 - \omega_1$ then you will find far away that $\omega_1 + \omega_2$ and $2\omega_1 + \omega_2$ and $\omega_1 + 2\omega_2$ these terms. So, this first 4 terms will be far away, whereas this term $2\omega_1 - \omega_2, 2\omega_2 - \omega_1$ which are third product. We fall very near and if there is a modulation here, the bandwidth will be more and modulation here the bandwidth is more than the multiplication of this frequency to

this frequency will fall within the band. Now, since the time it is short will continue with the discussion in the next period.

Thank you for the time being.