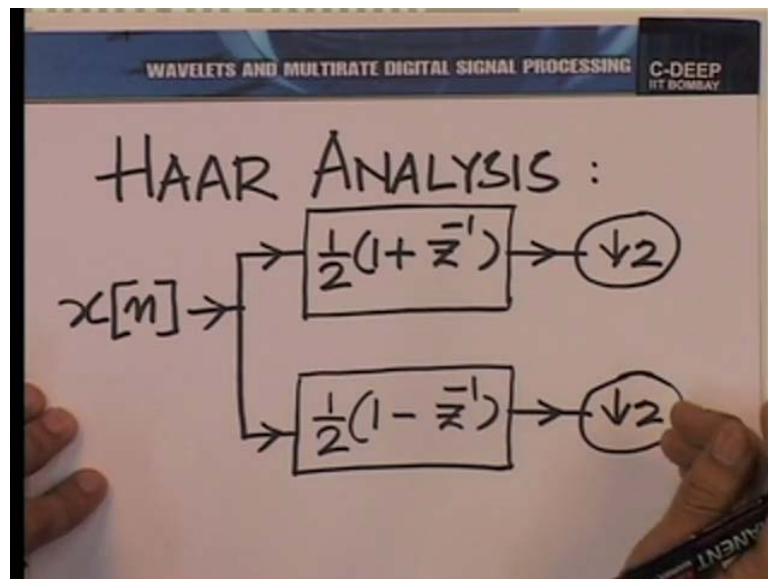


**Advanced Digital Signal Processing – Wavelets and Multirate**  
**Prof. V.M. Gadre**  
**Department of Electrical Engineering**  
**Indian Institute of Technology, Bombay**

**Module No. #01**  
**Lecture No. #07**  
**Haar Filter Bank Analysis and Synthesis**

A very warm welcome to the seventh lecture on the subject of wavelets and multi-rate digital signal processing. Recall that we had ended the previous lecture by hinting at the structure of the synthesis filter bank corresponding to the Haar multi resolution analysis. Today, we begin by looking at both the analysis side and the synthesis side once again. I mean the analysis filter bank and the synthesis filter bank in the Haar multi resolution analysis.

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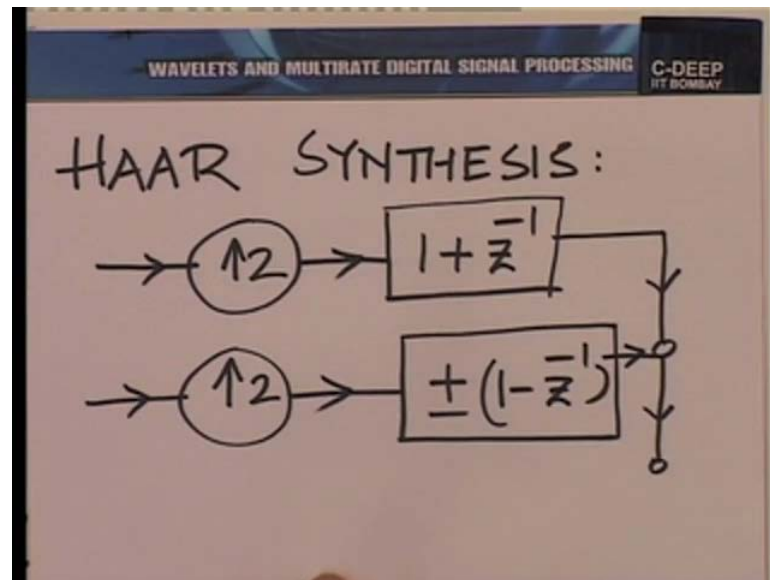


So, I just put down the two filter banks. Clearly, you will recall that on the analysis side, we had a structure like this. We had the sequence, let us call it  $x$  of  $n$  corresponding to this to the function in V1. Essentially, it was subjected to the action of two filters. A filter of the form half 1 plus  $Z$  inverse, another one of the form half 1 minus  $Z$  inverse followed by a down some link by 2.

We had also derived the structure of the synthesis filter bank and interestingly, we saw the structure was very similar. In fact, it looked almost like a mirror image here. Except

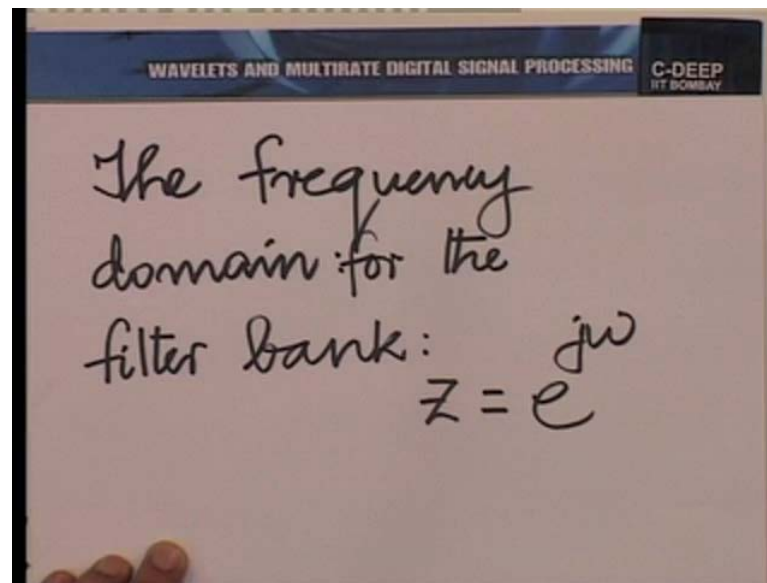
for the fact that you had an up sampler instead of a down sampler followed by the filters once again, so here the filters had the form  $1 + Z^{-1}$  and  $1 - Z^{-1}$ . Now, the only catch is I am going to allow for an ambiguity of sign here plus 1 minus  $Z^{-1}$  inverse. A small variation from last time, a subtle point but important.

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Now, there are several things to which we must pay attention. One is if you look at the structure of the analysis in the synthesis filter banks, the filters are almost identical. These are the two filters for the analysis side and these are the two filters for the synthesis side.

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Please note I am allowing an ambiguity here. What would be the physical meaning of the ambiguity be? If you just determine where I place the some sample and the different sample. With a plus sign, the some sample will get placed at the even locations and the different sample at the odd locations. With the minus sign to be the other way around, so let us leave the ambiguity for a moment.

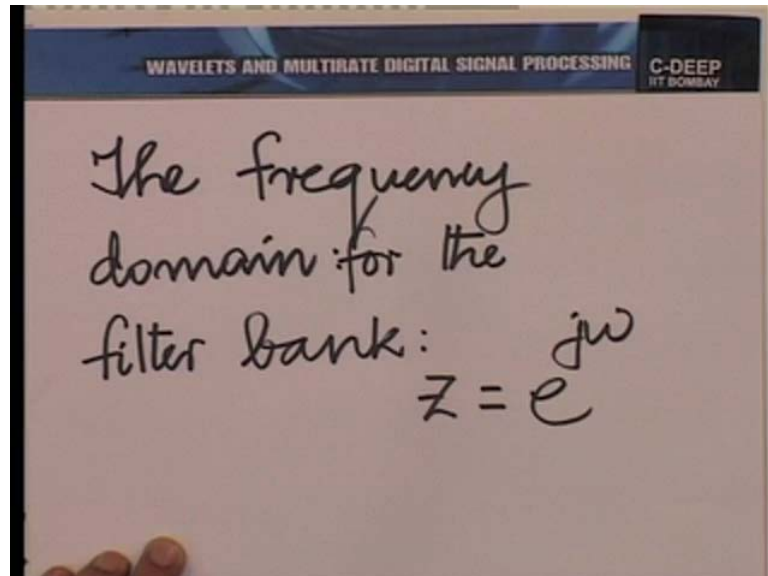
If we try and resolve the ambiguity right away, we might actually get more confused. So, allowing the little ambiguity for a moment, let us analyse the whole structure in general and then resolve the ambiguity. Anyway, coming back to the filter banks structures, we see one very beautiful thing that we notice about the Haar filter bank is that the filters on the analysis side and the synthesis side are almost the same, except for this sign ambiguity.

If we really look at it, these two filters are also very meaningful in another domain of which we shall soon have more information. Now, what we going to do from here onwards, is to look at this general structure. You see we want to understand why there are multi-resolution analysis though attractive is not adequate.

I have been saying all the while that if we understand the Haar multi-resolution analysis and if we understand the filter bank corresponding to the Haar multi-resolution analysis, we understand quite great deal about filter banks and multi-resolutions analysis. Most of

the concepts are captured, then why should we look for other multi-resolution analysis. That is a subtle point which we shall see by going into other domain.

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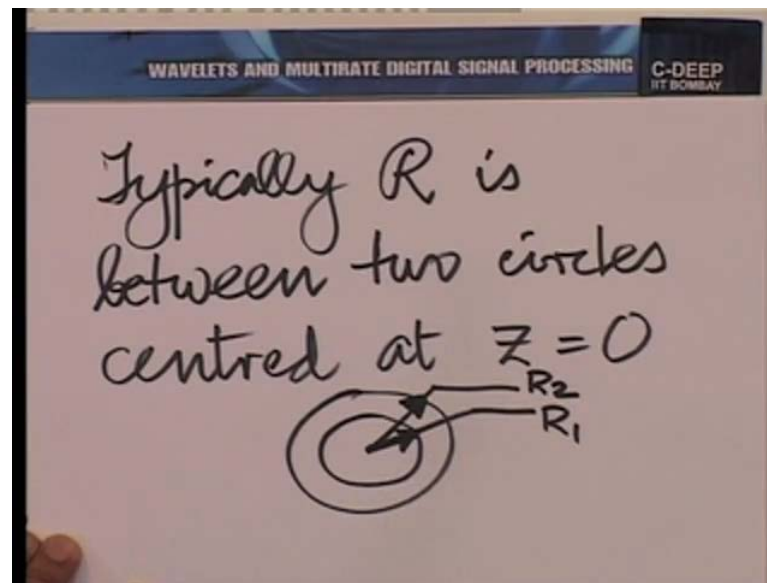


Now, our objective here is to look at the frequency domain behaviour and how would we get a frequency domain representation of the Haar filter bank. So, what we will do is, we will progress follows first we shall look at the frequency domain for the filter bank. How would we do that? We would do that by substituting  $Z$  equal to  $e$  raise the power  $j$   $\omega$ .

Let me once again recapitulate a few concepts from discrete time signal processing for the benefit of the class. Although, one would have done this in course on discrete time signal processing, it helps to put some of this discussion in prospective.

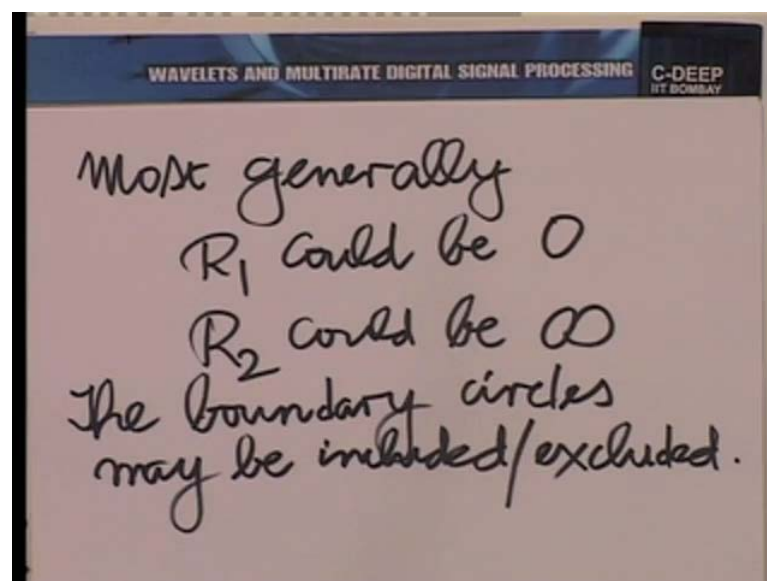
You will recall that we had defined the  $Z$  transform last time. We had said that if you have a sequence  $x$  or  $n$ , its  $Z$  transform is capital  $x$  of  $Z$  defined by summation  $n$  running from minus to plus infinity  $x$  of  $n$   $Z$  raise the power minus  $n$  with  $Z$  belonging to a region of convergence.

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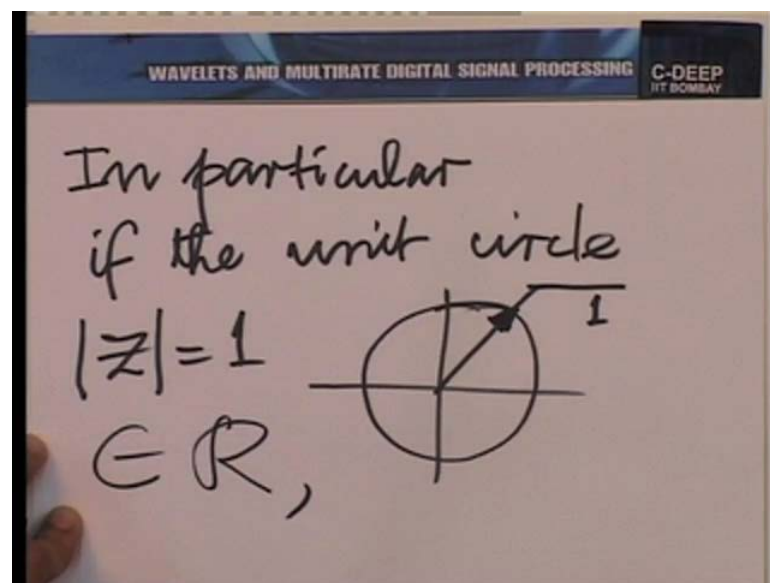
Now, in particular if the region, so let the region be script  $R$ , in particular if this region includes the unit circle, so you know let me say a little bit about the regions of convergence of a typical  $Z$  transform. Typically,  $R$  has the following patterns.  $R$  is between two circles centred at the origin. So, it has an appearance something like this and both of these are centre at the origin. So, you have  $R_2$  and  $R_1$ . So, you know here the radius is  $R_1$ . I mean here the radius is  $R_2$ .

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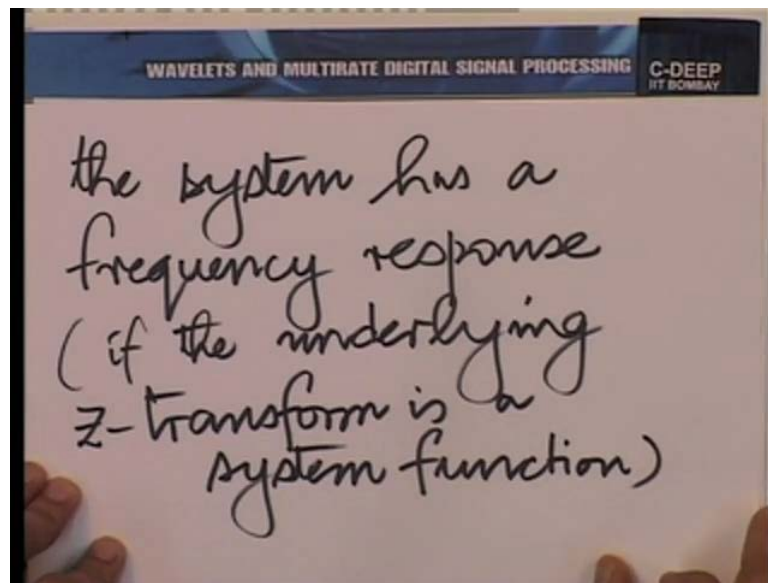
Now, it could be true that  $R_2$  might be infinity or  $R_1$  might be 0. So, we have to allow these possibilities. Most generally,  $R_1$  could be 0,  $R_2$  could be infinity. Moreover, the boundaries may or may not be included; the boundary circles may be included or excluded. In fact, if these values  $R_1$  and  $R_2$  are non 0 and finite, most of the time the boundaries are excluded. It is only when  $R_2$  becomes infinity or when  $R_1$  becomes 0 that there is a question is the boundary included or excluded and that is not a trivial issue. Whether the boundary is included or excluded makes the difference to the properties of the system.

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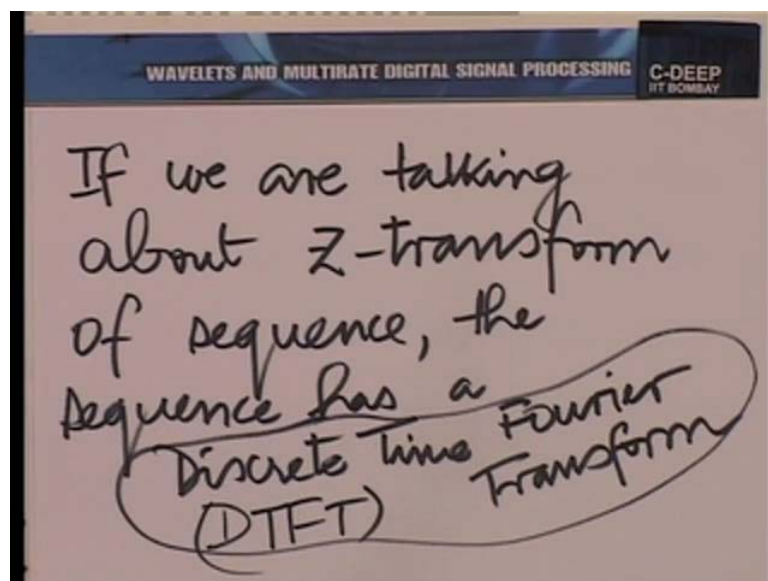
Well, all these is essential to recall a few points about the Z transform and now coming to the frequency domain. So, in particular if the unit circle that is  $\text{mod } Z$  equal to 1 is a circle, you see  $\text{mod } Z$  is equal to 1 is a circle of radius 1 in the Z plain. Say, if the unit circle is included in  $R$ , then we have a frequency response for the system.

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The system has a frequency response. That is you see we talk about the system having a frequency response if in the underlying Z transform is a system function. If the underlying Z transform is a system function and of course, otherwise in case we are talking about a sequence, then we say the sequence has a discrete time fourier transform.

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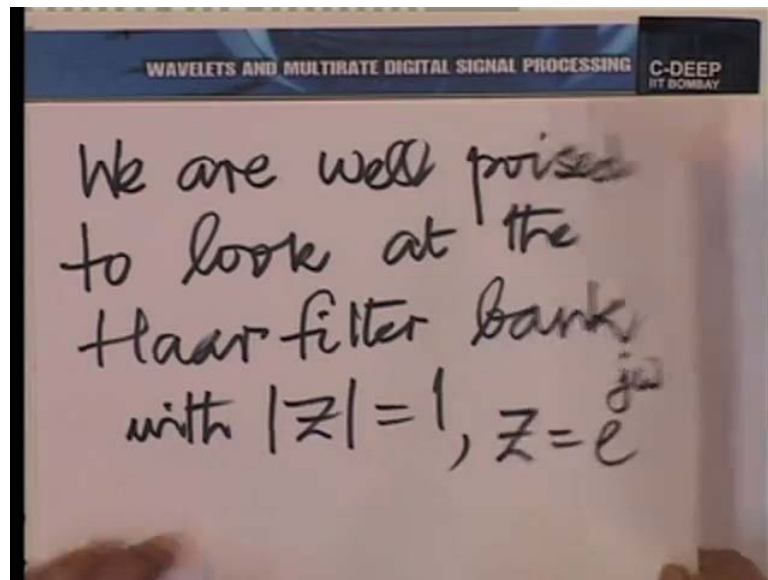


So, if we are talking about the Z transform of a sequence, we say the sequence has a Discrete Time Fourier Transform. This is an important concept DTFT for short. Either



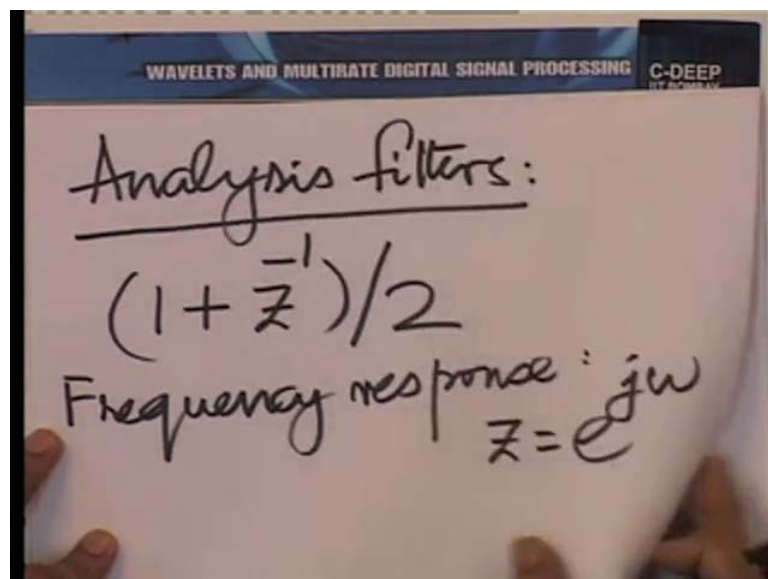
way, what we are saying is in case the units circled are included in the region of convergence, then we have an even more interesting interpretation of the system function of the sequence in question and in fact, if we look at all the Z transforms encountered in the Haar filter bank, they all satisfies.

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So, we are now entitled or we are now well poised to look at the Haar filter bank in the frequency domain. What do we mean by the frequency domain with mod Z equal to 1 or Z equal to e raise the power j omega.

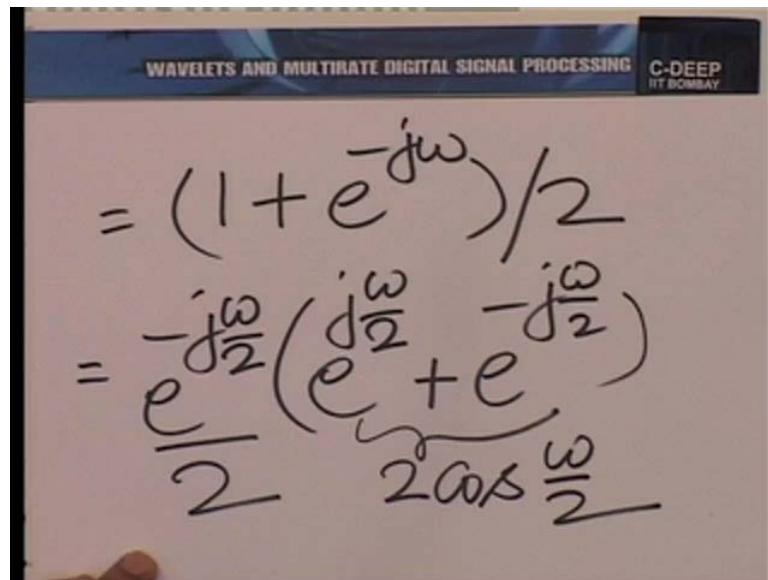
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Indeed, consider the analysis side and the analysis filters, both of them have a frequency response obviously. Let us take the filter  $1 + Z^{-1}$  by 2 and let us look at its frequency response. Of course, we would obtain the frequency response by substituting  $Z$  equal to  $e^{j\omega}$ .

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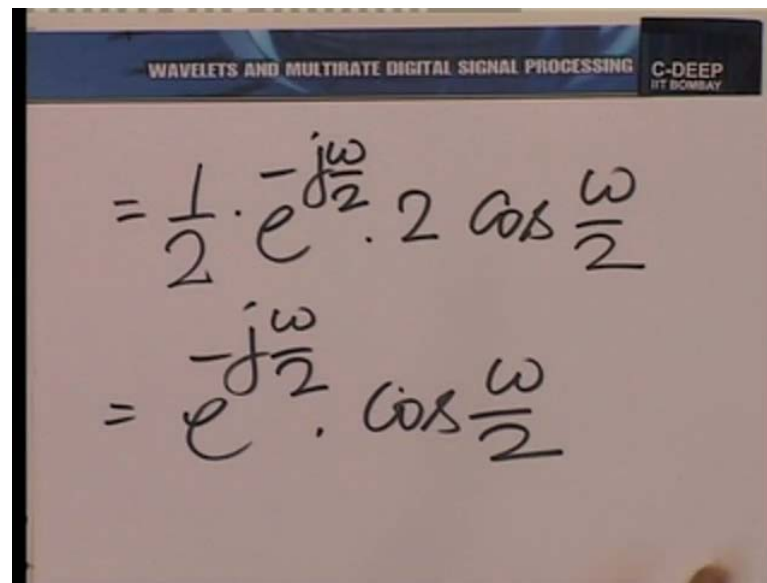


$$\begin{aligned}
 &= (1 + e^{-j\omega})/2 \\
 &= e^{-j\frac{\omega}{2}} \left( e^{j\frac{\omega}{2}} + e^{-j\frac{\omega}{2}} \right) / 2 \\
 &\quad \quad \quad \underbrace{\hspace{1.5cm}}_{2 \cos \frac{\omega}{2}}
 \end{aligned}$$

That would give us  $1 + e^{-j\omega}$  by 2. If you like which we can simplify, we can take  $e^{-j\omega/2}$  common here and then put  $e^{j\omega/2} + e^{-j\omega/2}$  inside the bracket and leave the half factor as it is.

So, this is what we have here. Now, recognise this is essentially 2 times  $\cos(\omega/2)$  and therefore, we have  $e^{-j\omega/2}$  times  $\cos(\omega/2)$ . This is the frequency response.

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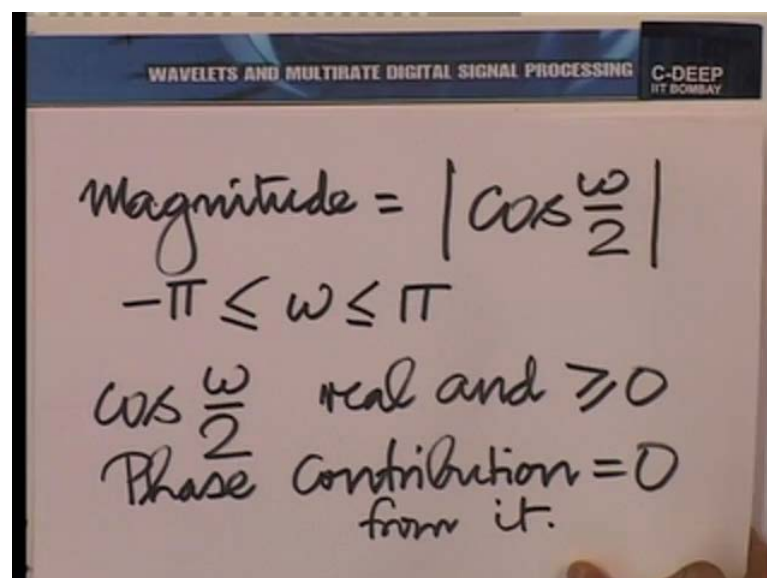


The image shows a handwritten derivation on a slide titled "WAVELETS AND MULTIRATE DIGITAL SIGNAL PROCESSING" by "C-DEEP IIT BOMBAY". The derivation is as follows:

$$= \frac{1}{2} \cdot e^{-j\frac{\omega}{2}} \cdot 2 \cos \frac{\omega}{2}$$
$$= e^{-j\frac{\omega}{2}} \cdot \cos \frac{\omega}{2}$$

Let us sketch the magnitude and the phase of this frequency response and recall that for discrete systems, it is adequate to sketch the magnitude and phase **of for a for that** to determine the magnitude and phase response in the region  $\omega$  going from minus  $\pi$  to plus  $\pi$ . We do not need to go outside that way because after all the frequency response is periodic to the period of  $\pi$ . So, whatever between minus  $\pi$  and  $\pi$  is going to be repeated around every multiple of  $2\pi$ .

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The image shows a handwritten analysis on a slide titled "WAVELETS AND MULTIRATE DIGITAL SIGNAL PROCESSING" by "C-DEEP IIT BOMBAY". The analysis is as follows:

$$\text{Magnitude} = \left| \cos \frac{\omega}{2} \right|$$
$$-\pi \leq \omega \leq \pi$$

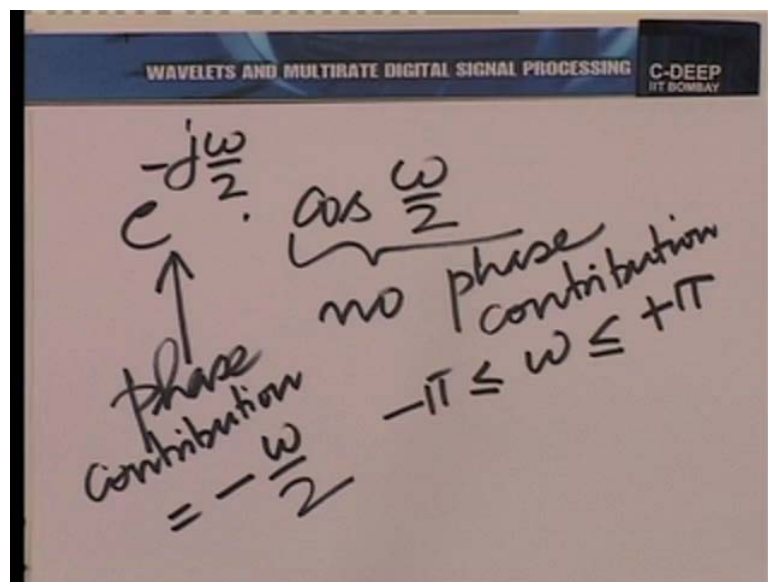
$\cos \frac{\omega}{2}$  real and  $\geq 0$

Phase Contribution = 0 from it.

So, the magnitude of this response would be  $\cos \omega$  by 2 and let us confine as I said  $\omega$  between  $\pi$  and  $-\pi$  where upon  $\cos \omega$  by 2 turns out to be non negative. In fact, essentially  $\cos \omega$  by 2 is real and greater than equal to 0 in this region. Thus, phase contribution for this term is 0. Say, if you look at the overall frequency response here, namely  $e^{j\omega} \cos \omega$  by 2 times  $\cos \omega$  by 2. This has no phase contribution.

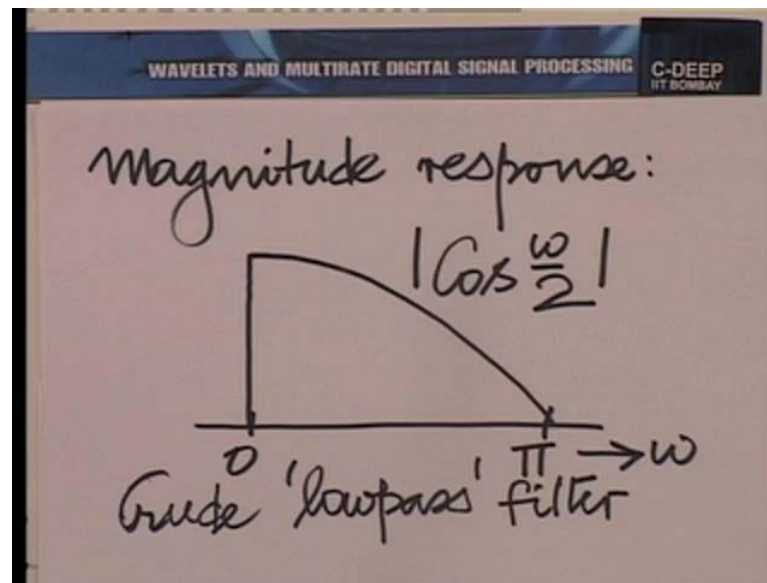
For  $-\pi \leq \omega \leq \pi$  and the phase contribution comes only from here. The phase contribution from this term is going to be equal to  $-\omega$  by 2.

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So, now we can sketch the phase and magnitude contributions very clearly. Let us sketch the magnitude response. The magnitude again, you know this is a real filter. This is a filter with a real impulse response.

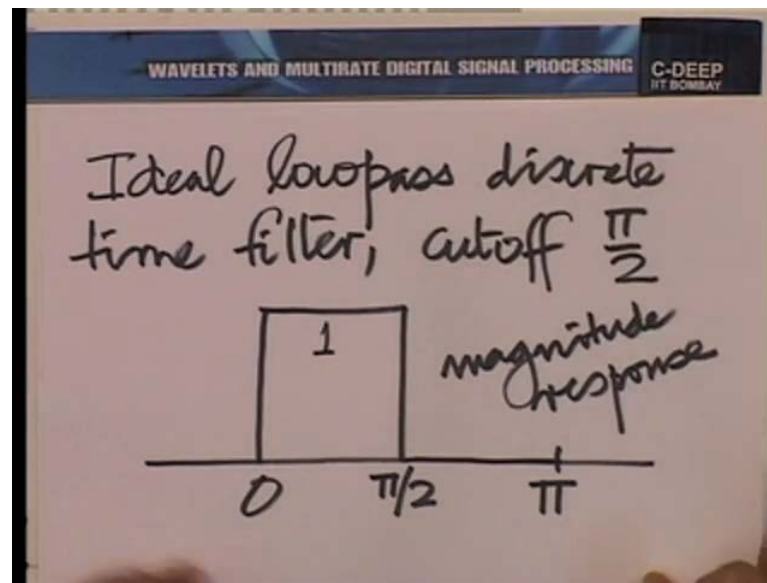
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Now, when an impulse response is real, the frequency response is conjugate symmetric. So, whatever is the  $\omega$  is also at  $-\omega$  in magnitude. Whatever is the  $\omega$  in phase is the negative of what is there at  $-\omega$  in phase. So, we need only to sketch the magnitude response and the phase response between 0 and  $\pi$ . We can ignore  $-\pi$  to 0 because there is going to be conjugate symmetry.

So, let us sketch it only between 0 and  $\pi$ . You can see that this is the kind of pattern that is going to show essentially of the form  $\cos \frac{\omega}{2}$  and for the moment, we can already see that this is something like a crude low pass filter. I say it is a low pass filter because it emphasises the lower frequencies and de-emphasises the higher frequencies. I say it is crude, it is far from ideal. In fact, if you have ideal low pass filter, then of course you need to specify the cut off  $\omega_c$ .

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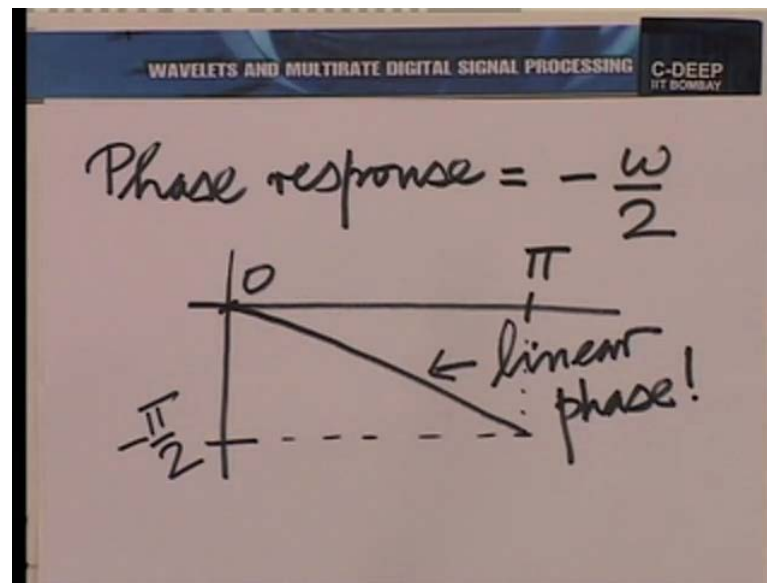


So, an ideal low pass discrete time filter with a cut off of  $\pi/2$  would look something like this. I mean in the magnitude sense. So, it would have a magnitude response that looks like this and ideally, the phase response would be  $0$ . So, it would be  $1$ . The response itself would be  $1$  between  $0$  and  $\pi/2$  and  $0$  between  $\pi/2$  and  $\pi$  and of course, mirrored as it is between minus  $\pi$  and  $0$ .

So, ideally we would have this magnitude and phase equal to  $0$  where are we in reality. We are trying to replace this ideal filter here with this crude approximation to the low pass filter here. So, please remember this is the ideal towards which we are striving and this is where we have reached in some sense with this very simple Haar multi-resolution analysis or Haar filter bank.

Now, we shall understand this even better. When we look at the magnitude response of the high pass or the other filter in the filter bank but for the moment, let us complete our discussion by also drawing the phase response. So, the phase response of this filter is as follows.

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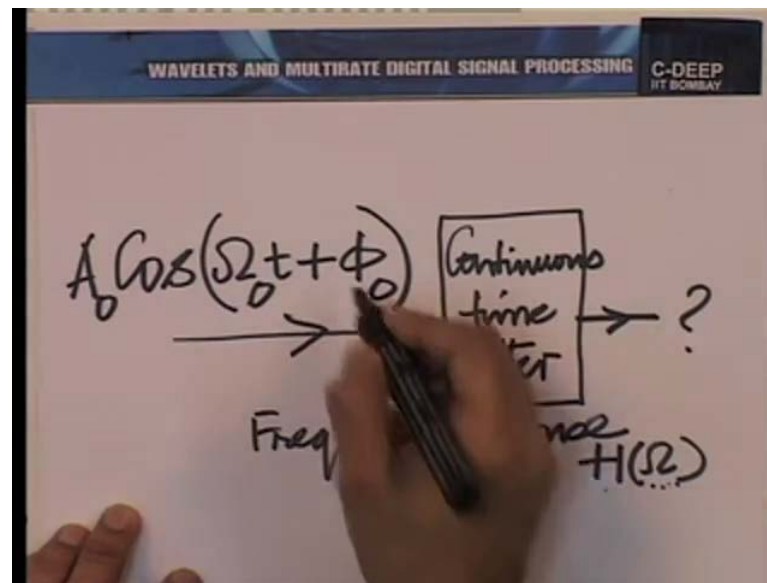


The phase response as we noted was minus omega by 2, so in the region from 0 to pi. At pi it would of course take on the value of minus pi by 2 and this is a straight line. So, in fact you get what is called linear phase. Now, linear phase is something very attractive in discrete time signal processing. In fact, one of the reasons why people go to discrete time signal processing from analog signal processing is because you can get linear phase.

Why is linear phase important? Let us spend a minute in reflecting on this. You see what is a phase response denotes or for the matter what is the frequency response denote?

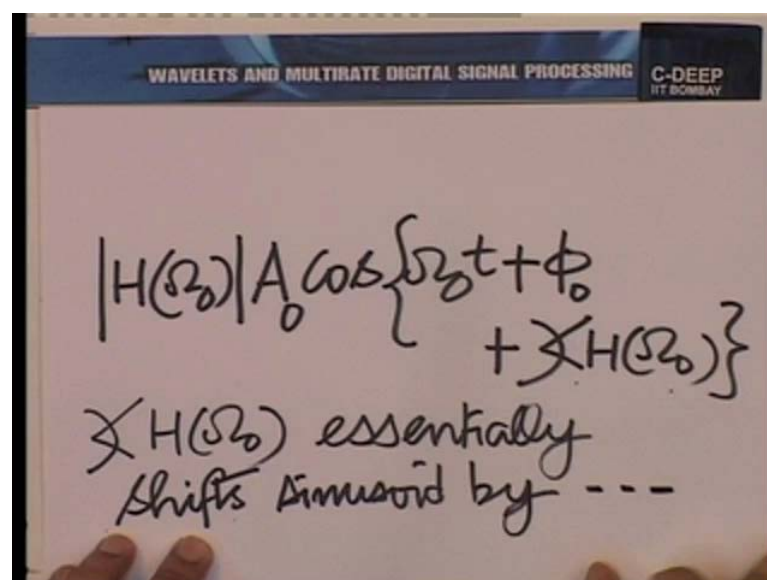
The frequency response tells us what happens to a sine wave when it passes through the system. So, in fact to understand this better, let us go to continuous time. First, suppose we fed a sine wave, let us say  $\cos \omega_0 t + \phi_0$  times  $A_0$ . So, amplitude  $A_0$  frequency  $\omega_0$  phase  $\phi_0$  to a continuous system to a continuous time filter. With frequency response, let us say  $H$  as a function of  $\omega$ . What would come out? Very simple.

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You would evaluate the frequency. This is of course, a complex number as a function of capital omega. You would evaluate this at omega equal to omega naught. The magnitude would multiply the magnitude. The angle would add to the angle here. In another words, what would come out is mod H evaluated at omega naught, A naught cos omega naught t plus phi not plus angle of H evaluated at omega naught.

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What is the effect of this angle? As you can see the effect of this angle is to change the phase and a change of phase is equivalent to a change in time. So, it is like shifting the



time, shifting the sine wave on the time axis. So, angle  $H\omega_0$  naught essentially shifts the sine wave, shifts the sinusoid by well you know,  $T$  is to be replaced by  $T$  plus something and that plus something is given by this divided by  $\omega_0$ .

So, let us write it out explicitly that way. Let us reason out what it should be explicitly. So, we will rewrite that expression.

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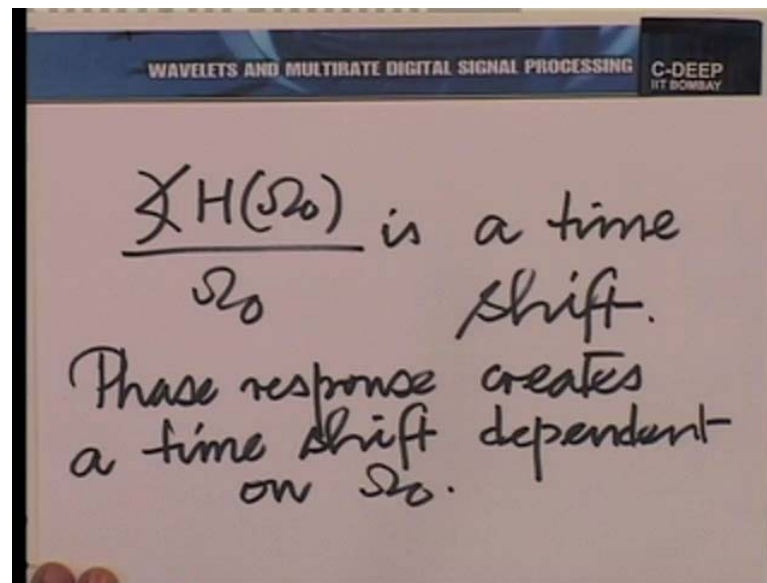
$$|H(\Omega_0)|A_0 \cdot \cos \left\{ \phi_0 + \Omega_0(t) + \frac{\angle H(\Omega_0)}{\Omega_0} \Omega_0 \right\}$$

$\Rightarrow t$  replaced by  $t + \frac{\angle H(\Omega_0)}{\Omega_0}$

We will write it as  $\text{mod } H\omega_0$  naught times  $A$  naught  $\cos$ . We keep  $\phi$  naught as it is. We will take  $\omega_0$  naught common and then we write  $t$  plus, the angle of  $H\omega_0$  naught divided by  $\omega_0$  naught. I am sorry. Yeah. Well, I will write  $\omega_0$  naught  $t$  plus this into  $\omega_0$  naught. So, again you know you have angle here. So, this into  $\omega_0$  naught, I will write in this way.

So, now I can rewrite, so forgetting about this part. See this part is eventually a change of magnitude. It is only this part I need to focus on.  $T$  has been replaced by  $t$  plus angle  $H\omega_0$  naught by  $\omega_0$  naught. So, essentially this quantity angle  $H\omega_0$  naught divide by  $\omega_0$  naught is like a time shift. Is that right? It is an important observation we made.

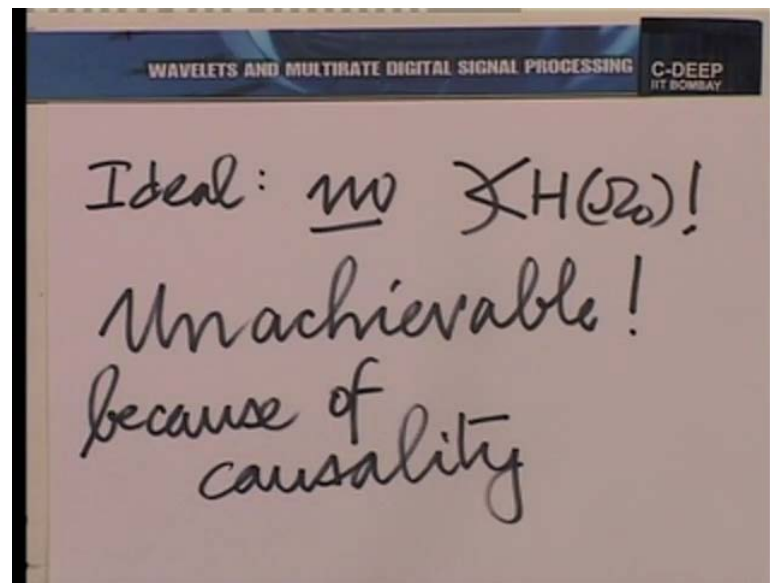
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Now, just in case it is independent of omega naught, we have a good situation. So, you know this time shift actually is what is called a necessary evil in the frequency response. You know most of the time when we give specifications for designing a filter, whether it is in the angular domain or in the discrete time domain, we do not really want the phase response. The phase response comes as a necessary evil and we have to work around it.

Now, what does a phase response do? At each frequency, it creates a time shift. The phase response creates a time shift dependent on frequency. What is a good situation to have an ideal situation is? No phase response. This is unachievable. In fact, it is unachievable because of causality. You know if you want the filters to be causal, then you cannot ask for 0 phase.

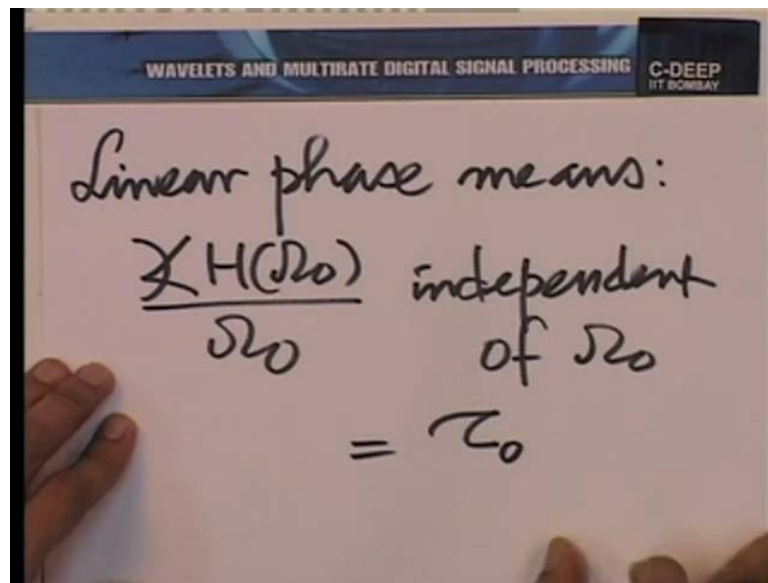
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Incidentally, that is why you can 0 phase filters in dealing with images in dealing with two dimensional data because in two dimensional data, causality is not an important requirement but when you are dealing with one dimensional data in time, causality is essential. You cannot avoid it and therefore, you cannot avoid a phase response either.

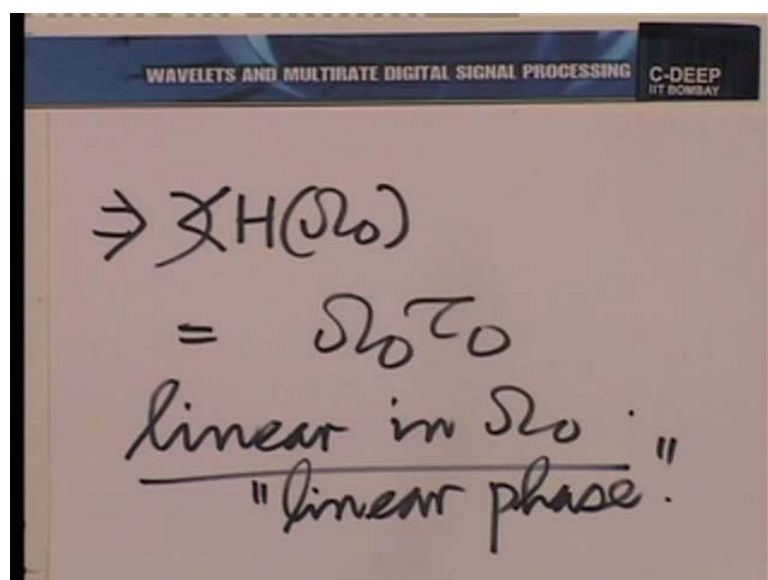
Now, if you must live with a phase response, what kind of a phase response would you like to live with? You would like to make sure the phase response does not treat different frequencies differently. So, if it has to shift a sine wave in time, so be it but then shift all sine wave by the same time and that is exactly what we are saying when we talk about linear phase.

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Linear phase means, angle  $H(\omega)$  divided by  $\omega$  is independent of  $\omega$ . That means it is a constant. Let us say it is some  $\tau_0$  or  $\tau_0$  if you like which means that the angle of  $H(\omega)$  is at the form some  $\omega$  times  $\tau_0$ . It is linear in  $\tau_0$  in  $\omega$ . That is why it is called linear phase.

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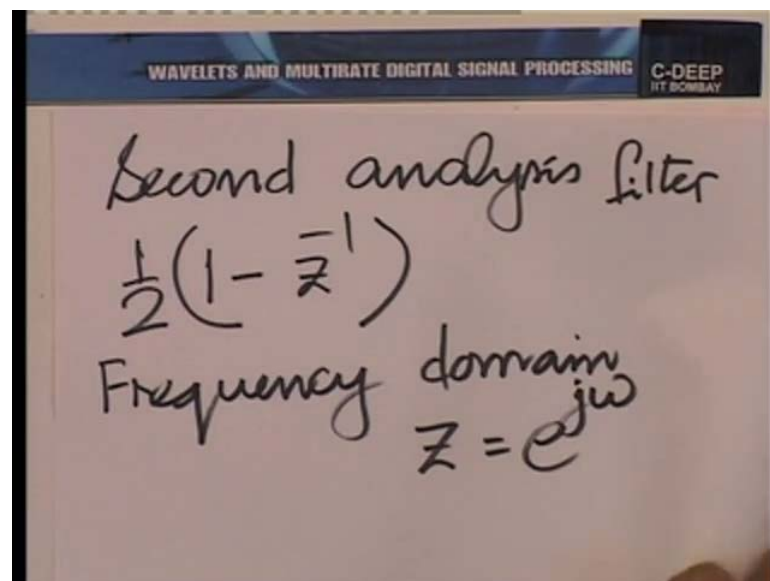
Now, this is what I am trying to emphasise at this point. This very simple filter bank, the Haar filter bank has this beautiful property of linear phase. By the way, this is something

unusual in filter banks. It is not easy to design filter banks of larger order with linear phase. In fact, only one class of filter banks has this property.

Linear phase in some sense has to be compromised with something else. So, in the Haar, you can have your cake and eat it too. So, you can have linear phase, you can have orthogonality but later we will see that if you know want to get something else out of your filter banks, if your filter bank must be better in some sense, you have to sacrifice linear phase.

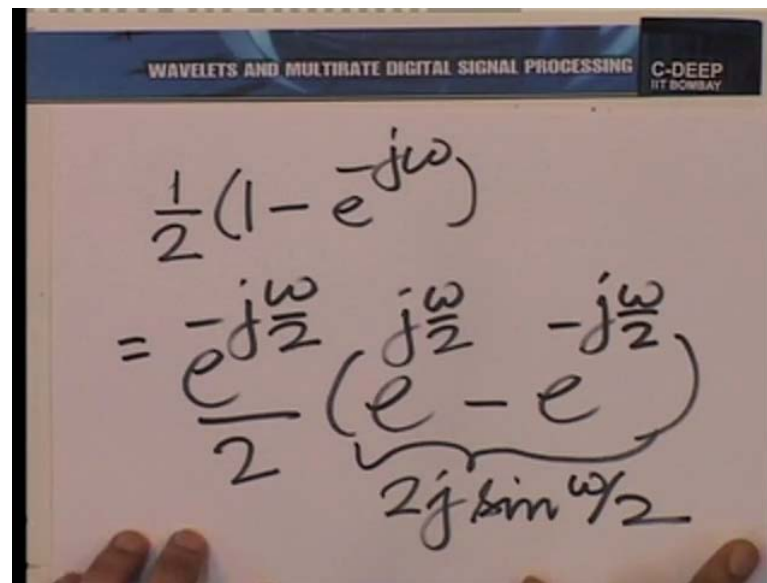
Anyway, so far so good we have linear phase. We are not going badly and if we look at the second filter in the Haar filter bank, we shall have something similar. So, let us look at the second filter.

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The second analysis filter and that is of course, 1 minus Z inverse into half. Let us again find out how the filter looks in the frequency domain. The frequency domain would show it as Z equal to e raise the power j omega where upon we have 1 minus e raise the power minus j omega by 2 and we play the same trick.

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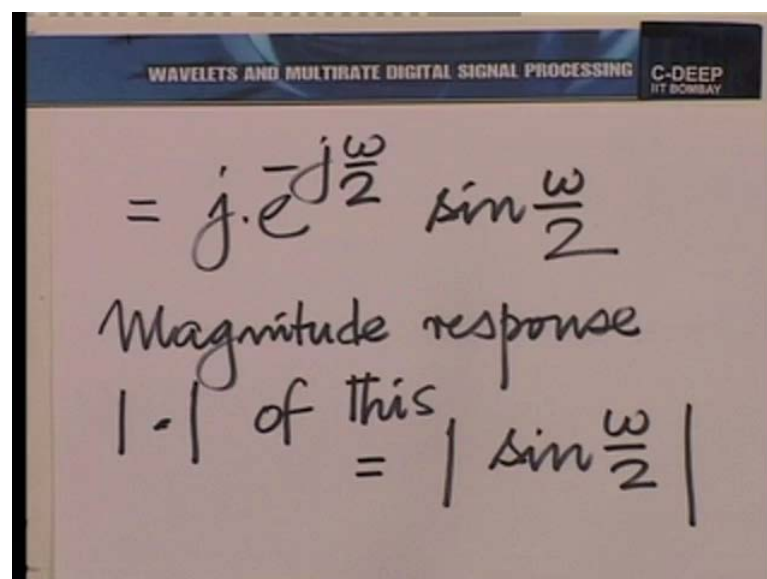


The image shows a handwritten derivation on a slide titled "WAVELETS AND MULTIRATE DIGITAL SIGNAL PROCESSING" by "C-DEEP IIT BOMBAY". The derivation starts with the expression  $\frac{1}{2}(1 - e^{-j\omega})$ . This is then rewritten as  $\frac{e^{-j\frac{\omega}{2}}}{2} (e^{j\frac{\omega}{2}} - e^{-j\frac{\omega}{2}})$ . A bracket under the term in parentheses indicates it is equal to  $2j \sin \frac{\omega}{2}$ .

$$\frac{1}{2}(1 - e^{-j\omega})$$
$$= \frac{e^{-j\frac{\omega}{2}}}{2} (e^{j\frac{\omega}{2}} - e^{-j\frac{\omega}{2}})$$
$$= \frac{e^{-j\frac{\omega}{2}}}{2} \cdot 2j \sin \frac{\omega}{2}$$

We take  $e^{-j\frac{\omega}{2}}$  common and we have  $e^{j\frac{\omega}{2}} - e^{-j\frac{\omega}{2}}$  and once again, one can recognise this is essentially  $2j \sin \frac{\omega}{2}$ .

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The image shows a handwritten derivation on a slide titled "WAVELETS AND MULTIRATE DIGITAL SIGNAL PROCESSING" by "C-DEEP IIT BOMBAY". It continues from the previous slide, showing the expression  $j \cdot e^{-j\frac{\omega}{2}} \sin \frac{\omega}{2}$ . Below this, it states "Magnitude response" and then shows the magnitude of the expression:  $| \cdot |$  of this  $= \left| \sin \frac{\omega}{2} \right|$ .

$$= j \cdot e^{-j\frac{\omega}{2}} \sin \frac{\omega}{2}$$

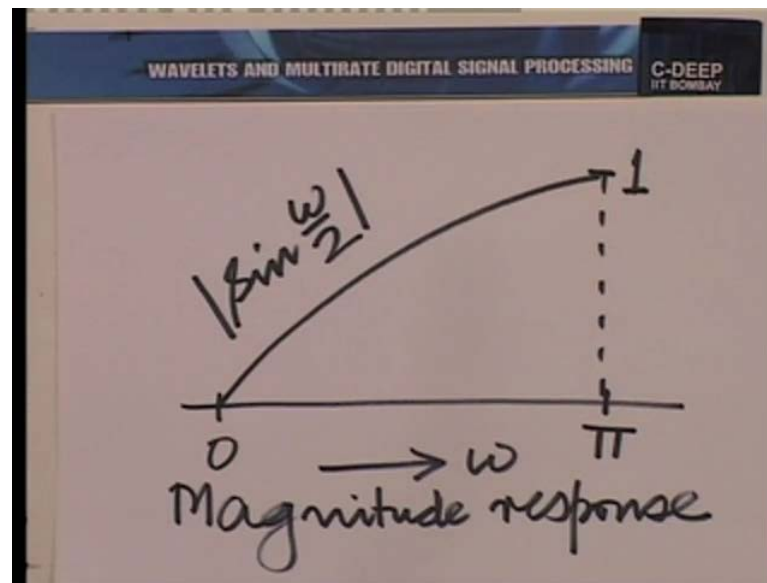
Magnitude response

$$| \cdot | \text{ of this } = \left| \sin \frac{\omega}{2} \right|$$

So, now I can simplify this putting it all together. Once again, I look at the magnitude response first. The magnitude response is a magnitude of this and that is easily seen to be  $\sin \frac{\omega}{2}$ .

Let us sketch the magnitude response as a function of  $\omega$ .

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Again, we will sketch it only between 0 and  $\pi$  for the reasons that I have just explained. So, it will have an appearance something like this. This is going to be 1 here, this is  $\sin \omega$  by 2. Now, for the phase response, now please remember last time we had a convenient situation.

We had two terms. One of them contributed, no phase the other one contributed the phase. So, we were comfortably put. This time we have to be little careful.

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WAVELETS AND MULTIRATE DIGITAL SIGNAL PROCESSING C-DEEP IIT BOMBAY

$\omega: 0 \rightarrow \pi$

$j \cdot e^{-j\frac{\omega}{2}} \cdot \sin \frac{\omega}{2}$

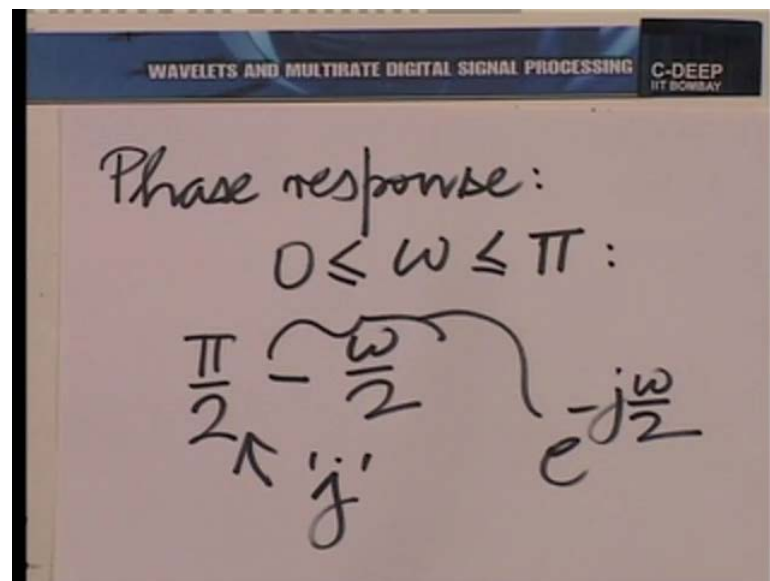
$\sin \frac{\omega}{2} \geq 0$  : no phase contribution



So, you know let us make life easy by first looking only 0 to  $\pi$ . Remember, we are going to have conjugate symmetry. So, let us consider  $\omega$  from 0 to  $\pi$  and let us look at the frequency response expression  $j e^{j\omega/2} \sin(\omega/2)$ .  $\sin(\omega/2)$  is non-negative. So, no phase contribution here.

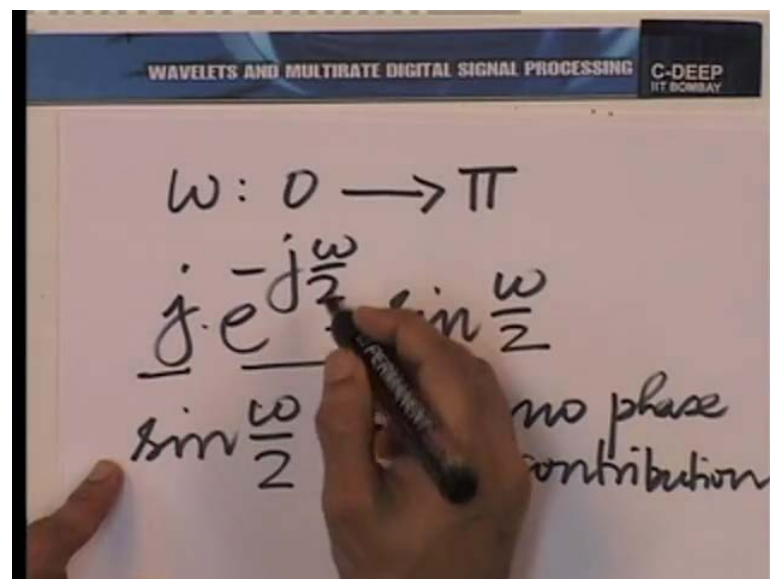
However, both of this term and this term have a phase contribution. In fact, the phase contribution is 90 degrees or  $\pi/2$  from here and  $-\omega/2$  from here.

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Phase response:  
 $0 \leq \omega \leq \pi$ :

$\frac{\pi}{2} - \frac{\omega}{2}$   
 $\uparrow$   $j$   $e^{-j\frac{\omega}{2}}$



$\omega: 0 \rightarrow \pi$

$j e^{-j\frac{\omega}{2}} \sin \frac{\omega}{2}$

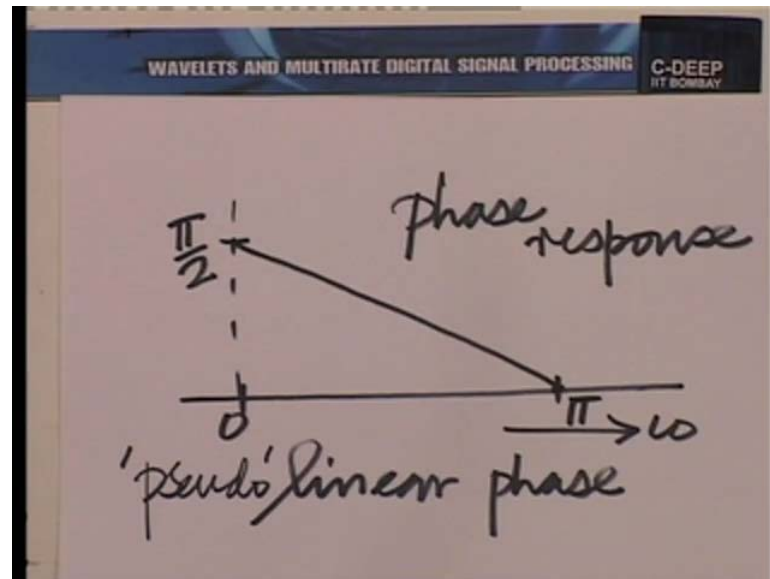
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$\sin \frac{\omega}{2}$  no phase contribution

So, over all the phase contribution or the phase response is I mean only between 0 and  $\pi$ ,  $\pi$  by 2 minus  $\omega$  by 2. This is contributing essentially  $j$  in the expression and this part is coming from  $e$  raise the power minus  $j \omega$  by 2 in the expression.

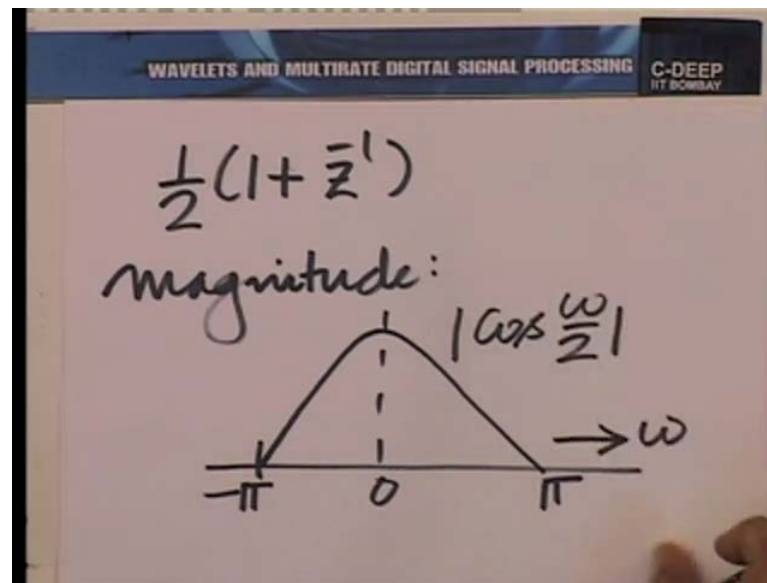
Let us sketch this response, I mean the phase response.

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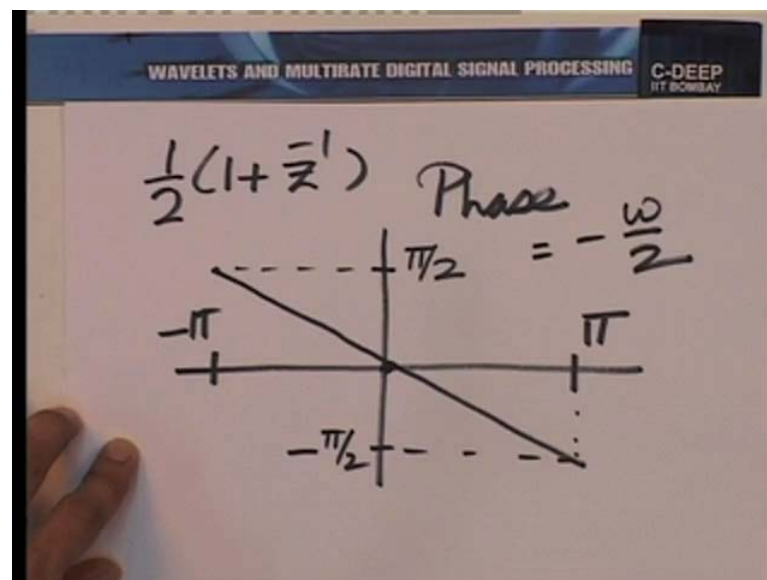
So, of course at  $\omega$  equal to 0, it is going to be  $\pi$  by 2 and at  $\omega$  equal to  $\pi$ , it is going to be 0. This is a situation. Now, once again we have a linear phase well almost not quite linear. If it was strictly linear phase, this would have been a straight line indeed but the straight line passing through the origin. So, it is not really linear phase, it is called pseudo linear phase. Seemingly linear phase. In fact, for completeness, let us draw the magnitude and the phase response all the way from minus  $\pi$  to  $\pi$  for both of these filters now for the sake of completeness.

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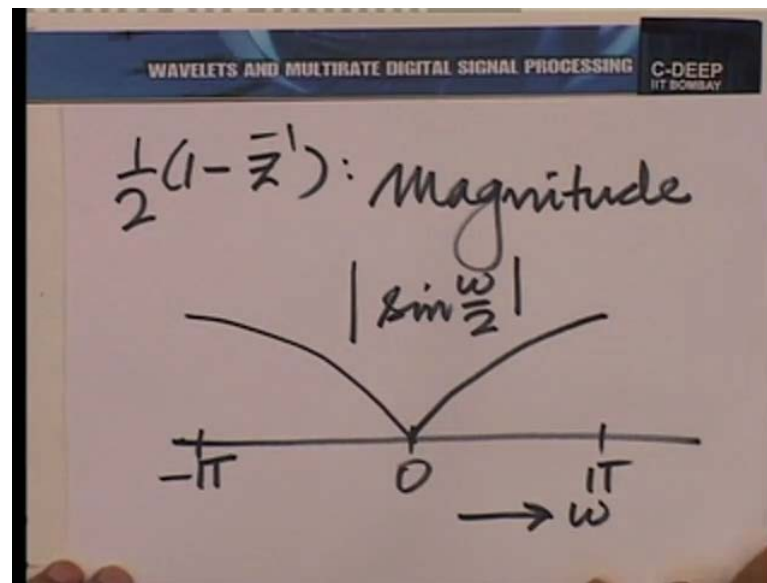
So, the situation is for the filter half 1 plus Z inverse. The overall magnitude response should look like this between minus pi and pi, I mean essentially, mod cos omega by 2 and the phase.

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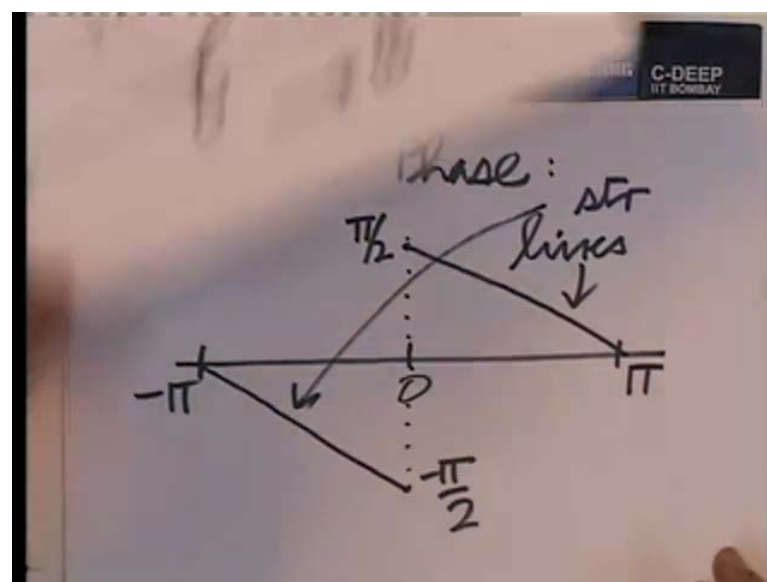
This starts at plus pi by 2 here and goes up to minus pi by 2 there, passes through the origin of course, the straight line.

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For the second filter, the overall magnitude response looks like this. Essentially, a sine mod sine omega by 2 and the phase response looks like this. Starts at pi by 2 there and goes to 0. It is a straight line segment, here it would start now. That is interesting.

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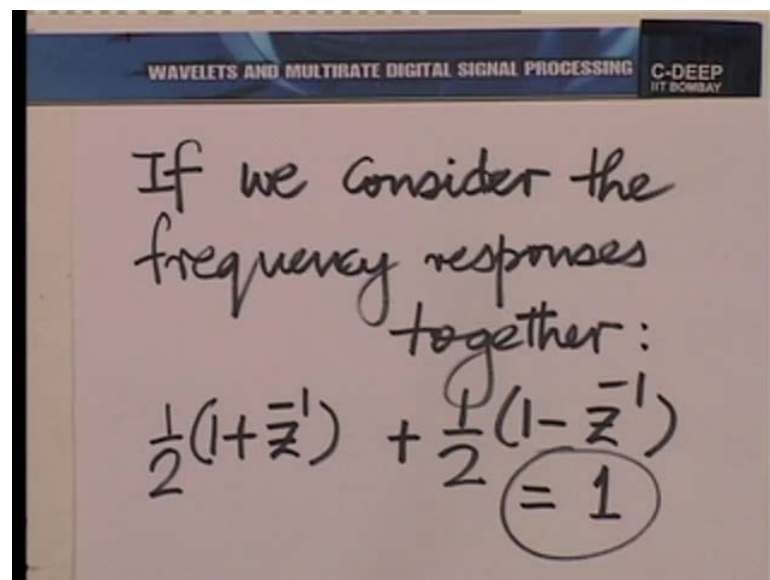


You know the phase on this side between minus pi and 0 needs to be negative of the phase between 0 and pi. So, it will be a mirror image. These are lines, straight lines. So, we call this pseudo linear phase. Now, one point needs to be understood. There is a peculiar situation at the point omega equal to 0 here.

The phase is both  $\pi/2$  and  $-\pi/2$ . How can this be possible? Well, the answer comes from the magnitude response. The magnitude response at that point  $\omega = 0$  is 0. When the magnitude response is 0 at a point, the phase response has no meaning. The phase response could be anything you see, it means that sine wave at  $\omega = 0$  is any way being destroyed.

So, what consequence is the phase response that is why there is an ambiguity in phase or a discontinuity in phase at a point  $\omega = 0$  in this phase response. A small detail but important when we try to understand this filter bank completely. Anyway, coming back to these magnitude responses now.

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WAVELETS AND MULTIRATE DIGITAL SIGNAL PROCESSING C-DEEP IIT BOMBAY

If we consider the frequency responses together:

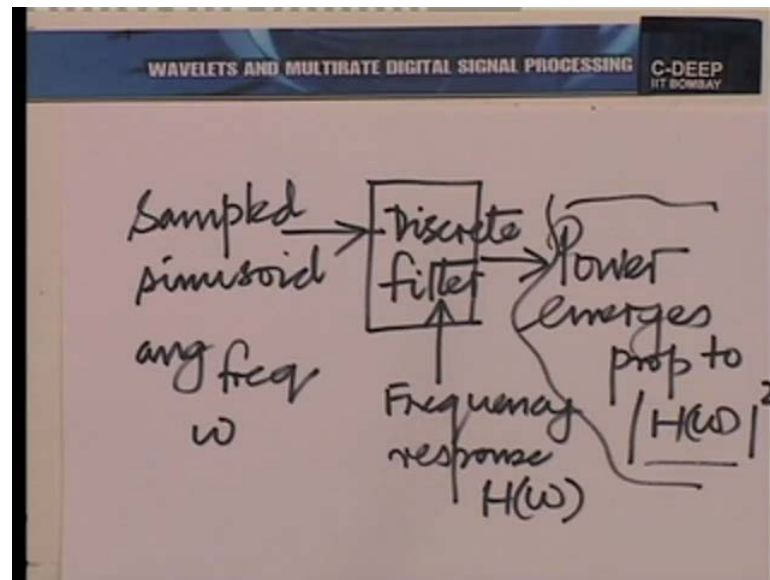
$$\frac{1}{2}(1 + \bar{z}^{-1}) + \frac{1}{2}(1 - \bar{z}^{-1}) = 1$$

If we consider the 2 magnitude responses together, in fact let us first consider the frequency responses together, both magnitude and the phase. A very interesting property emerges. You see suppose we add them, so suppose you take you know I do not even need to substitute  $Z$  equal to  $e^{j\omega}$  rise the power  $j\omega$ , let me keep it as it is. So, half into  $1 + Z^{-1}$  plus half into  $1 - Z^{-1}$ . It is very easy to see. It is equal to 1, a very interesting consequence.

What does it physically mean? It physically means that if I were to send a sample sine wave of frequency  $\omega$  into one of these filters and then the other and if I took these to sample sine wave from the two filters and put them together by adding, it would get back the original sine wave.

So, sine wave at frequency  $\omega$  is split by the two filters in such a way that the parts can simply come together and reconstruct the sine wave as it is. Now, let us look at something more interesting. What can we say about the power? So, recall that if you give a sample sine wave, a sample sinusoid to a discrete time filter.

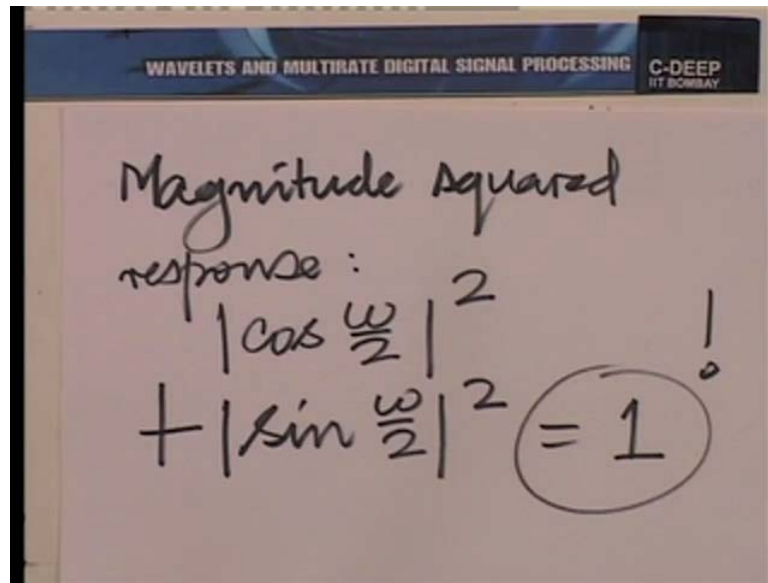
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Let us say the angular frequency is  $\omega$  and the frequency response here is  $H$  of  $\omega$ . Then the power that emerges from here is proportional to mod  $H$   $\omega$  squared. So, in other words, whatever is the power of a sample sinusoid with angular frequency equal to  $\omega$  here, is multiplied by mod  $h$   $\omega$  square where it emerges at the output.

So, the squared magnitude of a frequency response is indicative of the change in power of the sine wave when it goes to that discrete time signal. What can we say about the power change of a sine wave when it goes through either of these two filters. Here, let us see. That means in another words we are asking a question.

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WAVELETS AND MULTIRATE DIGITAL SIGNAL PROCESSING C-DEEP IIT BOMBAY

Magnitude Squared  
response :  
 $| \cos \frac{\omega}{2} |^2$   
 $+ | \sin \frac{\omega}{2} |^2 = 1$

What is the magnitude squared response?

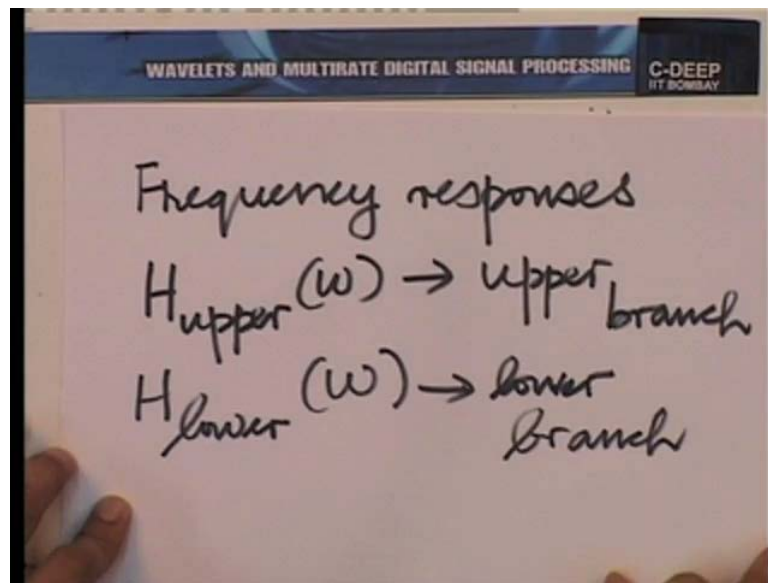
In the first one, it is mod cos omega by 2 the whole squared and in the second one, it is mod sine omega by 2 the whole squared and low in the whole when you add these, you get 1 as well. That is a very interesting observation. Not only does it happen that when you add the two responses together, you know you literally took 1 plus Z inverse by 2 and 1 minus the Z inverse by 2, the actual frequency responses irrespective of Z.

In fact, I said there you do not even need to substitute Z equal to e raise the power j omega. You just added the system functions together and you got 1.

So, if you put a sine wave of frequency omega, I mean a sample sinusoid of frequency angular frequency omega and look at the corresponding emerging sine wave on the top branch and the lower branch and just added them together, you get back the original sine wave. Not only that, what we have just shown is that when you multiply, if you look at the power emerging from the upper branch and power emerging from the lower branch, the powers also add. So, in fact, you have two kinds of complementarity in the filters. This is something very interesting here.

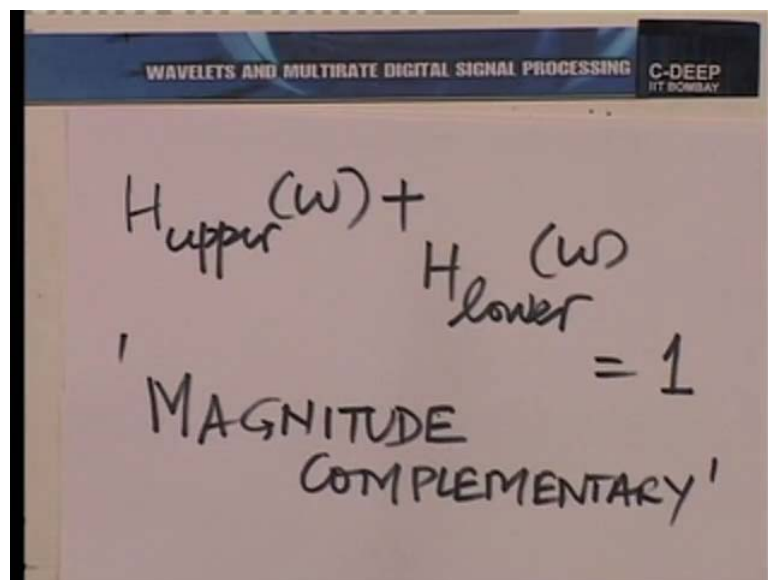


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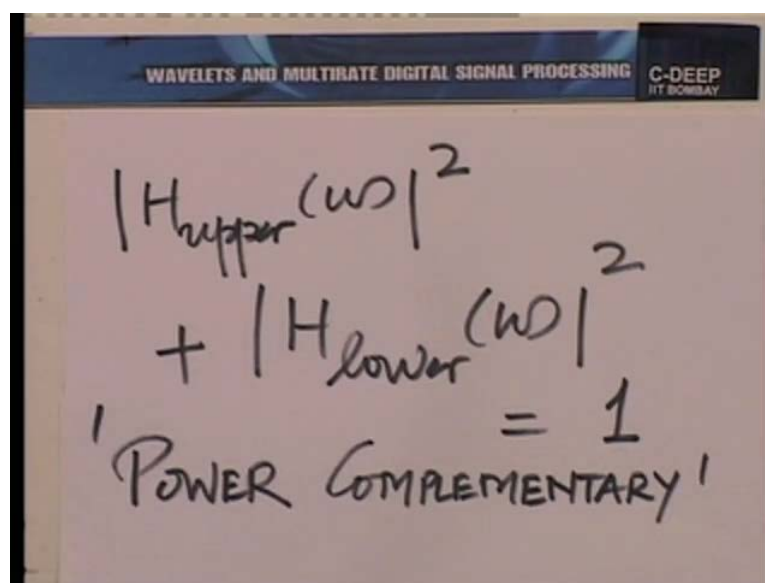
So, if you call the frequency responses of the upper branch and lower branch, respectively as  $H_{\text{upper}}(\omega)$  and  $H_{\text{lower}}(\omega)$ . Upper branch, lower branch. Then two properties are immediately satisfied.

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$H_{\text{upper}}(\omega) + H_{\text{lower}}(\omega)$  is equal to 1. This is called magnitude complementary property and in addition,  $|H_{\text{upper}}(\omega)|^2 + |H_{\text{lower}}(\omega)|^2$  is identically equal to 1. This is called the power complementary property.

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$$|H_{upper}(w)|^2 + |H_{lower}(w)|^2 = 1$$

'POWER COMPLEMENTARY'

A very interesting result, the Haar analysis filter bank is both magnitude complementary and power complementary. In fact, I leave it to you to study the synthesis filter bank and come to a similar conclusion. The filters are magnitude complementary and power complementary.

Whatever it be, this is something striking. Now, you see what I mean when I said the filters have individual properties and collective properties. Magnitude complementarity and power complementarity are collective properties. The low pass and the high pass nature if you recall, the second filter that we had was high pass because we emphasise the higher frequencies and de-emphasise the lower frequencies.

So, low pass and high pass properties are individual properties. The magnitude and the power complementary properties are collective properties. So, we have filters with individual and collective properties forming two filter banks, the analysis filter bank and the synthesis filter bank. Now, you know the idea of a filter bank is very deeply entrenched in multi-resolution analysis. In subsequent lectures we shall study this connection even further.

So, for today we shall conclude the lecture here by noting that we have already established even more deeply the frequency domain behavior of the filter bank that we brought out in the previous lecture. Thank you.