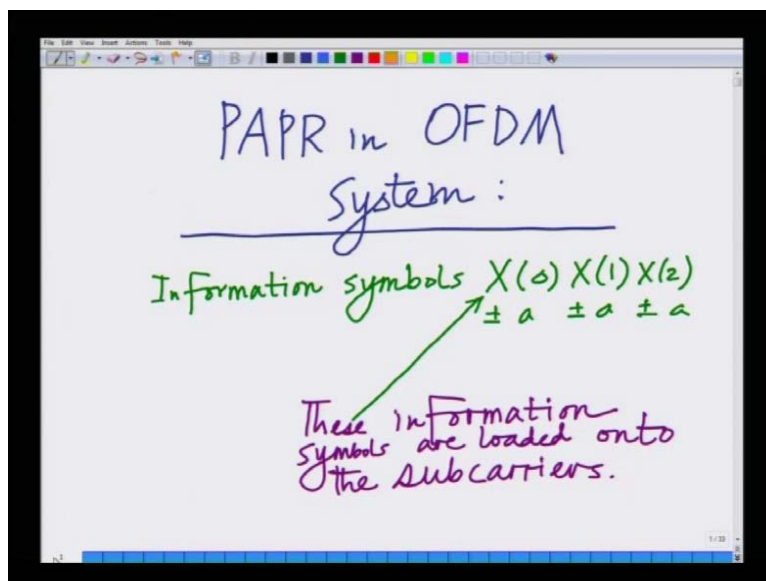


Advanced 3G and 4G wireless communication
Prof. Aditya K. Jagannatham
Department of Electrical Engineering
Indian Institute of Technology, Kanpur

Lecture - 35
SC-FDMA (Contd.) and Introduction of Wireless Propagation

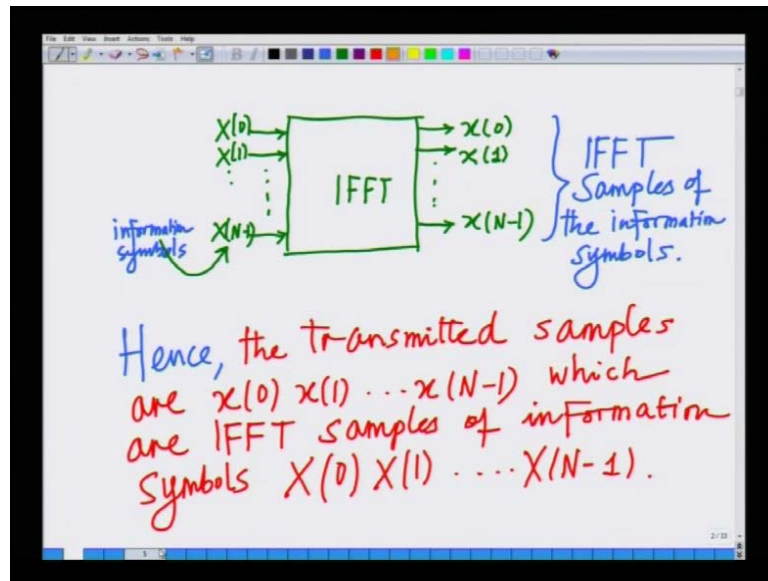
Hello, welcome to another lecture in the course on 3 G, 4 G wireless communication systems.

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In the last lecture we had looked at the PAPR problem in OFDM systems; that is the peak to amplitude power ratio problem in OFDM system what we said was the information symbols a capital X_0 , X_1 , X_2 so on are correspond to let us say BPSK modulated symbols plus or minus a plus or minus a plus or minus a .

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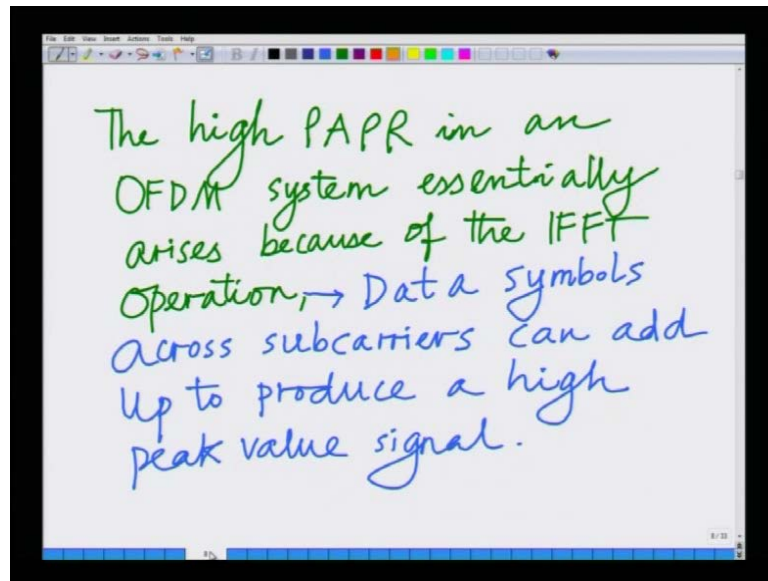
Before we load these information symbols on to the subcarriers and perform an FFT. So, the actual transmitted samples $x(0) x(1) \dots x(N-1)$ correspond to the IFFT of these information symbols.

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The slide contains handwritten text in purple and blue ink. It starts with "Hence, Peak to Average power ratio (PAPR)" followed by the equation
$$= \frac{a^2}{a^2/N} = N$$
 where N is double-underlined. A blue arrow points from the N in the equation to the text below: "Hence, PAPR in an OFDM system can be significantly higher."

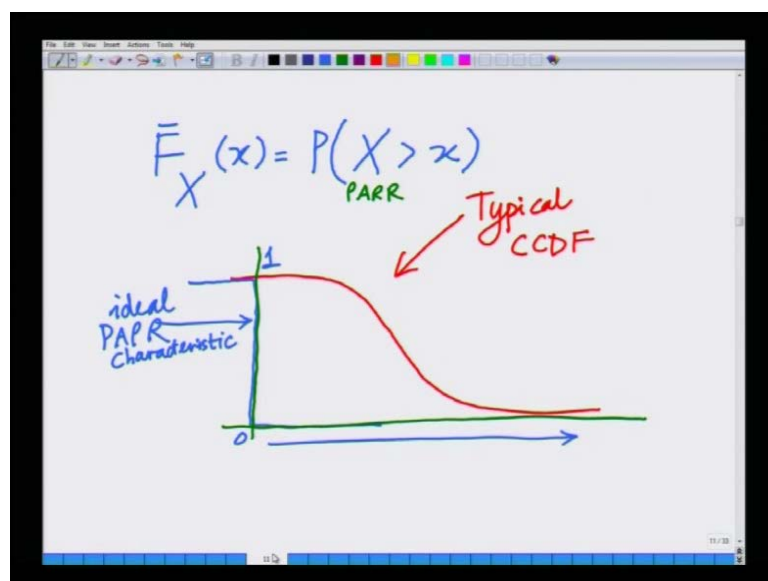
Hence what happens, what essentially happens is when you look at this we have a peak to average power ratio that increases with the number of subcarriers, and that is the as the number of subcarriers increases the peak to average power ratio increases.

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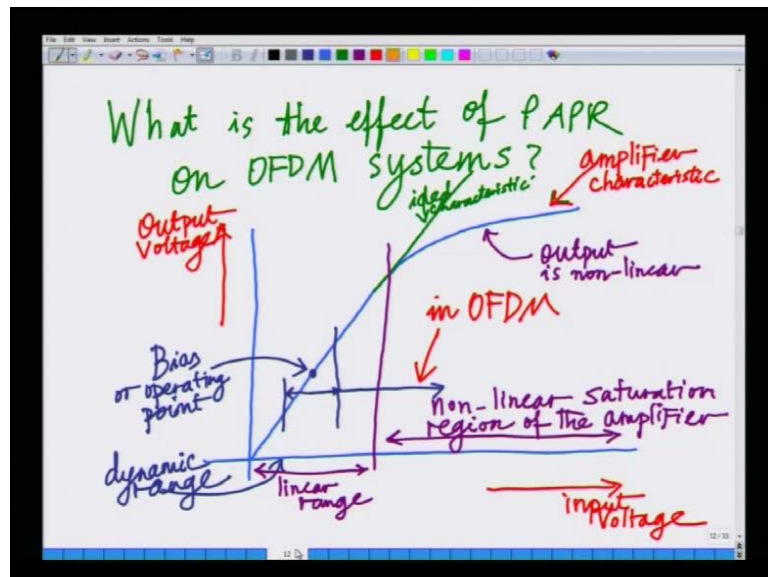
And why is the peak to average power ratio increasing because we said the high peak power raises from the IFFT that is being performed in OFDM, which can occasionally result in a high peak value signal, so because these signals are being combined in the IFFT of the symbols are being combined in the IFFT. They occasionally produced a high peak value signal, which is significantly deviating from the other ways the mean value of the signal. Hence, the peak deviation is much higher over the mean that results in a high ratio of peak to average a high peak to average power ratio in an OFDM system.

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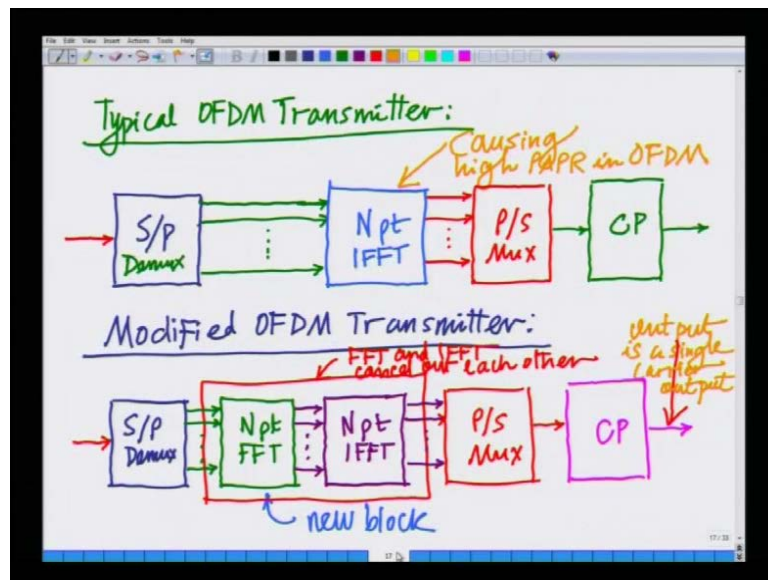
And we also saw that the peak to average power ratio can be measured by this CCDF that is the probability, that the peak to average power ratio is greater than a certain threshold. We also looked at examples for different of how the PAPR CCDF curve looks for different numbers of subcarriers.

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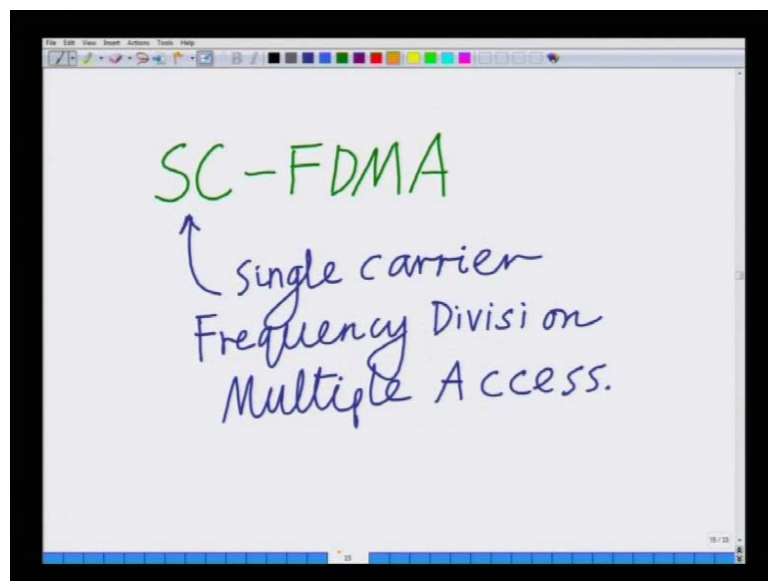
Now, what is the ill effect of PAPR we said the PAPR causes distortion in an OFDM system. Since, every OFDM amplifier has a certain linear range which is biased about the mean. Now, if the deviation about the mean is significantly large that is the peak value occasionally significantly deviates over the mean, then this amplifier crosses over into the saturation or the non-linear range, but its amplification is not linear anywhere. Now, when the amplification is not linear that results in distortion and that results in inter carrier interference; that results in a loss of orthogonality amongst the different OFDM subcarriers, which results as we saw in the case of carrier frequency offset results it is decrease in the net SNR.

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And if we look at a solution, how can we expect to solve this PAPR?

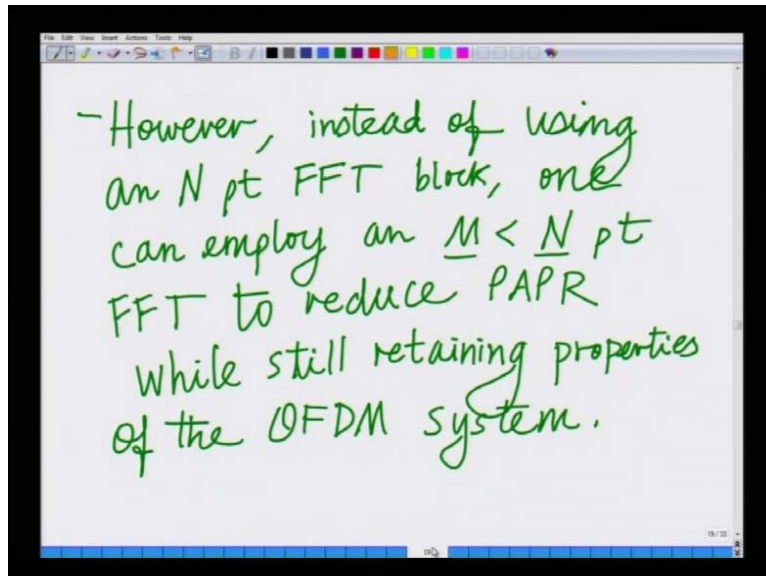
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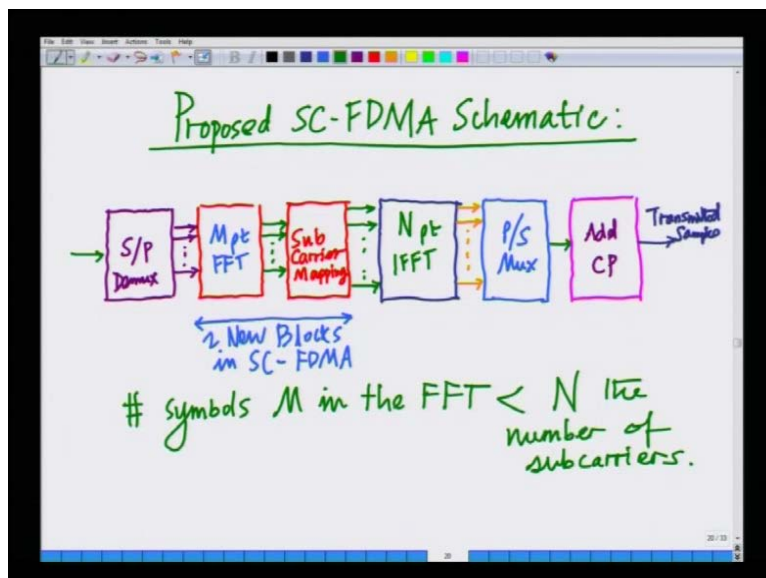
The solution we said is to use single carrier FDMA and that is as follows that is if you observe the OFDM transmitter schematic, if I introduce an N point FFT. Before the N point IFFT the FFT and IFFT cancel and this reduces to a single carrier system, which PAPR is very low. It is almost close to 0 dB that is what we said. Hence, what I want to do is I want to introduce an FFT block before this IFFT. However, I do not want to do an N point FFT

because that will go back to single carrier system and intermediate inter symbol interference. I want to do something in between this single carrier system and essentially OFDM.

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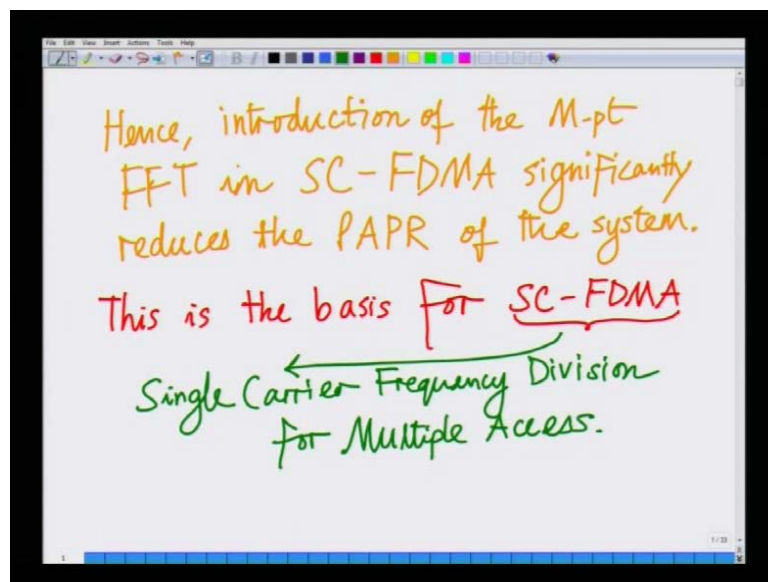
So, I am going to choose an FFT size M , which is much smaller than N . Then map these M symbols on to N subcarriers. Hence, the net schematic looks as follows, I take this M point FFTM symbols perform their FFT map them to the subcarriers. And after I map them to the subcarriers, I can now perform an N point IFFT here. I will perform an N point IFFT here. I will perform an N point IFFT and the rest is exactly like we had earlier, which is out of this N

point IFFT will serialize it. That is I will convert from parallel to serial that is a multiplexing operation.

Once I multiplex these signals, I will then add the cyclic prefix and transmit these I will add the cyclic prefix and then transmit these samples, okay? So, these are the transmitted samples and if you look at this these are the two new blocks that we are talking about. If you are looking at this the rest all are conventional OFDM blocks these are the two new blocks in SCFDMA that is these are the the M point FFT and the subcarrier mapping. These are the two new blocks that we are adding in SCFDMA. We also said that the number of symbols in the M point FFT number of symbols, min the FFT is much smaller than N, which is the number of subcarriers.

So, the number of symbols M in the FFT is much smaller than because if N equal M, we are going back to a single carrier system and we do not want to do that. So, M which is the number of symbols in the FFT is less than M and this is M point FFT is introduced for the purpose of reducing the PAPR in the OFDM system. After the d f and this step reduces.

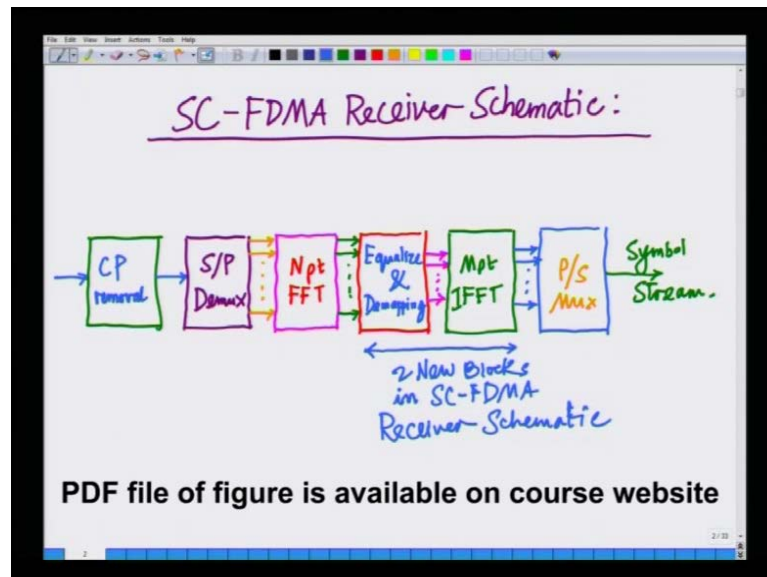
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Hence, hence introduction of this M point FFT significantly reduces the PAPR of the M point FFT in SCFDMA significantly reduces the PAPR, significantly reduces the PAPR of the system. And this is essentially transfer this is essentially the techno this is essentially the SCFDMA scheme, which is single carrier FDMA. Hence, this is the basis SCFDMA where SCFDMA as we have talked about stands for single carrier frequency division multiple. This

stands for single carrier frequency division for multiple this transfer single carrier frequency division for multiple access, end of this actually reduces the PAPR that is peak your amplitude power ratio of the OFDM system. How does the SCFDMA receiver schematic look? We have looked at the SCFDMA transmitter schematic.

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So, now what we want to do is we want to look at the SCFDMA receiver schematics. So, I want to look at the SCFDMA receiver schematic and that SCFDMA receiver schematic looks as follows. What we want to do is we want to essentially add the receiver similar to FDM, once I get the symbols. What I am going to do is I am going to remove the cyclic prefix and followed by I am going to do a serial to parallel de-mux operation that is serial to parallel the multiple; that is I am going to block this. I am going to block into the original FFT size, which is which is original IFFT size, which is N subcarriers.

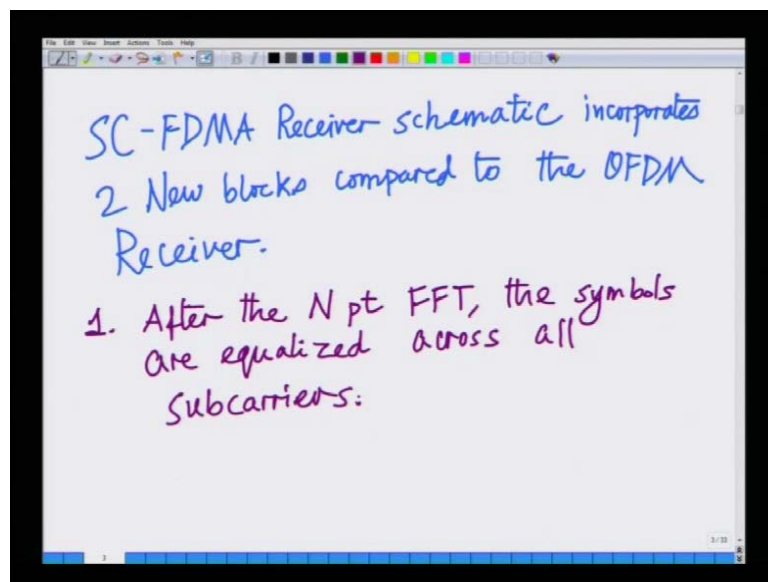
So, I am going to have similar to what I had earlier, I am going to have hence subcarriers over which I perform N point FFT. So, here I am going to perform N point FFT. Now, after I perform the N point FFT, what I am going to, have to do is I am going to have to equalize these symbols. Previously remember we had a detection, but before detection now we have to equalize because this is signal carrier system. So, we have to equalize and then we have to do a equalize across each subcarrier. Then we have to do a de-mapping.

So, this is equalize and now do a de-mapping de-mapping back to the M symbols. Now, we have to do a subcarrier de-mapping and once we de-map we de-map back into the M, we de-

map into M symbols and now we perform the M point, we perform the M point FFT operation after we perform I am sorry we perform the M point IFFT operation and after we perform the M point IFFT operation, I can serialize this. So, I convert from parallel to serial, which is essentially I multiplex this into the data stream or essentially or essentially the symbol stream.

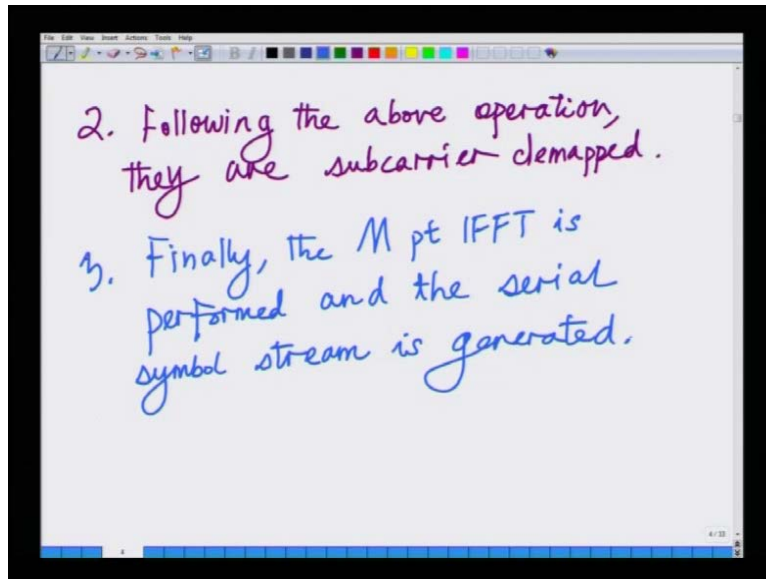
So, this is how the SCFDMA receiver schematic looks. That is cyclic prefix removal serial to parallel demark multiplexing this is same as in OFD M N point FFT. Now I have to equalize and de-map remember into the M symbols. So, I equalize de map perform the M point IFFT multiplex it and I get back my symbol stream. So, if we look at this these are again the two new blocks that we introduce in the two new blocks, in the SCFDMA receiver schematic. These are the two new blocks that we introduce in the SCFDMA receiver schematic and then I get back my symbol, my symbol stream. So, it incorporates two new blocks essentially.

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So, this SCFDMA are so s c f d m a receiver schematic. Incorporates two new blocks compared to the OFDM compare to the OFDM after the after the N point FFT the symbols are equalized. So, first N point FFT, the symbols are equalized across all they are equalized across all subcarriers. Then they are subcarrier de-mapped following the above operation.

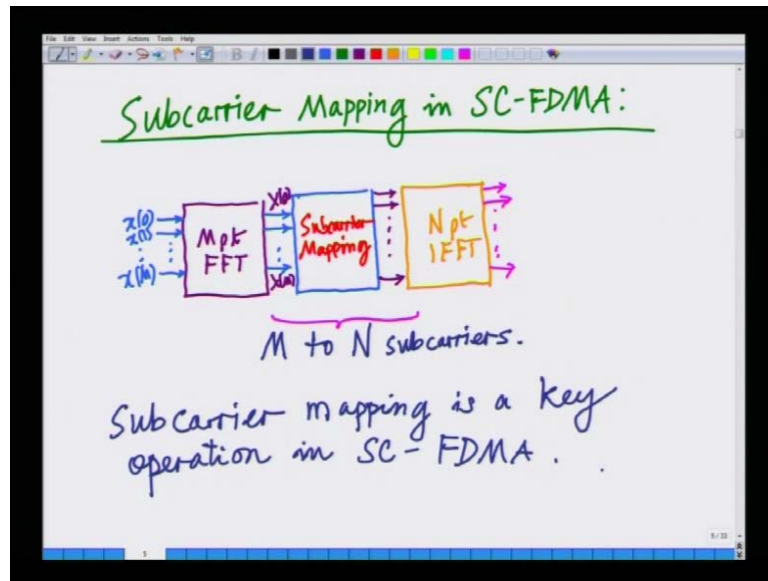
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They are subcarrier de-mapped, this is essentially inverse of the mapping operation that was done at the transmitter. Remember earlier the OFDM transmitter schematic, we had a subcarrier mapping operation. Now, we have a de-mapping operation at the receiver. Finally, the IFFT is carried out and the serial symbol stream is generated. Finally, the M point IFFT is performed and the serial symbol stream is generated.

So, you feel like that is first after the N point IFFT these symbols are equalized across subcarriers. After equalization that are de-mapped to the M de-map from N to M subcarriers after the de-mapping they are again, you perform the M point. IFFT to invert to reverse the M point FFT operation the receiver and then you then you give back the serial symbol stream at and this serial stream is again generated all right? So, that is how the serial symbol stream is generated and that is one last aspect that we need to talk about in the in this SCFDMA system, which is essentially the subcarrier mapping operation. How are these carriers mapped at SCFDMA transmitted?

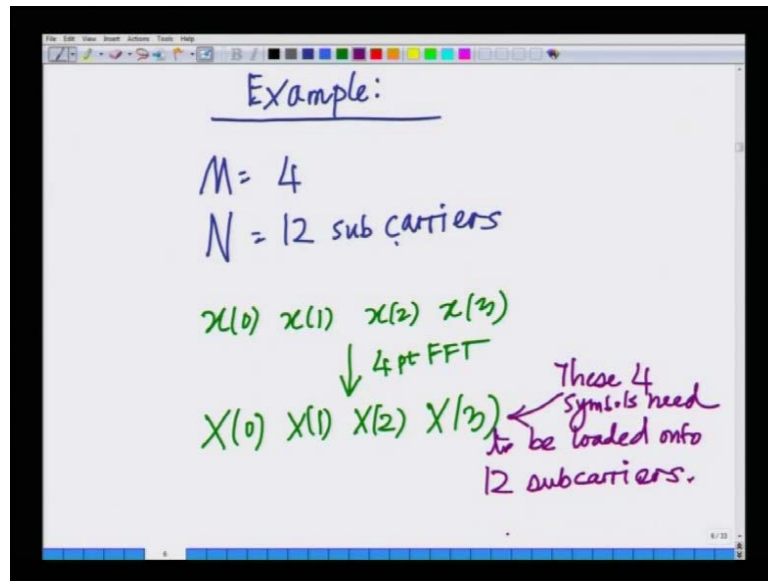
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So, we want to talk about the subcarrier mapping, how are these subcarriers mapped in an SCFDMA? If I look at a subcarrier mapping operation, then what I am I what, I am looking at essentially is let me go back again to my SCFDMA transmitter schematic, I have an incoming stream of I have M symbols X_0, X_1 so on up to X_{M-1} , which I am mapping to capital M . So, I am performing here, I am performing the M point FFT and the M point FFT is mean which I am now mapping to the capital N subcarriers. So, here I will have X_0 up to X_M , which I am mapping to N subcarriers.

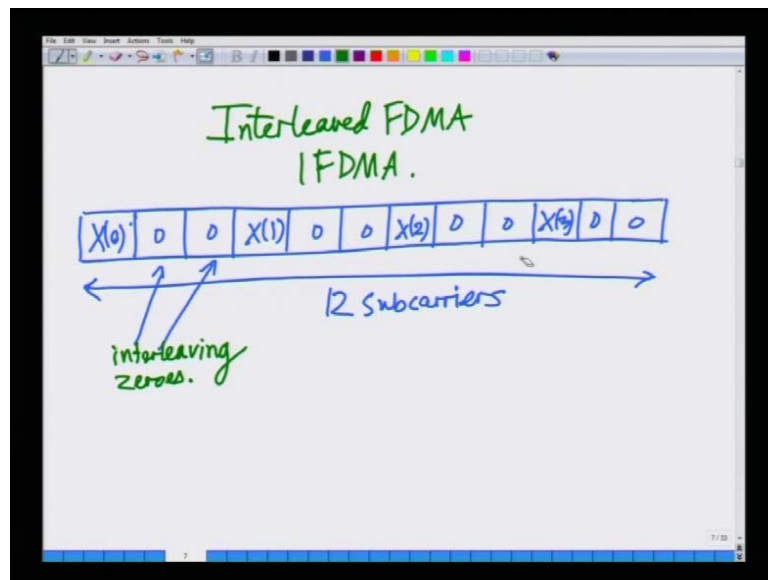
So, here I am performing subcarrier, here I am performing subcarrier mapping and I am subsequently performing the N point IFFT. I am performing the N point IFFT. So, the essential idea is how are we mapping from these capital M capital M to N subcarriers. M to N , how are we mapping these subcarriers, this we can illustrate by so the subcarrier mapping is a key operation. So, this subcarrier mapping is actually a key operation in SCFDMA. Let us illustrate this for a certain example.

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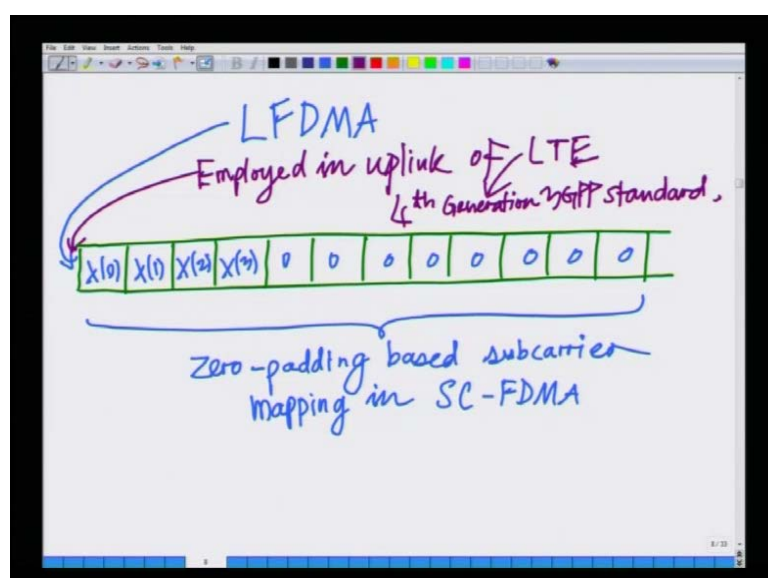
So, as a simple example to illustrate subcarrier mapping what I am going to do is, I am going to consider. For example, as an example scenario consider M equals 4, that is the size of the M point FFT that is I am going to consider M equals 4 and N equals 12, N equals 12 subcarriers, which means I have $X(0)$ 4 information symbols, $X(0)$, $X(1)$, $X(2)$, $X(3)$. I perform the M point FFT, which is essentially the 4 point FFT, these are $X(0)$, $X(1)$, $X(2)$, $X(3)$. So, these are the symbols that are now to be loaded on to the N 12 subcarriers. So, these 4 symbols need to be loaded on to 12, this 4 symbols need to be loaded on to the 12 subcarriers and this can be done as follows.

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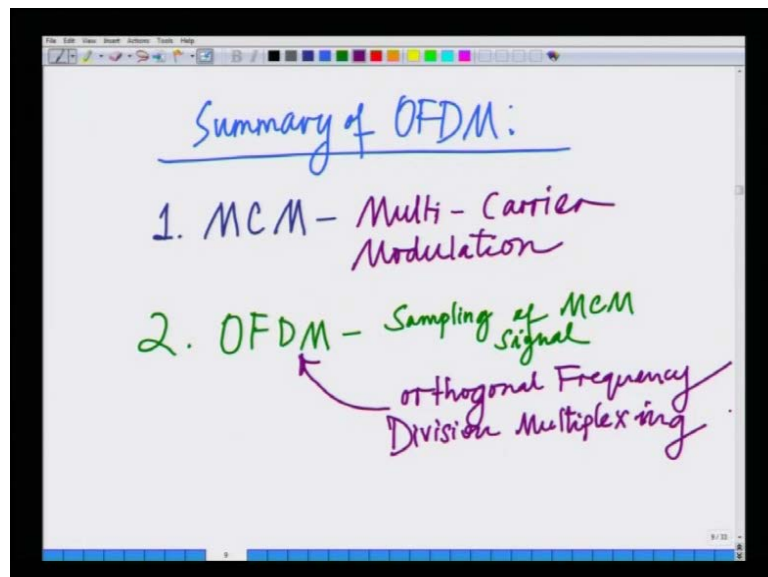
For instance, what can be done, one way to do this is so I have 12 subcarriers. So, how I am going to do, so I have 12 subcarriers. I can load X zeros as follows. I can load X 0, 0, 0 X 1, 0, 0, X 2, 0, 0, X 3, 0, 0, so these are the 12 subcarriers, carriers. I am even looking at this, I am interleaving the zeros with the symbols. So, these are I am interleaving zeros. This is turned as this is termed as interleaved FDMA FDMA or essentially IFDMA, all right? So, one way to load these 4 FFT symbols on to the 12 subcarriers is to interleave them with zeros. I have namely 1 symbol 2 zeros, 1 symbol 0 zeros, 1 symbol 2 zeros, 1 symbol 2 zeros and so on and now perform the N point IFFT. This is known as interleaved FDMA.

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Another way another simply way as we all know is of course, to simply do 0 padding operation. That is written 2, 3, 4, 5. So, again I have 12 subcarriers. So, what I can do here is, I can load them on to the first four subcarriers and leave the rest of them 0. This is essentially 0 padding based subcarrier, mapping this is 0 padding based subcarrier mapping in SCFDMA and this in fact is known as LFDMA. This scheme is termed as LFDMA and in fact this is the scheme that is used in the uplink of the 3 g p p that is 4 generation standard LTE. This is used in employed in uplink of LT LTE, which is the fourth generation 3 g p p.

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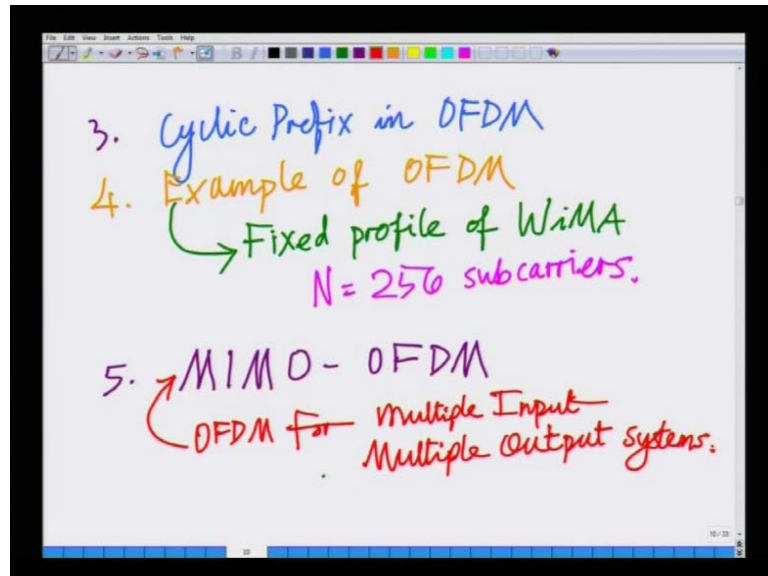


Hence, there are two techniques; one is interleave the 0 this is termed as IFDMA, the other is 2 0 pad, this is termed as LFDMA. In fact this is used in LTE, which is the fourth generation wireless communication standard. So, this brings us to the conclusion of section on OFDM. Hence, let us now summarize the different modules that we have seen in OFDM. Now, let us look at the summary of the OFDM modules that is summary on what we have seen in OFDM so far.

So, in OFDM starting with the first thing we have seen is the first thing we have seen is multi carrier modulation, which forms the basis for OFDM. So, we have started with multi carrier modulation, which forms the basis for OFDM. Second we saw OFDM itself, this leads to OFDM, which is results from the sampling of the MCM signal. This we said sampling of

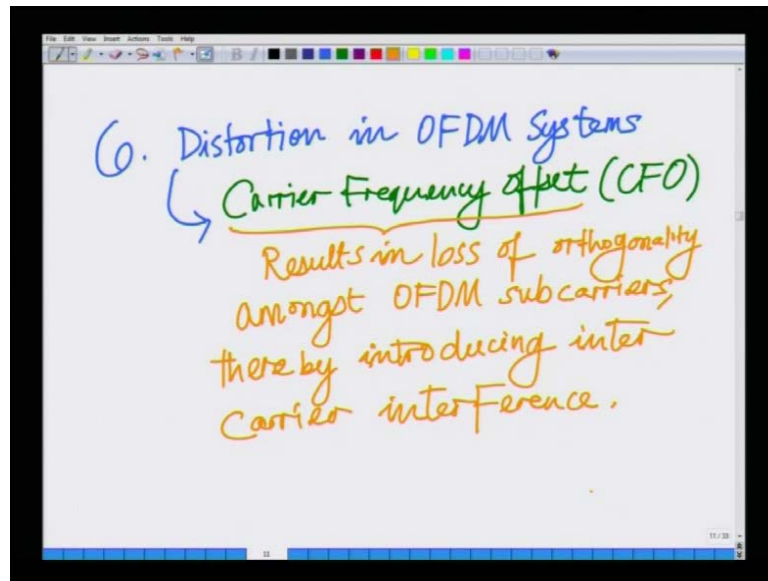
MCM signal, this is nothing but stands for orthogonal OFDM stands for orthogonal frequency division orthogonal frequency division multiplexing.

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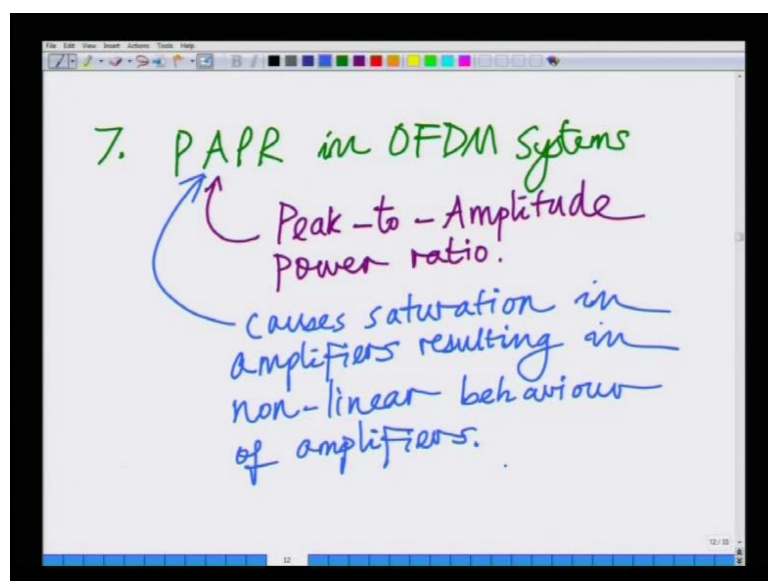
Then we looked at the concept of cyclic prefix we looked at the concept of CP or cyclic prefix. We also looked at an example a practical example of OFDM, this related to the fixed profile of wi max which is the 4 G wireless standard with 256 subcarriers. So, we looked at the fixed profile of wi max, this had N equals 256. This had N equals 256 subcarriers. Then we looked at an important aspect that is MIMO OFDM, which is essentially multiple input multiple output OFDM that is this is essentially OFDM OFDM for multiple input multiple output system. So, this is essentially OFDM for multiple input multiple output systems.

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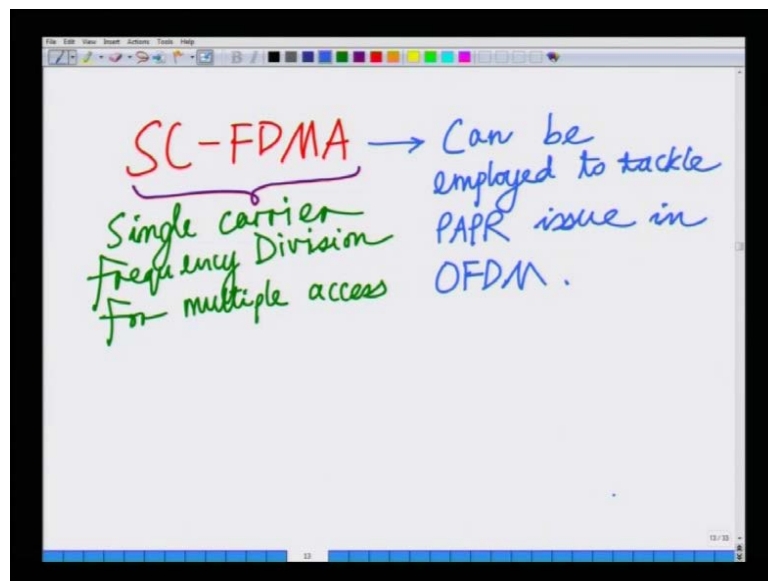
Then we looked at distortion in OFDM systems. We looked at distortion in OFDM systems, namely we looked at the problem of carrier frequency offset or CFO which arises in OFDM. This is serious problem we said because this results in loss of orthogonality amongst OFDM subcarriers thereby introducing inter symbol interference inter carrier interference. Thereby introducing inter carrier interference.

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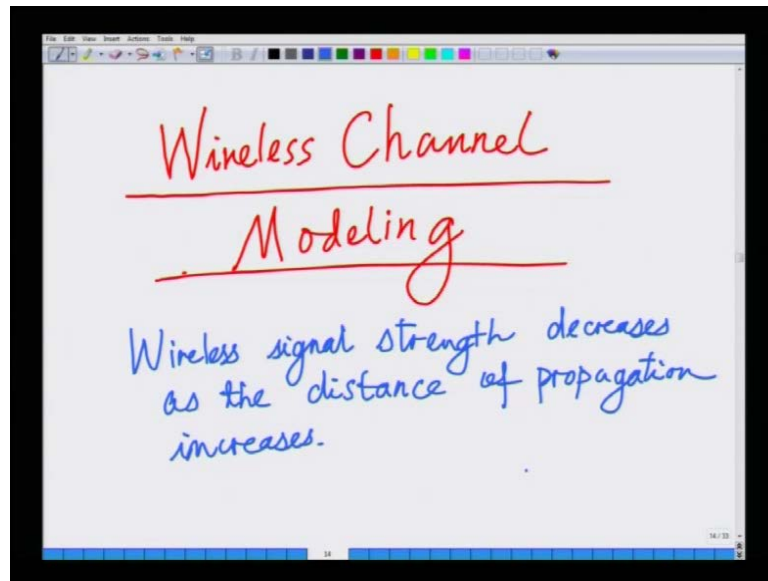
The next we said another important factor that needs to be considered in OFDM is the PAPR in OFDM systems were PAPR stands for peak to amplitude. PAPR stands for peak to amplitude power ratio in OFDM and this also we said causes saturation in amplifiers, causes saturation causes saturation in amplifiers resulting in non-linear behavior, resulting in non-linear behavior of amplifiers in the OFDMA systems. So, that is the problem of PAPR.

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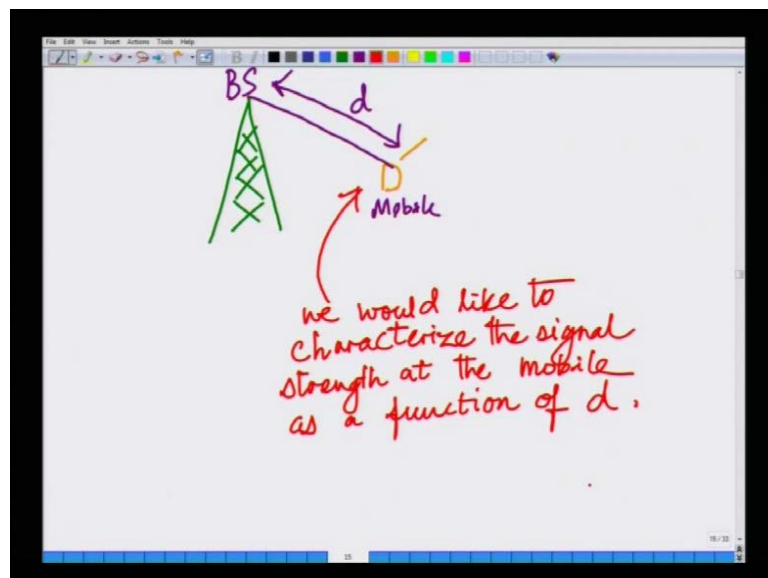
We said tackle the problem of PAPR we can use SCFDMA that is SCFDMA, which stands for single carrier this stands for single carrier frequency division for multiple access. This can be employed to tackle PAPR issue in OFDM, we said PA single carrier FDMA can be employed to address or can be employed essentially to tackle the problem of peak to amplitude power ratio. That is problem high that is the PAPR high peak to amplitude power ratio in OFDM systems. So, with that we come to a conclusion of the OFDM module and now we want to start a new module, which essentially leads to channel modeling in wireless systems.

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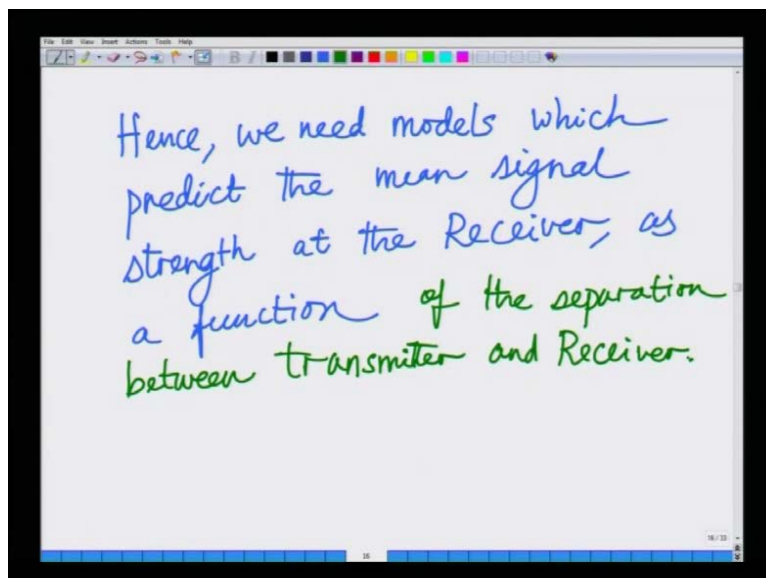
So, the next module we want to talk about or the next module we want to talk about is essentially wireless channel modeling. This is the next topic that we want to talk about and we want we all we know already from our basic knowledge of RF propagation that the wireless signals strength decreases with increasing distance. So, we know that wireless signal strength decreases as the distance of propagation. We know the wireless signal strength decreases as the propagation distance increases.

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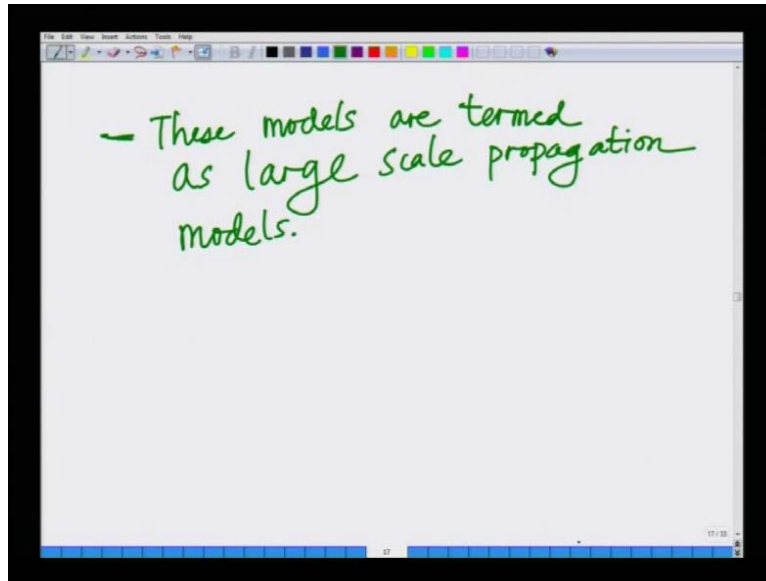
For instance we look at of base station and a mobile and we look at the distance d between the base station and the mobile. In fact we can also look at the straight line distance d between the base station and mobile. We would like to predict, we would like to find the signal strength required at the base station to receive a signal at the mobile at an intelligible signal at the mobile at a distance d . Hence, what we would like to do we would like to do characterize, like to characterize the signals at the mobile as we would like to characterize the signals strength at the mobile, as a function of d . This these since we need models which predict the mean signal strength as a function of the distance between the transmitter and receiver for essentially the design of a cellular system.

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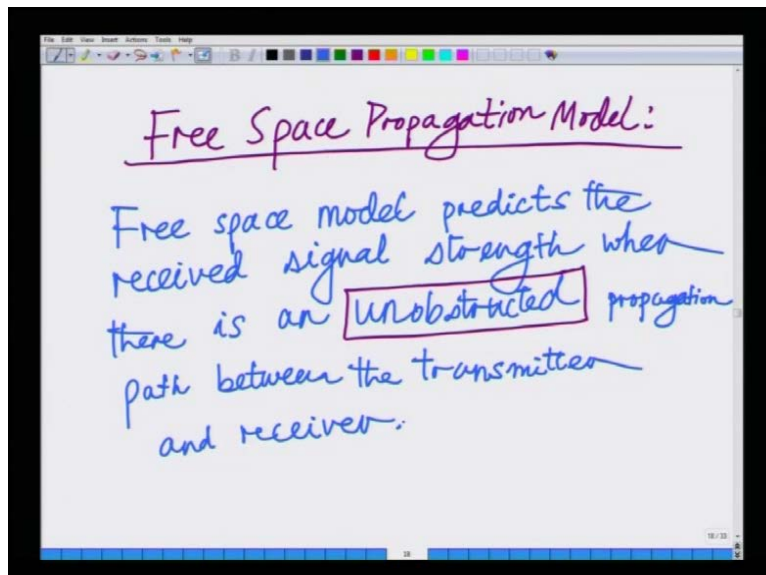
Hence, hence we need models which predict the mean signal strength which predict the mean signal strength at the receiver as a function of the separation between transmitter and receiver. Hence, we need essentially need what do you want to do is we want to build models, which can actually essentially characterize the signal strength at the receiver as the function of the separation between this transmitter, which is the base station and receiver. Same when the mobile is the transmitter and the base station is receiver, we need models which can characterize the signal strength. So, that we can characterize the transmit power. So, that we can characterize the received power and so on and these models are essentially termed as propagation models.

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Hence, these models are termed as channel models or large scale propagation models these models. Models are termed as large scale propagation, these models are termed as large scale propagation model, we will start looking at some of these propagation models to characterize the received signal strength in a wireless communication system.

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So, let us start with the basic model which is the free space propagation model. So, I want to start with the basic model which essentially the, which is the free space propagation model. The free space propagation model it predicts the receive signal strength when there is an

unobstructed part within the between the transmitter and the receiver. So, this the free space model predicts the received signal strength when there is an unobstructed. Remember this is the key which is essentially when there is an unobstructed path between, there is an unobstructed propagation part between the transmitter and the receiver. There is an unobstructed propagation path between the transmitter and the receiver.

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The image shows a handwritten slide titled "Governed by the Friis Free space Equation." The equation is written as:

$$P_r(d) = \frac{P_t G_t G_r \lambda^2}{4\pi d^2 L}$$

Annotations include:

- $P_r(d)$: received power as a function of distance d
- P_t : Transmitted power
- G_t : Transmit antenna gain
- G_r : Receive antenna gain
- λ : Wavelength, where $\lambda = c/f_c$
- d : distance
- L : system loss factor, where $L \geq 1$

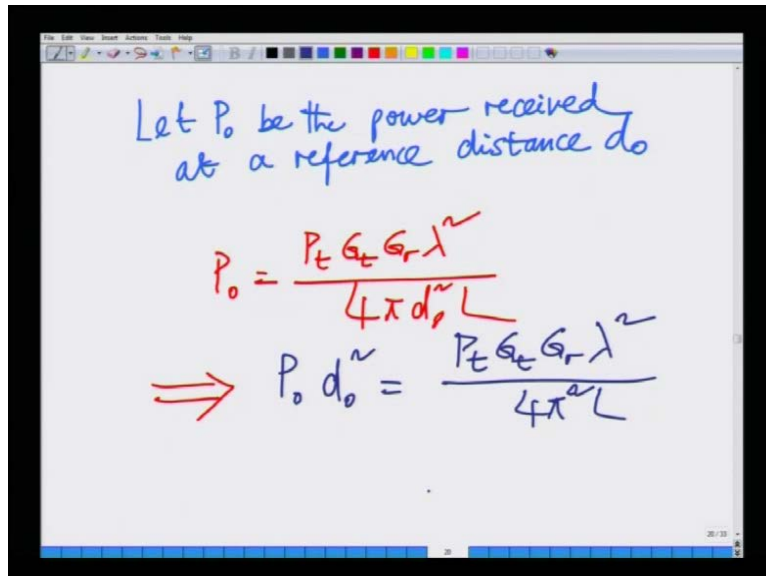
The slide also mentions "Friis Free space Equation" and "PDF file of figure is available on course website".

This is governed by the Friis free space equation. This is governed by the Friis free space equation where they received power as a function of d P_r that is the received power as a function of distance d is given as $P_t G_t G_r \lambda^2$ divided by $4\pi d^2 L$ that is the received power P_r as a function of d is given by $P_t G_t G_r \lambda^2$ divided by $4\pi d^2 L$, where each of this quantities is defined as follows. P_t is nothing but the transmitted, this is the transmitted power G_t is a transmit antenna gain, G_r is a receive antenna gain and λ is nothing but the wavelength, this is the wavelength, which is equal to c/f_c where f_c is the carrier frequency and this d of course, d is the distance.

This L is the system, L greater than equal to 1, this is nothing but the system loss fact. That is why it gives giving by the transmit power times, the transmit antenna again times the receive antenna, again times λ^2 where λ is the wavelength divided by $4\pi d^2$ where s is the distance and the system loss factor all right? So, this is essentially what we have as the expression. So, this is our expression that we have basically for this received

power as a function this this is nothing but the Friis free space equation. Let me just write this again this is nothing but the, this is the Friis, this is nothing but the Friis. Free space equation.

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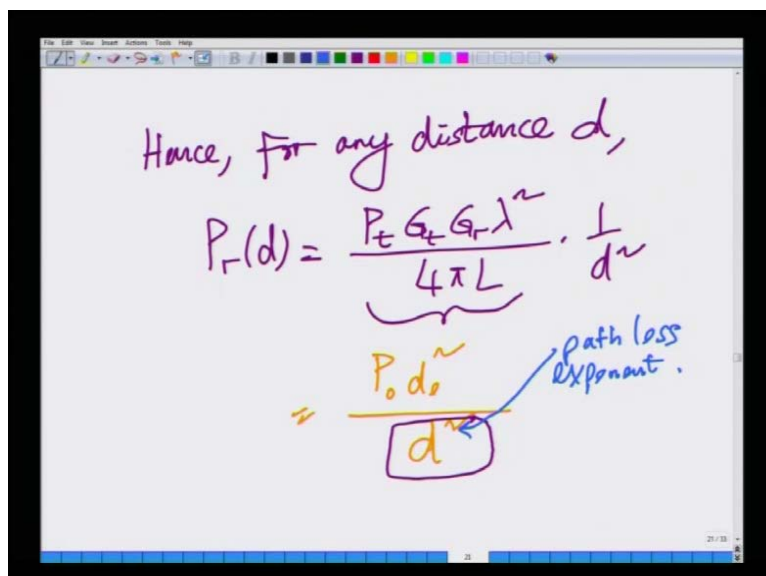
Let P_0 be the power received at a reference distance d_0

$$P_0 = \frac{P_t G_t G_r \lambda^2}{4\pi d_0^2 L}$$

$$\Rightarrow P_0 d_0^2 = \frac{P_t G_t G_r \lambda^2}{4\pi^2 L}$$

Now, we can simplify this a full loss let us consider let P naught be the power received at reference distance d naught, let P naught be the power received at a reference distance d naught, then we have we have P naught equals $P_t G_t G_r \lambda^2$ divided by $4\pi d$ naught square L implies. If we consider P naught d naught square that is equal to $P_t G_t G_r \lambda^2$ by 4π square L that is equal to 4π square L .

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Hence, for any distance d ,

$$P_r(d) = \frac{P_t G_t G_r \lambda^2}{4\pi L} \cdot \frac{1}{d^2}$$

$$\approx \frac{P_0 d_0^2}{d^2}$$

path loss exponent.

Hence, for any distance d , hence for any distance what we have is P received as a function of d equals $P_t G_t G_r \lambda^2$ divided by $4\pi d^2$. This what we already saw is nothing but, $P_{\text{naught}} d^2$ hence this is equal to this is equal to $P_{\text{naught}} d^2$ by d^2 that is the power received at any distance d . Some constant which is $P_{\text{naught}} d^2$ that is reference power P_{naught} received at distance d divided by d^2 .

This factor actually d^2 is the most important that is it shows that the power decreases as the square of the distance. This factor 2 this power 2 is known as the path loss exponent. Shortly we are going to see how the path loss exponent differs its nominally. It is true, but path loss exponent in urban urban regions can be greater than 2 in fact it lies usually between 2 and 4 all right? Hence, one small last step which is we want to cover convert this received power in dB.

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Convert received power to dB

$$P^{db} = 10 \log_{10} P = 10 \log_{10} \frac{P_0 d_0^2}{d^2}$$

$$= 10 \log_{10} P_0 + 2 \times 10 \log_{10} \frac{d_0}{d}$$

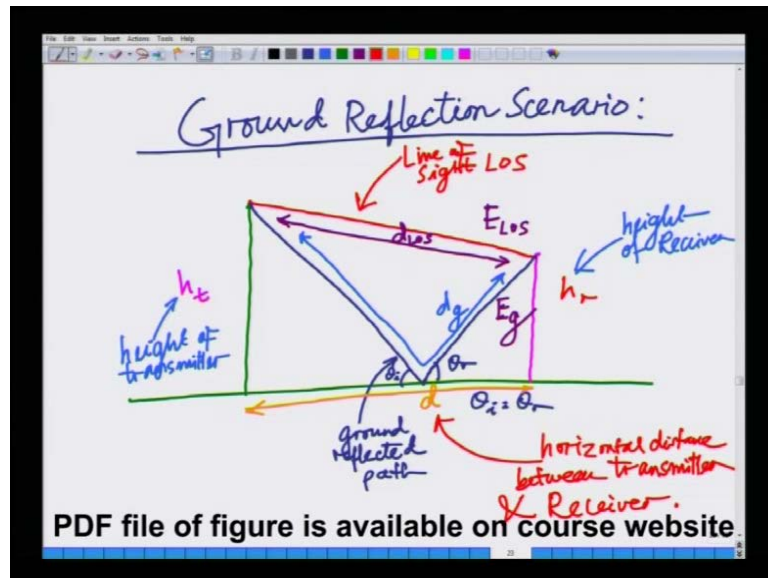
Received power in dB in free space

$$P^{db} = P_0^{db} - 20 \log_{10} \frac{d}{d_0}$$

Convert received power to dB, we have P^{db} is nothing but $10 \log_{10} P$, which is equal to $10 \log_{10} P_{\text{naught}} d^2$ divided by d^2 , which is essentially $10 \log_{10} P$ plus twice into $10 \log_{10} d$ by d , which is essentially P_{naught}^{db} . There is reference power in dB minus $20 \log_{10} d$ by d_{naught} . So, P^{db} this is the free space received power in dB this is a received power in dB in free space. We saw that for free space path loss exponent is true, is 2 for free space.

However, in cellular environments in urban cellular as defined by the first lecture, there is a dense clutter there is lot of scattering there is a lot of reflection. Hence, there is rarely free space propagation alright there might be a line of sight where there are also several reflected and scatter bath in such scenarios. We see that the path laws exponential can be greater than d square. In general the path loss exponent can be in between 2 and 4, we are going to see an example of this, for instance let us consider the ground wave deflection scenario.

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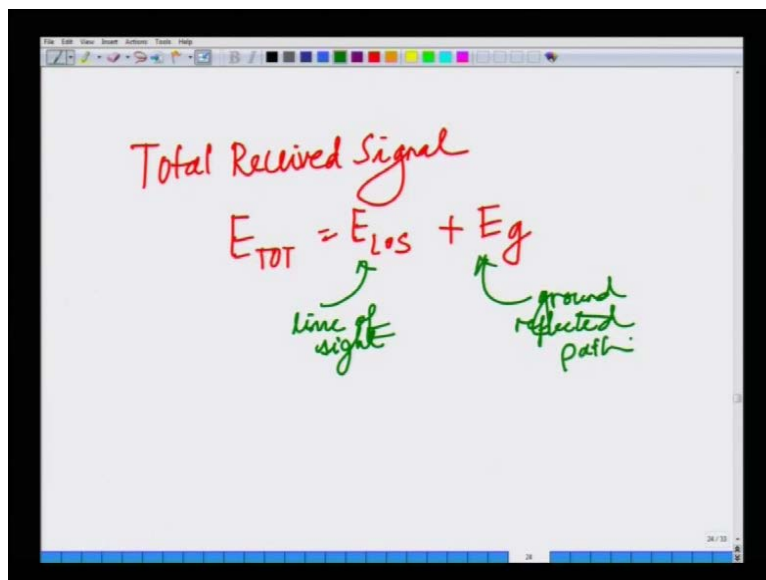
So, let us as an example to see how the path loss exponent can be greater than 2, let us consider a typical ground reflection. Let us consider a typical ground reflection scenario. The ground reflection scenario can be modeled as follows. I have a transmitter at a height t and I have a receiver at height h_r , so h_t is the height of the transmitter h_r is the height of the receiver. Now, there is a direct path between the transmitter and the receiver. This is the line of sight or LOS path between the transmitter and receiver. There is as well also there is also another path which is a reflected path.

So, this path is essentially the ground reflected path such that the angle of incidence θ_i and angle of reflection are equal, angle of incidence and angle of reflection are equal. Let me call this distance as the line of sight distance and let me call this distance as the ground reflection distance. We can see the both these distances are different and we said h_t , this is nothing but the height of transmitter. That is let us say something like height of base station in or cellular

system and this is height of receiver that is length of the height of the person who is talking or may be who is on the building the height of the building and so on.

So, we have two paths now, we have one is the the LOS path. Let us say the field along the receiver of this path is E_{LOS} and the field at this path let us say is E_g , which is get coming from the ground reflected path. Further let us denote this distance horizontal distance between the transmitter and receiver by d , this is nothing but this is essentially horizontal distance between the transmitter. So, this is the horizontal distance between the transmitter and the receiver. So, that is what we currently have. Hence, what we observe is that we have two propagation paths that is one is the direct path one is the reflected path, once the line of statement is the reflected.

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The image shows a whiteboard with handwritten text in red and green. At the top, it says "Total Received Signal" in red. Below that, the equation $E_{TOT} = E_{LOS} + E_g$ is written in red. Under E_{LOS} , there is a green arrow pointing to it with the text "line of sight" written in green. Under E_g , there is a green arrow pointing to it with the text "ground reflected path" written in green.

Hence, the total received signal is nothing but E_{TOT} which is equal to E_{LOS} plus E_g . This is again from the line of sight path and this is from the ground reflected. This is from the line of sight path and the ground reflected path. Now, each signal E_{LOS} first for instance, let us look at the line of sight path that is some E_{LOS}

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$$E_{LOS} = \frac{E_0 d_0}{d_{LOS}} e^{j2\pi F_c \left(t - \frac{d_{LOS}}{c}\right)}$$

E is strength at distance d_0 .

Propagation distance of LOS path

Phase lag of the carrier at receiver arising due to propagation delay

$$\approx \frac{F_0 d_0}{d} e^{j2\pi F_c \left(t - \frac{d}{c}\right)}$$

Let E_0 be the reference strength at some distance d_0 . Remember the power decreases by distance by d^2 in free space which implies the strength of the signal decreases by a factor of d . Hence this is some $E_0 d_0$ and then there is going to be a factor in fact this is d_{LOS} and there is going to be a phase factor that is essentially arising because of the propagation distance. So, in this what we are seeing essentially that $E_0 d_0$ is strength or the field strength at distance d_0 that is some constant d_{LOS} is the propagation distance.

Remember this is the line of sight d_{LOS} is the line of sight propagation distance or propagation distance of LOS path. This we are saying is the phase factor arising in the carrier due to the propagation, this is the phase lag of the carrier at receiver arising due to propagation delay. Now, what I am going to do is I am going to use an approximation. I am going to set this d_{LOS} in the denominator as approximately equal to d .

Hence, I am going to use the approximation that this is approximately equal to $E_0 d_0$ divided by d times $e^{j2\pi F_c \left(t - \frac{d_{LOS}}{c}\right)}$, where I have approximated d_{LOS} that is the line of sight distance by the signal strength by d , because the major effect of the propagation distance is in the phase factor. The effect on the signal strength is not very significant. So, due to due to so because of shortage of time I have to end this lecture here and then again we are going to start from here and continue with this in the next lecture.

Thank you very much.