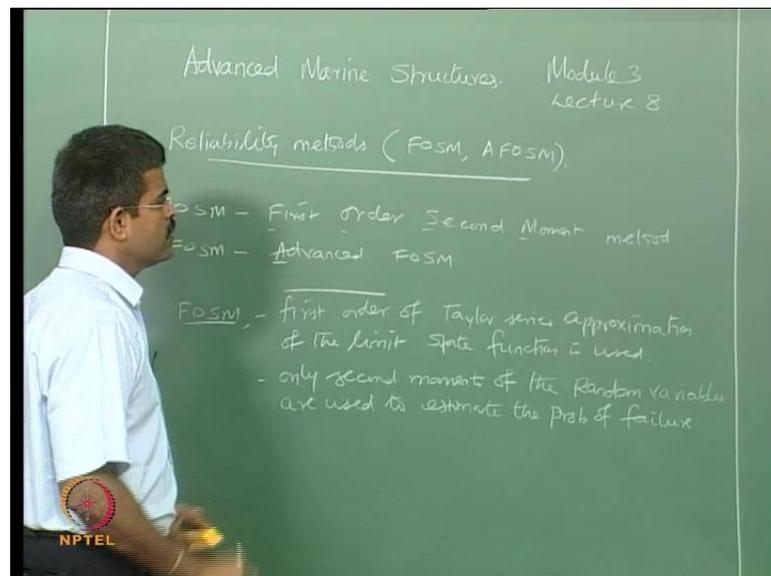


Advanced Marine Structures
Prof. Dr. Srinivasan Chandrasekaran
Department of Ocean Engineering
Indian Institute of Technology, Madras

Lecture - 8
FOSM and AFOSM Methods of Reliability

So, in the last lecture we have seen what are the different factors, like a statistician, probabilistic engineer or probability engineer, then reliability engineer and a marine engineer who all jointly play a role to estimate the reliability or formation of reliability problem in a given space.

(Refer Slide Time: 00:48)



Now, let us quickly see there are two important methods by which reliability studies can be carried out easily for a linear limit state function, for a non-linear limit state function, which we call as FOSM and AFOSM. FOSM stands for first order second moment method; AFOSM stands for advanced first order second moment method. Then first order second moment method, first order of Taylor series expansion or I should say Taylor series approximation not expansion of the limit state function is used, that is why it is called first order.

So, you approximately formulate the limit state function in Taylor series, and in that series you can construct only the first order terms and if you do that, then that method of

reliability is generally called as FOSM. Further, only the second moments of the random variables are used to estimate the probability of failure.

(Refer Slide Time: 03:21)

Limit state function G defined as:

$$M = R - S \quad \text{--- (1)}$$

- Where R, S are statistically independent
- They are also assumed to be normally distributed

$$\left. \begin{aligned} \mu_M &= \mu_R - \mu_S \\ \sigma_M &= \sigma_R^2 + \sigma_S^2 \end{aligned} \right\} \text{--- (2)}$$

$$P_f = P(M < 0)$$

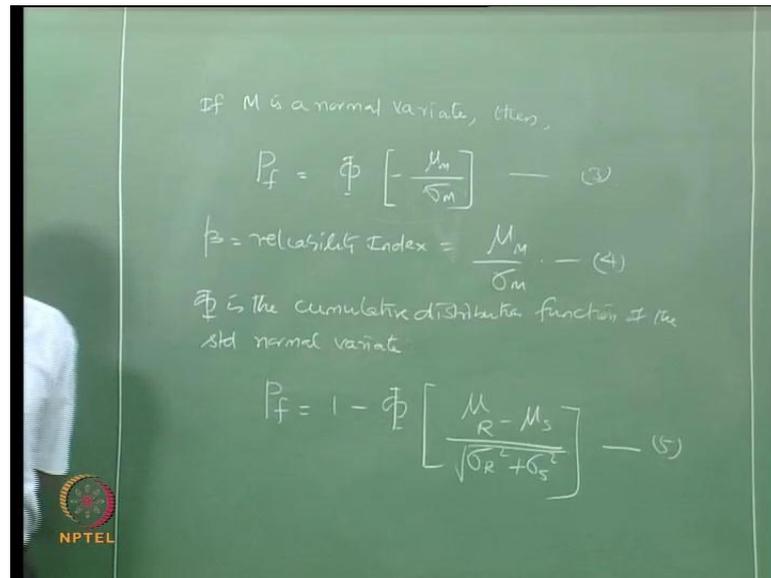
$$= P[(R - S) < 0]$$

 NPTEL

Let us say the limit state function is defined as M is equal to R minus S , M is a margin of safety where R and S are statistically independent. They are also assumed to be normally distributed. So, one can say μ_M and σ_M as μ_R minus μ_S and σ_R^2 plus σ_S^2 . I call this equation two.

Therefore, probability of failure is M less than 0, that is, R is lesser than S . What is the probability of M less than 0, which can otherwise, you say probability of R minus S less than 0.

(Refer Slide Time: 05:46)



If M is a normal variate, because R and S are normally distributed, then we already know this probability of failure is simply given by phi of minus mu M by sigma M, equation number 3, where the reliability index beta is nothing but mu M by sigma M. And phi in this case is the cumulative distribution function of the standard normal variate.

I can substitute from mu and sigma M, as we saw from the equation number 2. Its probability of failure can be 1 minus phi of mu R minus mu S by sigma R square plus sigma S square. Phi of any function can be 1 minus phi of this. This, of course, is root. Equation number what, say I call this as 4, this as 5.

(Refer Slide Time: 08:25)

If R & S are log-normal,

$$\sqrt{P_f} = 1 - \Phi \left[\frac{\ln \left(\frac{\mu_R}{\mu_S} \right) \sqrt{\frac{1+V_S^2}{1+V_R^2}}}{\sqrt{\ln(1+V_R^2)(1+V_S^2)}} \right] \quad (6)$$

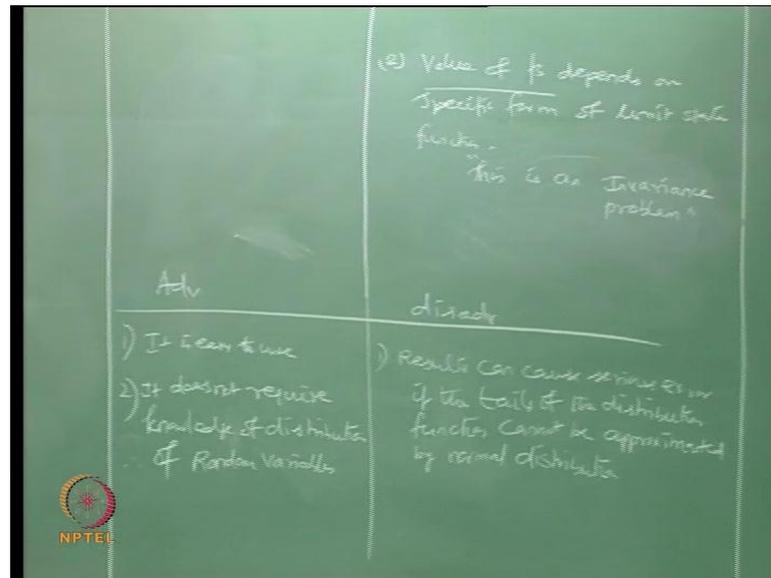
Adv	disadv
1) It is easy to use 2) It does not require knowledge of distribution of Random Variables	1) Results can cause serious error if the tails of the distribution



If R and S are log normal, we have already given in this equation, you can easily tell what is the probability of failure. We have already given in this, this 1 minus phi of, when they are log normal distributed, natural logarithm of mu () by mu s. 1 plus V R V S square (()), this is V S and V R. This is equation number 6. If they are log normal, be on this equation, if this is normal distributed we have this equation.

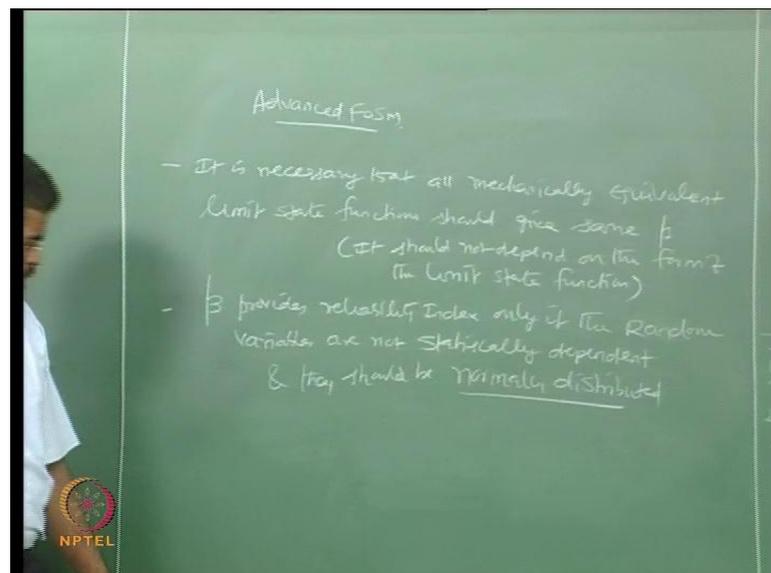
Now, FOSM method has some advantages and disadvantages. The advantages are the following. It is easy to use because you should know only the mean and standard deviation variance of R and S. You can find the probability of failure directly using these two expressions of 5 and 6, if they are normally distributed or log normal. So, it is easy to use. Most importantly, it does not require knowledge of distribution of random variables. Disadvantages are results can cause serious error if the tails of the distribution function cannot be approximated by normal distribution.

(Refer Slide Time: 12:19)



The second disadvantage could be value of reliability index depends on specific form of limit state function. As in this case you have seen that you have considered only first order approximation to illustrate this expansion, so depends upon specific form; that is very, very important. Why advanced FOSM was introduced? The value of reliability index depends only on the specific form of limit state function; that is very important, it is form dependent. This is what we call as an invariance problem.

(Refer Slide Time: 13:33)

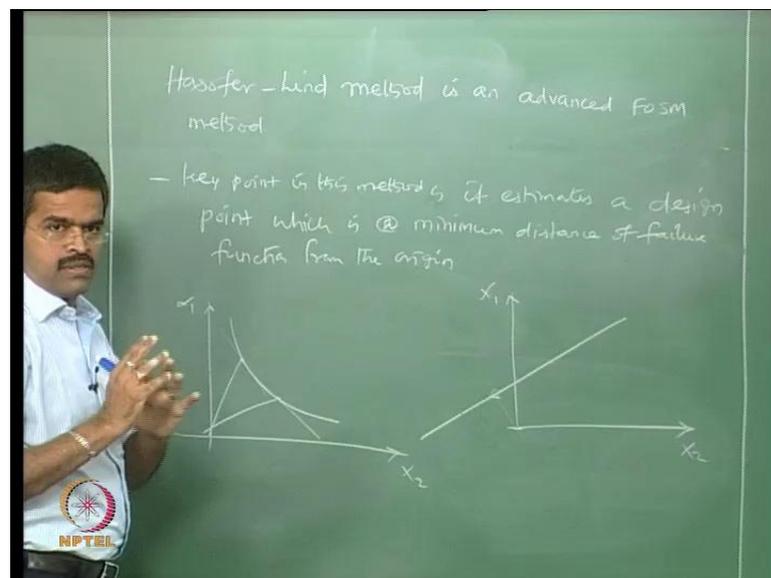


Let us talk about advanced FOSM. We all understand that it is necessary, that all mechanically equivalent limit state functions should give same beta reliability index. On the other hand, it should not depend on the form of the limit state function.

Now, we all know, that beta provides reliability index only if the random variables are not statistically dependent, that is, if they are independent, then beta gives the reliability value and they should be normally distributed. That is why we said, calculating reliability index using FOSM does not require any knowledge of distribution of random variable; it is understood, that random variables are normally distributed.

If these two conditions are violated, then how to estimate reliability function or the reliability index beta, that is the question. So, that is addressed in advanced FOSM. Hasofer-Lind has given a method or algorithm based on which the reliability index can be computed.

(Refer Slide Time: 16:20)



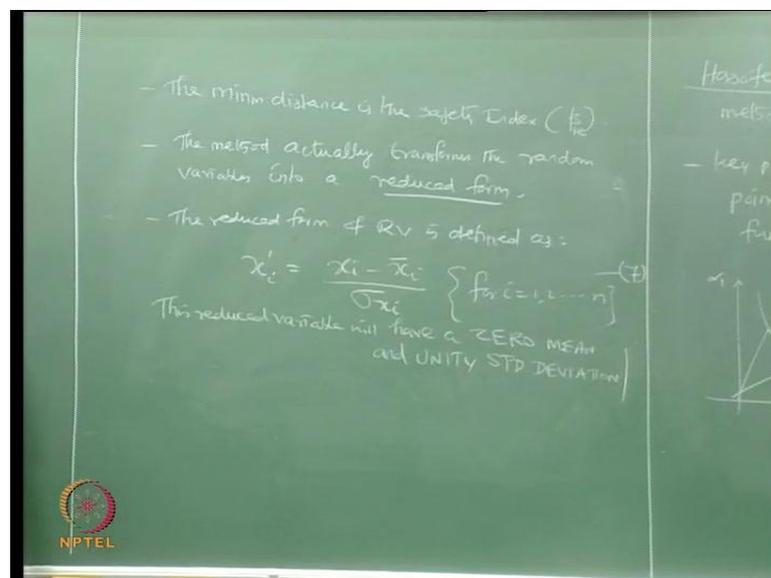
Hasofer-Lind method is an advanced FOSM method, which we will discuss. There are some limitations to this method also, we will also discuss them. Now, the key point in this method is, it estimates a design point, which is at minimum distance of failure function from the origin. I will come to that.

Let us say, I have two variables, x_2 and x_1 , I have a linear failure function; it is a linear failure function. To this linear failure function, I must find a point on this failure function, so that the point remains at a minimum distance from origin. So, obviously, I have to draw a perpendicular and this becomes my point and this becomes my minimum distance, I call this as a design point.

Now, if the function is linear you can easily find this. If the function is non-linear for example, then if you take a point here and draw a tangent and say, this is my minimum point. If you take a tangent here, you will say this is my minimum point. So, beta keeps on varying, is it clear.

So, if the function is linear or non-linear between variables x_1 and x_2 , how to handle this? So, the whole key issue in Hassofer-Lind method is to estimate a design point, which is located on the failure envelop or the function, which is minimum distance from the origin. Now, one may ask why it should be a minimum distance, why not maximum? I will answer this question.

(Refer Slide Time: 19:53)



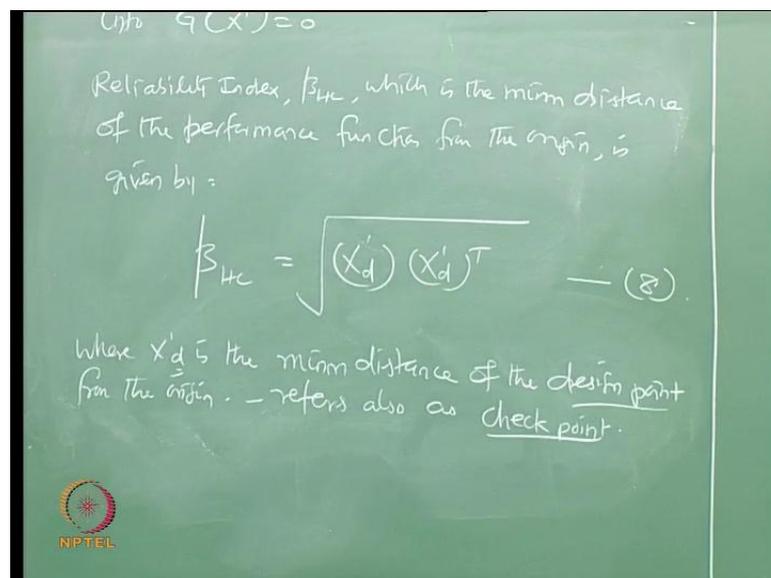
Hassofer-Lind method says, the minimum distance is the safety index directly in this geometric meaning. So, the minimum distance, if it is estimated geometrically, that itself is the safety index or beta. To be very specific, we write beta HL, HL stands for Hassofer-Lind. Now, the method is very simple, the method actually transforms the random variables into a reduced form. I will come to that, what is reduced form? The reduced form

of random variable is defined as x -th value, which can be $\bar{x} \pm \sigma x$ if σ equals, let me call this equation number, what is the number?

Student: 7sir.

7, see instead of using directly the random variable, which are R and S , I am going to use a modified, a reduced form of the random variable x dash, where x dash will be value given by this expression 7. Now, the interesting part is this reduced form or this reduced.

(Refer Slide Time: 23:10)



Now, the performance function G of X_0 is now converted into G of X dash equals 0. I am now transforming the variable from x to x dash. Reliability index, which is β_{HL} , which is the minimum distance of the performance function from the origin, is given by... Where x dash is a minimum distance of the design point from the origin. So, d stands for the design point. Some literature refers this also as check point, so design point or check point.

(Refer Slide Time: 25:45)

The reduced values are

$$R' = \frac{R - \mu_R}{\sigma_R} \quad (10)$$

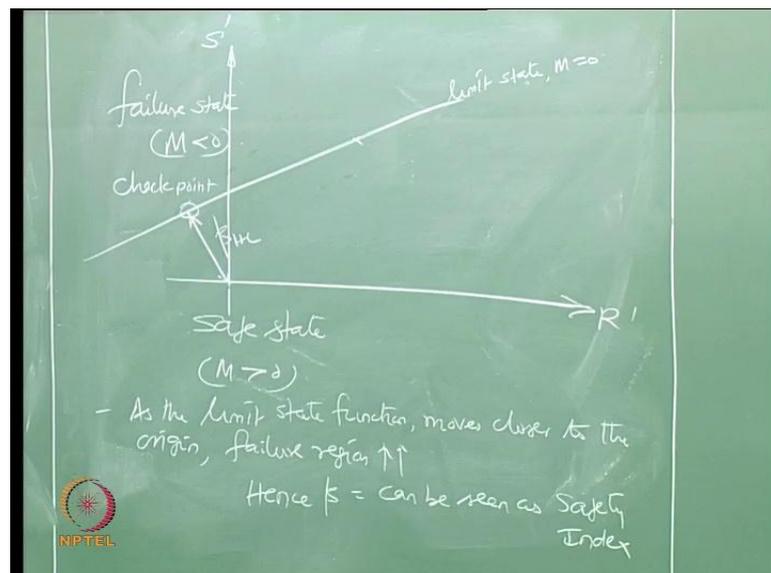
$$S' = \frac{S - \mu_S}{\sigma_S}$$

Substituting (10) in (9),

$$M = (\sigma_R R' + \mu_R) - (\sigma_S S' + \mu_S) \quad (11)$$


Now, let us take two cases. Case 1, when the limit state function is linear, we will see how to handle this. So, let us consider $M = R - S$, which is equal to 0. The reduced values are R' and S' , which are $R - \mu_R$ by σ_R , which is $S - \mu_S$ by σ_S , equation 10. So, I must substitute R and S here. I have R and S here, rearrange this term, I can rewrite M . Now, substituting 10 in 9, M can be rewritten as $\sigma_R R' + \mu_R - \sigma_S S' - \mu_S$; call the equation number 11.

(Refer Slide Time: 27:57)

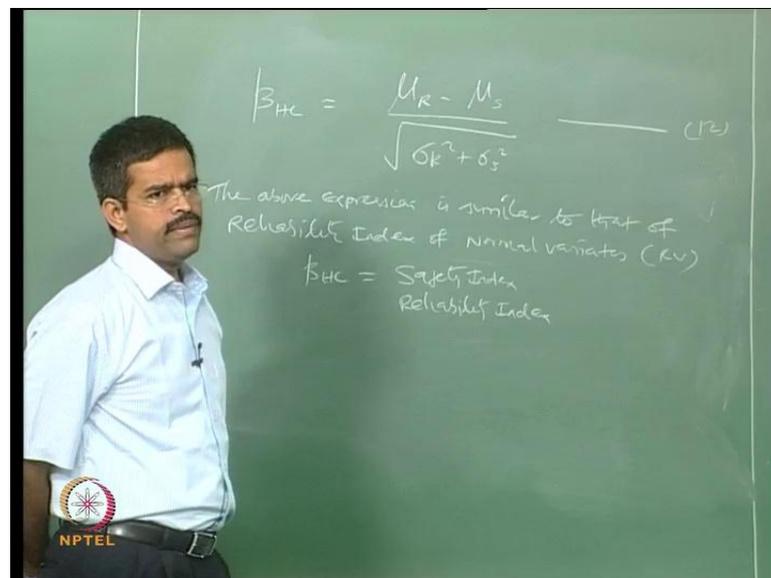


So, in limit state function they look like this, which can be R dash and S dash. It is a straight line, it is a straight line, R minus S , this will limit state M is equal to 0. This is my β_{HL} and this becomes my check point and this is my failure state, where M less than 0 and this is my safe state, where M greater than 0. We can see here, for all values here, for all values, for example, this point we can see, the slope is gentle, is mean, R is greater than S , safe state, whereas in this case, given to be failure state.

Now, you can see from this figure, as the limit state function moves closer to the origin, what will happen when this moves, line keeps on moving closed to the origin? The failure state will be kept on increasing, the failure state or I should say, the failure region keeps on increasing. So, there is a level at which the failure state is optimized and that is controlled by the minimum distance from the origin. Hence, β can be seen as safety index. That is the reason why, the minimum distance is considered as reliability index in Hasofer-Lind technique. Is this clear?

Now, let us move to the...

(Refer Slide Time: 30:51)

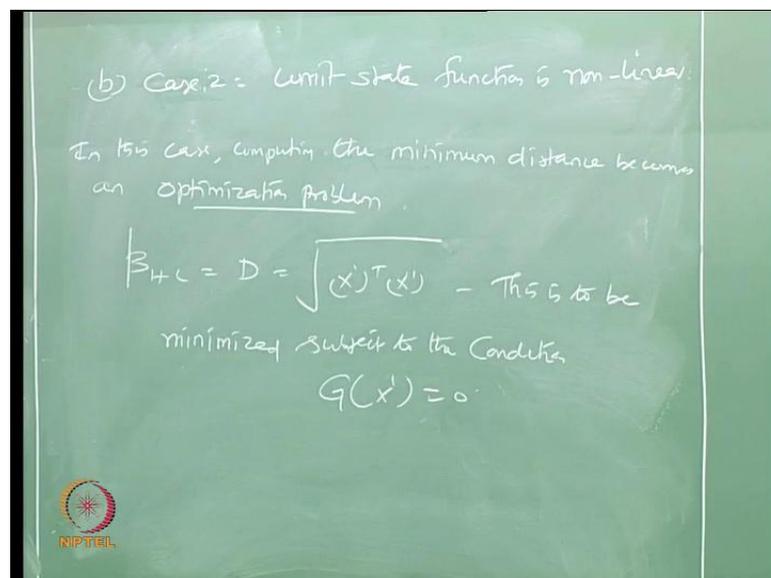


So, in my case, β_{HL} , β_{HL} can be simply μ_R minus μ_S by σ_R square plus σ_S square. What is the equation number? 12, you will see, that this expression is same even in the case of normal variates, is it not? Expression is same, the above expression is similar to that of reliability index of normal variates, random variates, is it not? That is why, β_{HL} is also called safety index or accepted reliability index. Remember, β_{HL}

equation has been derived using the geometric calculation from this figure, is not from the formula.

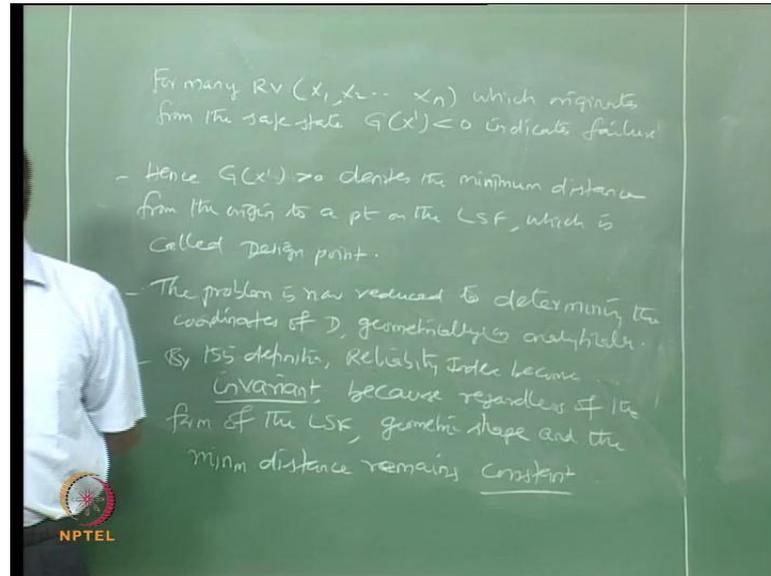
It is a very simple issue, that I want to find the minimum distance between the line from the origin 2-D geometry problem, you can easily find this. I have not shown the mathematical working out of finding on beta, as on geometrically I will get this equation, but this equation is fortunately same as that you have for the normal variates. Therefore, I can call this minimum distance as reliability index; that is the definition why Hasofer-Lind index is called as a safety index. Now, when the limit state function is non-linear, now it is linear, it is a straight line, when it is non-linear what happens?

(Refer Slide Time: 33:12)



In this case, computing a minimum distance becomes an optimization problem. So, what you are going to do is, beta HL is nothing but a distance, which is given by x dash transpose x dash, we have got to minimize this, subject to the condition G of X dash is said to 0.

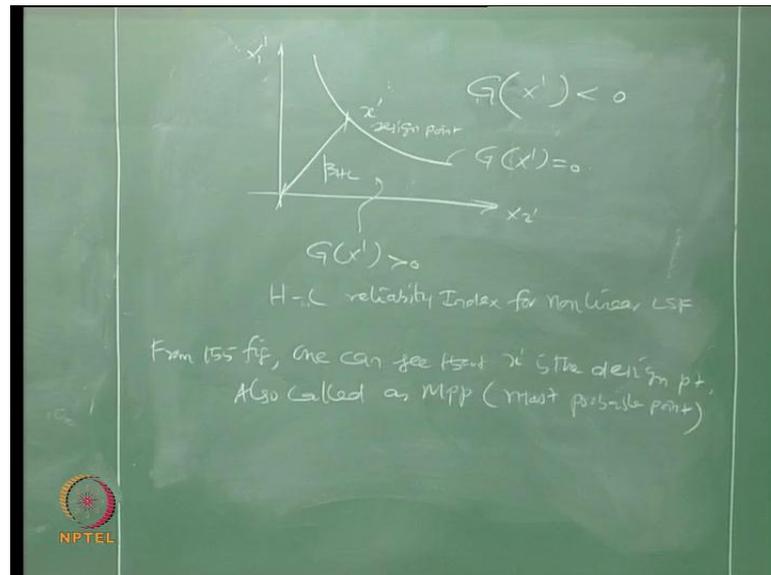
(Refer Slide Time: 35:18)



For many random variables, x_1, x_2, \dots, x_n , which originates from the safe state G of X less than 0 indicates failure. Therefore, G of x greater than 0 denotes the minimum distance from the origin to a point on the limit state function, which is called design point. So, the problem is reduced to determining the coordinates of D , design point, geometrically or analytically.

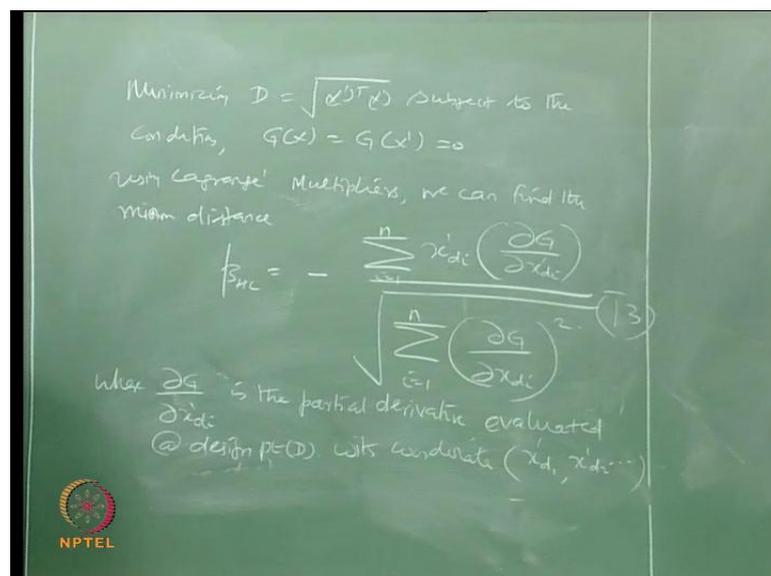
So, by this definition, reliability index becomes invariant because regardless of the form of the limit state function the geometric shape, geometric shape and the minimum distance remains constant. The one, which was a difficulty in FOSM is now handled by Hasofer-Lind by a different technique. Because now, by obtaining the coordinates of this point D for any form of the geometric shape of the limit state function, the minimum distance will remain constant, has to remain constant.

(Refer Slide Time: 39:08)



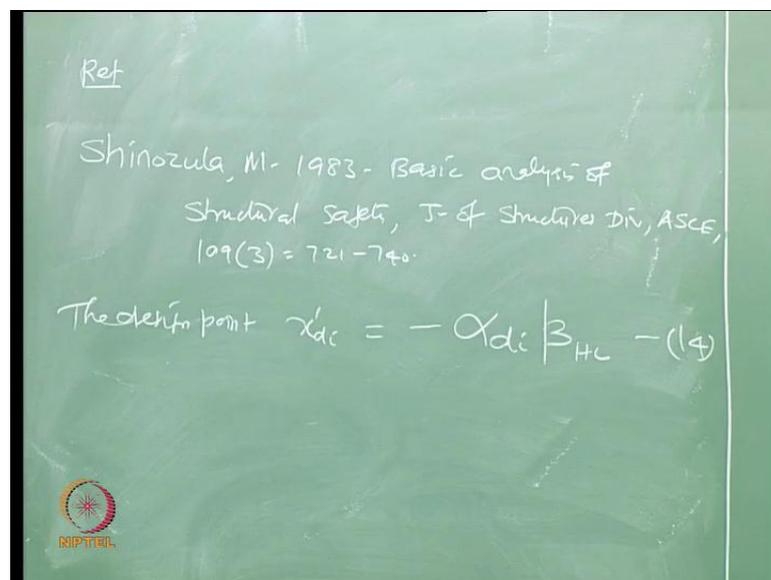
Let us say, the plot of these two variables, x_2 and x_1 for a non-linear limit state function looks like this. Let us say this is my design point, I call this point as x' . So, this is my design point and this is where G of x is less than 0 and this is the distance, what I call as beta HL and this is the function G of x is equal to 0. This is a function, there is an area where G of x is greater than 0. So, this is Hasofer-Lind reliability index for non-linear limit state function. So, from this figure one can see, that x' is the design point, also called as MPP, most probable point.

(Refer Slide Time: 41:23)



So, minimizing D , which is equal to square root of x dash and x , subject to the condition G of X , that is, G of x dash should, is equal to 0 because I am transforming the coordinates from x to x dash; that is what you are doing in advanced methods. Using Lagrange's multipliers we can find the minimum distance, β_{HL} , as minus of sum of α_{di} to n x dash d_i , d stands for the design point, i is a summation. Is what equation number is this? 13, where $\frac{\partial G}{\partial x}$ is the partial derivative. Why it is partial derivative? The values of x are no more independently evaluated at design point D with coordinates x dash d_1 , x dash d_2 , and soon. These are the coordinates of the design point.

(Refer Slide Time: 44:43)



So, the study has got a very interesting reference I want to give you the reference, Shinozuka, M-1983, Basic analysis of structural safety, journal of structures division ASCE, 109 (3), 721 to 740. The design point x dash d_i , because I am interested in only finding the design point, is simply given by minus α_{di} β_{HL} ; is equation number 14.

(Refer Slide Time: 48:28)

$$\alpha_{di} = \frac{\frac{\partial G}{\partial x_{di}}}{\sqrt{\sum_{i=1}^n \left(\frac{\partial G}{\partial x_{di}}\right)^2}} \quad (15)$$

which are direction cosines along the coordinate axes x_i

In the space of original variables, design point can be given by:

$$x_{di} = \mu_{xi} - \alpha_{di} \sigma_{xi} \beta_{HL} \quad (16)$$

Where α_{di} is $\frac{\partial G}{\partial x_{di}}$ divided by the root of the summation from 1 to n of $\left(\frac{\partial G}{\partial x_{di}}\right)^2$, equation number 15, which are direction cosines along the coordinate axis x_i . So, in the space of original variables, because x_{di} are all reduced form of variables, in the space of original variables, the design point can be given by x_{di} , is $\mu_{xi} - \alpha_{di} \sigma_{xi} \beta_{HL}$, that is the equation 16. Of course, this method has got few limitations and there are improvements suggested on this method, which we are not discussing in the scope of this lecture.

So, in this class, in this lecture we have seen two interesting cases, where I have picked up the first order second moment method of reliability analysis and showed you how to find out the safety index or reliability index for a given standard variate, which is normally distributed. But we have seen, that limitation for FOSM is, that it depends upon the form of the limit state function. If it is linear, it gives a different answer; if it is non-linear, it gives a different answer. But strictly speaking, it should not then advanced method of (()) suggested by Hasofer-Lind saying, that generalize this function in a different reduced form, which has got unit standard deviation and 0 mean process and find out the coordinates of the so-called design point or the check point or maximum probability point on the limit surface.

So, this becomes an optimization problem, you have got to minimize the distance d with respect to the failure function, as we have discussed in the case. So, as the process goes

ahead we can easily find the design point coordinate using this expression where β_{HL} will give.

So, this process, it is an iterative process. Initially, you have got to assume, that the reduced form of variables are all standard variable as mean, as standard deviation, find out from equation 15, or in our case, equation 14. The new β_{HL} or you will find the x_{di} in terms of β_{HL} . Then substitute back in the original equation of β_{HL} to find out the value of β_{HL} , substitute again back in equation 14, keep on getting new x_{di} . So, you will ultimately get the coordinate of the design point, which does not vary between the first approximation of the standard variate to the actual real random variables, which are depended on each other. So, the corresponding β_{HL} will give you the safety index of the problem.

So, there are good illustrations and examples available in the literature. Unfortunately, in this lecture I am not able to show you some examples of the workout problems. If time permits, we will see an appendix later in the end of this course, but still as a part of this particular module we are introducing reliability in this scheme of advance marine structures. We have discussed that in length.

So, I wish, that you have understood the fundamental concepts of reliability as applied to marine structures, what are the limitations. what are the different levels, what are uncertainties, where are they formed and how are they responsible, how are they interdependent, how do they control the whole design process, why reliability cannot be accurate, how reliability can be a design scheme, what are the limitations, what are the fields of application, what are the players involved in reliability methodology and what is AFOSM and FOSM, that is the focus of this whole module, which we discussed.

And if you have any questions, you can always address me to NPTEL, IIT Madras, under this scheme. I hope you will go through this lecture once again and try to understand. Of course, there is an advanced course on reliability, especially handling on marine structures, which will come up in the next scheme of NPTEL. You can look for that course where we address only reliability problems and marine structures with classified site examples. So, we have finished three modules, now we have got one more module, which we will take up in the next class onwards, which will go in to address the (()) strength of marine structure members.

Thank you very much.