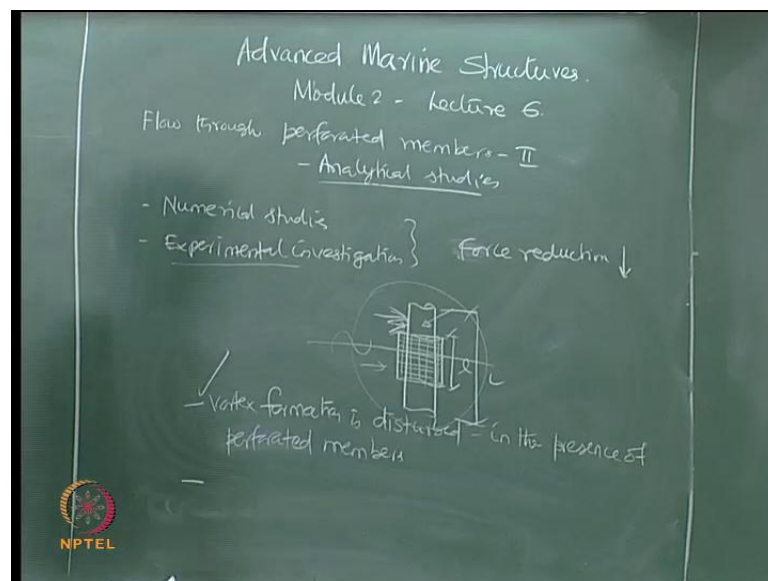


Advance Marine structures
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Lecture - 6
Flow through perforated
members-numerical studies – II

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So, we have been discussing about the flow induced vibration in the last lecture. So, we discussed about the numerical studies, and experimental investigations carried out on cylinders and application of this problem on tlp's, where we said that there has been phenomenal force reduction in the members when a cylinder which is solid is covered by a perforated layer or a perforated outer cover which as perforations or along the periphery when this covers in a cylinder is expected that under the action of waves, the forces on the inner cylinder is reduce tremendously. So, one can easily look at perforations are perforated covers as an effective method of reducing forces are retrofitting or rehabilitating, the existing structural members ,which are already weak because of many reasons like material deteriorations, stress concentration factors, etc.

So, we have shown you how experimental investigations can be conducted in a scaled module of a tlp as well as group of cylinders of different perforate an outer covers, and we evaluated this results with that of the numerical studies from using software by names star ccm plus. But, we already told you yesterday that there are some difficulties of not

able to trace the velocity potential variation along the depth of water, when you look at application of numerical studies in this case. Primarily, our interest is though it is force reduction, but we wanted to really understand and we have understood that whenever in outer cover which is poor us or perforated, the vortex formation is disturbed; the vortex formation is disturbed in the presence of perforated covers or perforated members.

So, this is one of the great advantages of application what we looking at which is recommended by researchers in the recent studies, that this can be one of the effective methods of reducing the vortex formation in a given member. In the present lecture, we will talk about how this problem can be handled using analytical formulation or mathematical modeling. For example, I want to write a program on my own or coding on the own to find out auto trace the velocity potential variation or water botanical kinematics essentially the velocity and acceleration variations along the depth, on the inner cylinder because the presents of outer cylinder. So, always we are focusing on what is happening to the inner cylinder when it is in compressed by an perforated cover, in the earlier example also we saw the same thing and in the present example also we will see the same thing.

So, it is very simple to understand basically why this kind of disturbance happen, when a solid cylinder is encountering waves, it results in flow separation and that results in vortex formation. When you have a cover which is having pours or holes the fluid is made to flow through the holes, therefore vortex formation is disturbed is a very simple physical phenomena.

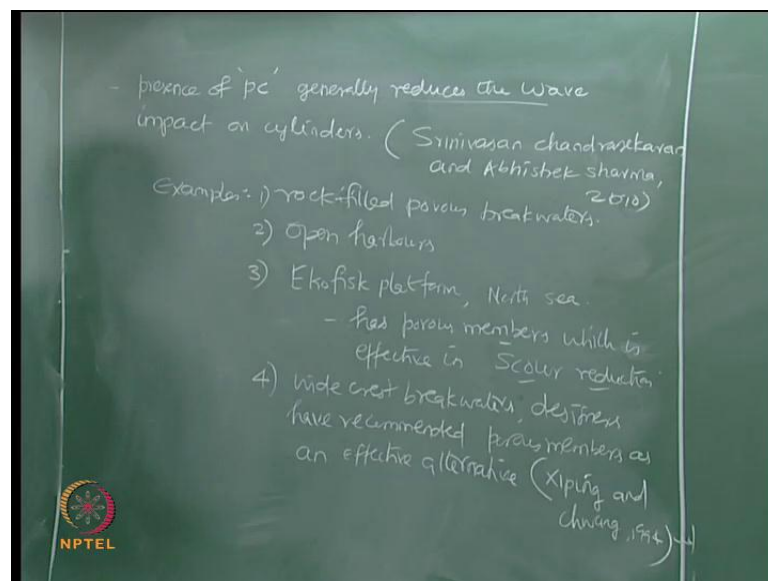
So, this is effective in two forms; one vortex formation is reduced and secondary vibrations cost by the fluid flow in the vicinity of the member or the structure is reduced significantly. The second advantage is when the member cannot take the intended load, because of it is material detraction age factor, stress concentration in the joints etc, can still provide strength in the member by providing an outer cover not over an entire link of the member, but on the regions where the stress concentration is maximum. It is expected that near that flash zone, you will always have the maximum forces accepted by the waves.

So, we can always try or attempt to put an preferred cover for a specific link which is going to be a function of the entire link of the member as parametric study, where I can

move this position of the perforation above, below, etc, and see which is going to be the optimum location of the perforated cover which can reduce by forces on the member. Now, let us look at this example again revisit this case analytically, and see can he do a mathematical formation on this problem, and can I derive the velocity potentials for this problem mathematically, that is what you have got you look at today's study. Do you have any questions on the previous lectures, where we have been talking about flow through perforated cylinders?

So, we discussed experimental investigation, we also discussed numerical studies, we have understood that per porosity or perforated cover can be one of the effective method and mean to reduce vortex formation is a designer prospective. Now, we look in to a hydrodynamic prospective of this using a mathematical model.

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It has been seen in the literature that I am using pc for perforated covers, where need not have to write total you can easily understand this, presents of perforated covers generally reduces the waves impact on cylinder. There are studies reported on this, which can be by Poppa and Abhishek Sharma 2010. You can add many examples of this application in reality, if you have attempted this idea in reality. For example, there are rock-filled porous breakwaters of a very large dimension where the breakwaters remain porous, and it has been estimated and seen that there is tremendous reduction in the wave impact on these breakwaters.

The second example can be, construction of what we understand as open harbors. These are very famous application examples where one can look at the presence of perforated cover or a porous structure as a mechanical means of reducing wave impact on members. We have another classical example of a gravity based structure which is an ecofisk platform, it is a gravity platform constructed in the North Sea. This gravity platform has porous members, which has been essentially used to reduce the movement. I say members they are structural members, porous members which is effective in cover reduction, because you understand in gravity based structure, because of the mask this cover on the seabed is a major problem.

So, that is essentially cost, because of the impact by the waves and current on the structure, and the providing porous members this effect was reduced significantly and people have shown that there has been reduction in the cover. For wide crest breakwaters, designers have recommended porous members as an effective alternative, this can be seen in studies conducted by Xiping and Chuang 1994.

So, there are many references available in the literature where people you have used effectively the presence of porous members are perforated cylinder or structures to reduce the wave impact on the members. But, they have been essentially applied on coastal structures; the coastal structure also part of marine structures not on any deep water large floating systems, that is not been applied, but people have used it for breakwaters, coastal protection structure people have applied, and they have seen that and there has been reduced impact.

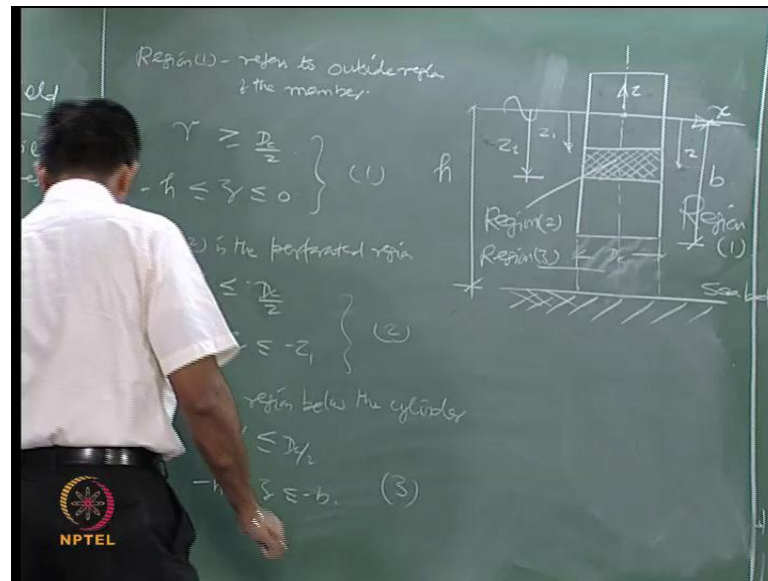
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Now, let us talk about the presence of floating structures in the flow field, because this was any attempt which is not available in the literature, very few mention about this applications available in this literature will discuss in this detail, because about the fixed platform like gravity based structures, people have conducted studies and you can find a lot of references on this and for breakwaters people have conducted studies, and you will find a lot of experimental as well as analytical studies available on this. From floating structures, this has been very scarce, so let us look at that and revisit this area, the movement of the floating structures or interfering with the flow field.

It causes alteration in the wave field by diffraction and radiation of waves from the structure. Now, interestingly this problem of equation formulation will have two solutions; one is the solution of the diffraction problem which yields the excitation forces on the structure, where the solution of radiation potential results in motion caused by the structure which produces acceleration, and velocity proportional forces. So, this problem has two kinds of solution; one is the diffraction potential solution, other is radiation potential solution. One yields me the excitation force, other yields me the acceleration in velocity proportional forces. Now, in these two components the acceleration proportional non-dimensional amplitude gives added mass values, and velocity proportional non-dimensional amplitude gives radiation damping.

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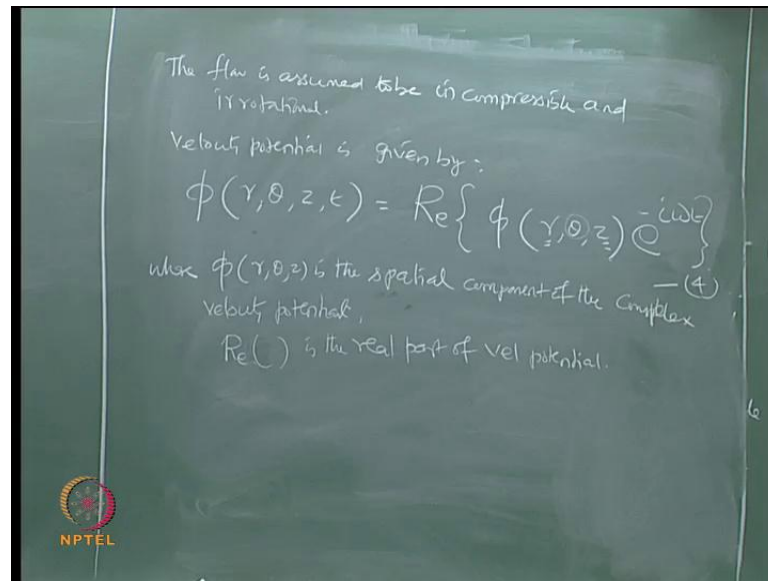


Now, let us take a system, this is my sea bed, this is my cylinder, this is my perforated region, this is my mean sea level and starts from here, and of course x is in the forward direction of the wave propagation. I call this distance water depth as h , I call the diameter of the member as D suffix c and I call this as z_1 , and this says z_2 , and any value here as a variable z . I divide this for mathematical modeling into three regions; there are three (()) I say region one, I say this is region two, and I say this is region three.

Let us explain these regions. Region one refers to the outside region of the member, so in this case r radius is greater than $D/2$, $D/2$ is the diameter of the member of the cylinders, c stands for the cylinder and z varying between minus h to 0 , is it not minus h to 0 , this is the region I call this equation number 1. Region two is my perforated region, where r is less than equal to $D/2$ and z varies between minus z_2 to minus z_1 , is it ok, this equation number two. Region three is a region below this cylinder that is this region where in this region also r is less than $D/2$, r is a radius. Let's call this value as b , depth of the cylinder.

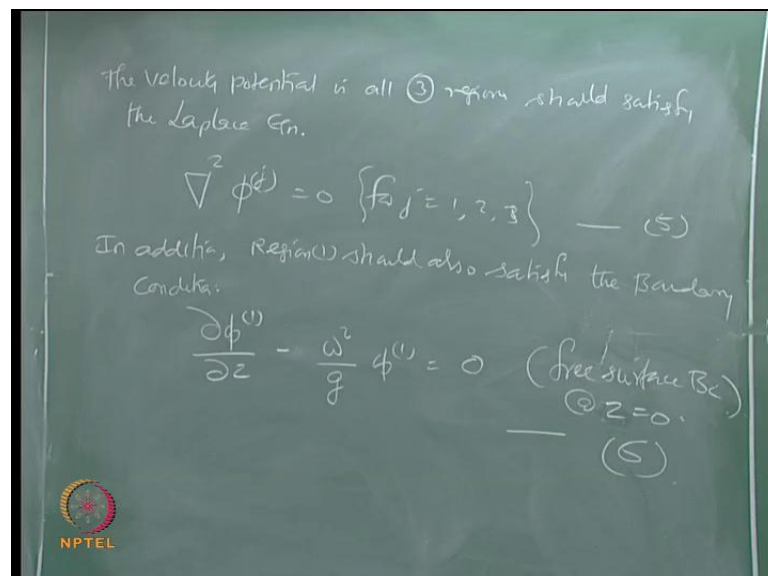
So, z varies between minus h to minus b is that ok, equation number three. So, we have divided this into three regions, and I am now I am going to derive the diffraction potential on the radiation potential in all these three regions independently.

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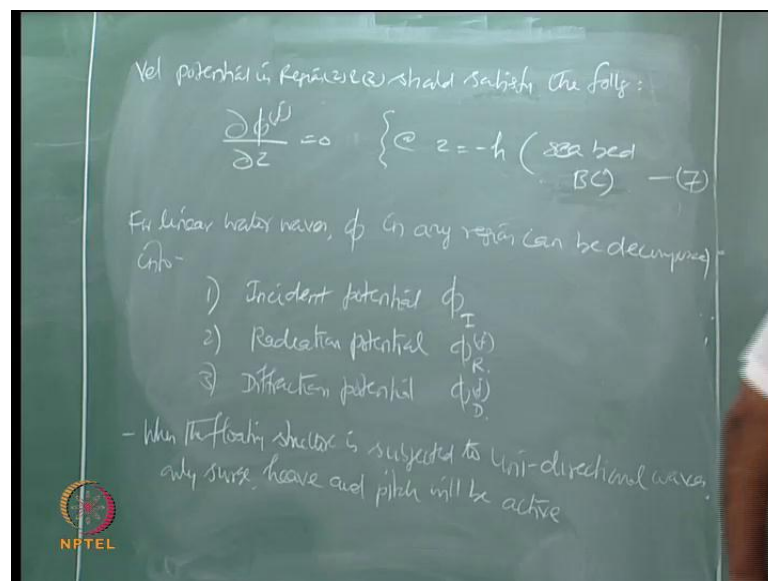
Now for this analysis, the flow is assumed to be incompressible and irrotational. Therefore, the velocity potential is given by equation number 4, where ϕ , r , θ , z is the spatial component, you can see here r is a radius, z is a position along the depth of water, and θ is the displacement deduction and ϕ is a special component of the complex velocity potential, because it is $i\omega t$ and Re of the argument is the real part of the velocity potential.

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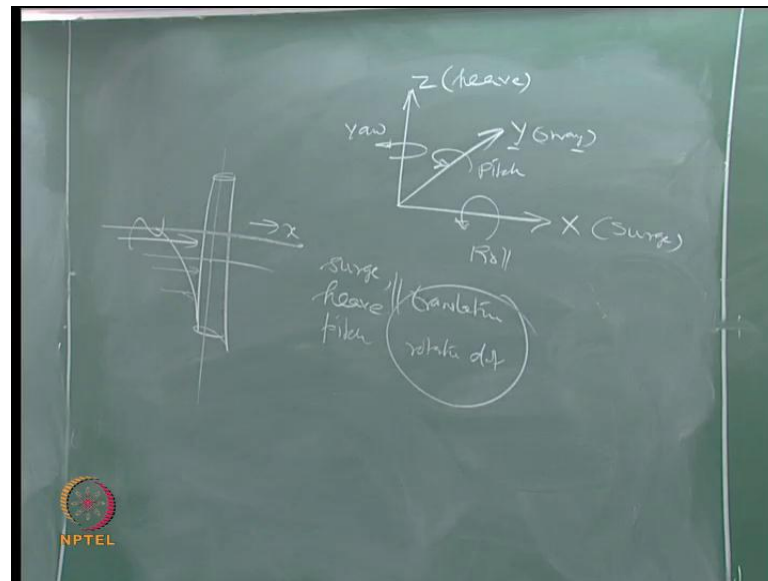
Now, the velocity potential in all the three regions should satisfy the Laplace equation. Call this as equation number 5. We will do one thing, we will use this different notation we will say $\nabla^2 \phi = 0$. In addition, region one should also satisfy the boundary condition, region is the outer region, this is a free surface boundary condition. Therefore, I should say this should be satisfied and at $z = 0$, z is measured from the mean level, call this equation number 6.

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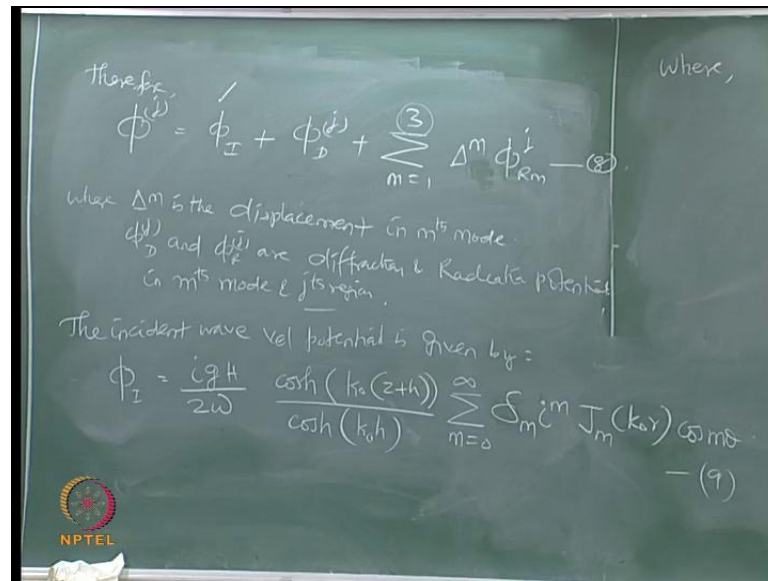
Now, velocity potential in regions 2, 1, 3 should satisfy also the following condition that is sea bed boundary condition, because z is minus h . I will call equation number 7, so for linear water waves ϕ , in any region can be decomposed into one - the incident potential which I call as ϕ_I , there radiation potential which I call as ϕ_R , and the diffraction potential which I call as ϕ_D . The radiation and depression potential will be valid for a count of J , I will explain this; there are three regions - 1, 2 and 3. Now, interestingly when the floating structure is subjected to unidirectional waves only surge, heave and pitch will be active.

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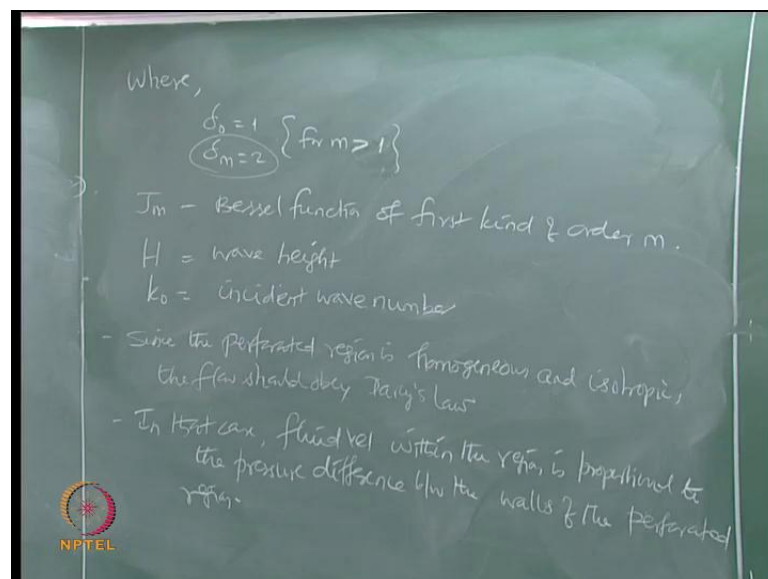
We all know that, and put you if comes towards this this four fingers will give me the direction of rotation, this wayyeah. Now, I have a cylinder acted upon some force velocity variation, so the force just becomes x direction, so I will have surge and we all known a floating system the setdown or the heave in the surge motion of strongly coupled setdown offset or coupled. Therefore, I will have heave and the differential forces at the any point will cause a movement and that movement will be a about normal to this axis nothing but pitch. So, we will have two translational and one rotational degree of freedom active, when the wave in unidirectional. So, only three modes will be active, surge heave a pitch; though it is got six degrees of freedom, but we will active only three, that is what I am writing here only surge heave and pitch will be active.

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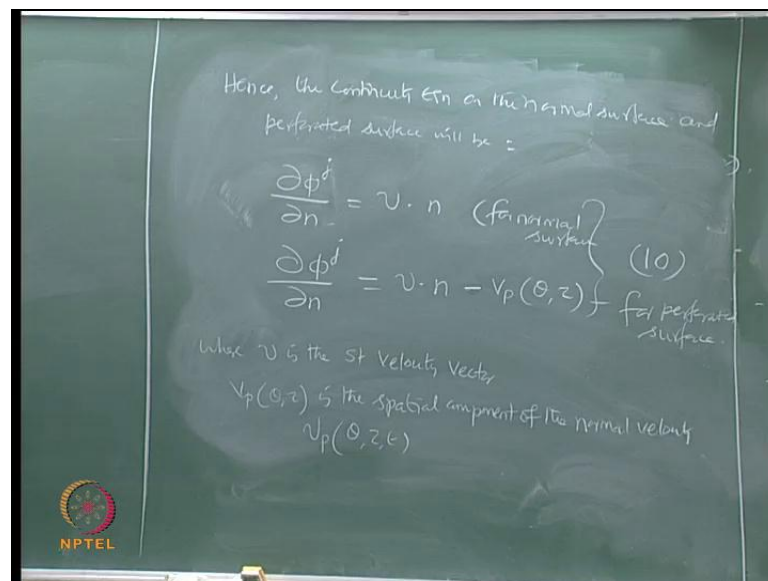
Therefore, ϕ can be expressed as incident plus diffraction, sum of so you can see here the summation done only for three modes. What is the equation number here? Where Δ^m is a displacement in m^{th} mode, ϕ_D and ϕ_{Rm}^j are diffraction and radiation potentials in m^{th} mode, and j^{th} region; j stands for the region. How many regions do we have in this problem? Three-region one is the outer periphery, region two is a porous periphery or the porous region, and region three is a region below region two, where defined the boundary condition for this regions, in equation 2, 3, and 4. Now, the incident wave velocity potential is given by ϕ_I , which is given by $2gH/\omega$ equation nine.

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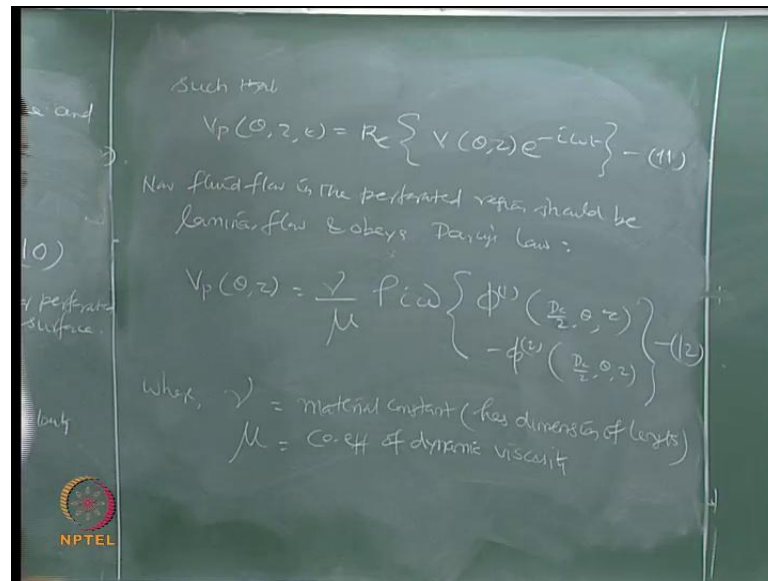
Where let me check this equation first. This is J_m , this is J_m , J_m is equal to 1, and Δm is equal to 2 for m equal to 1 greater than for any value m greater than 1 can say these values 2, when it is 0 when it is taken as unity in this expression. J_m is a Bessel function of first kind of order m . H is the wave height of course, and k is the incident wave number. Now for example since the perforated region is homogeneous. Let say an isotropic the flow should obey Darcy's law. In that case, fluid velocity within the region is proportional to the pressure difference between the walls of the perforated region.

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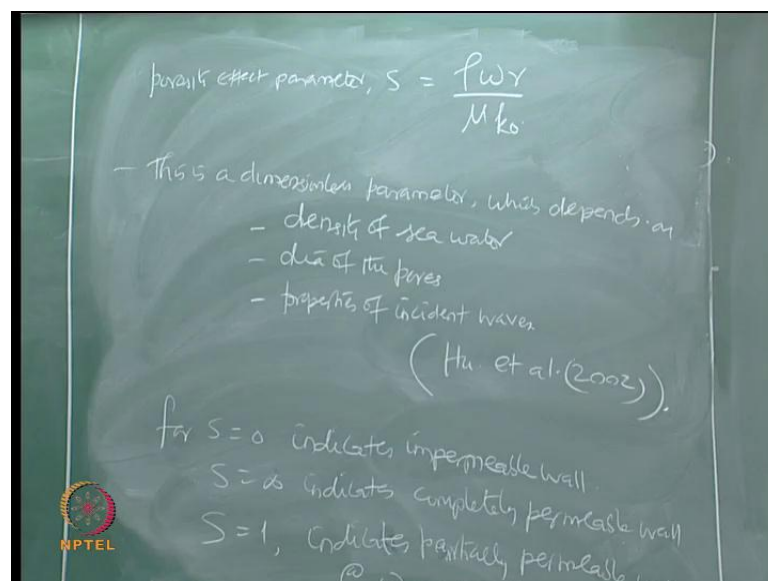
Hence, the continuity equation on the normal surface; normal surface means non perforated and the perforated region will be given by... Let me call this equation number 10, is it. So, this is for normal surface and this equation for perforated surface, where v is the structural velocity vector, and v_p of θ, z ; is a special component of the normal velocity, the normal velocity is v_p of θ, z of which is valid applicable to the perforated region only.

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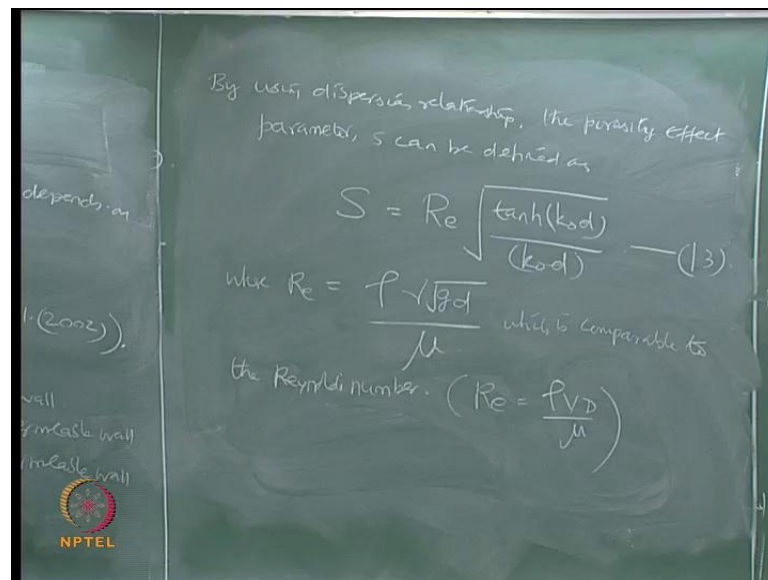
Such that there is the condition which is satisfy v_p of θ z of t is real component of v theta of z e minus i ω , call this equation number 11. Now, the fluid flow in the perforated regions should be a laminar flow, and obeys Darcy's law. In that case, v_p theta z is given by ν by μ rho ω ϕ one of D_c by $2D_c$ by 2 theta z minus ϕ 2 of D_c by 2 theta z . Let me check this equation, I call this equation number 12, where ν is a material constant, which has dimension of length in case of units, μ is the coefficient of dynamic viscosity.

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Let us now define in parameter call porosity effect parameter, which is define by S which is given by $\rho \omega r$ by μk naught, this is the dimension less parameter which depends on density of sea water diameter of the force, and properties of incident waves. This parameter was first suggested and dependency of this factors, where established by Huetal in 2002, then the porosity effect parameter S for S become 0, indicates impermeable wall and S equals infinity indicates completely permeable wall, that is wall does not exist. In the present study, we have assumed S is equal to unity, which indicates partially permissible wall at a specific frequency of 0.3 radian per second. Now, one can compare this porosity effect parameter with the well-known established relationship Reynolds number by using dispersion relation.

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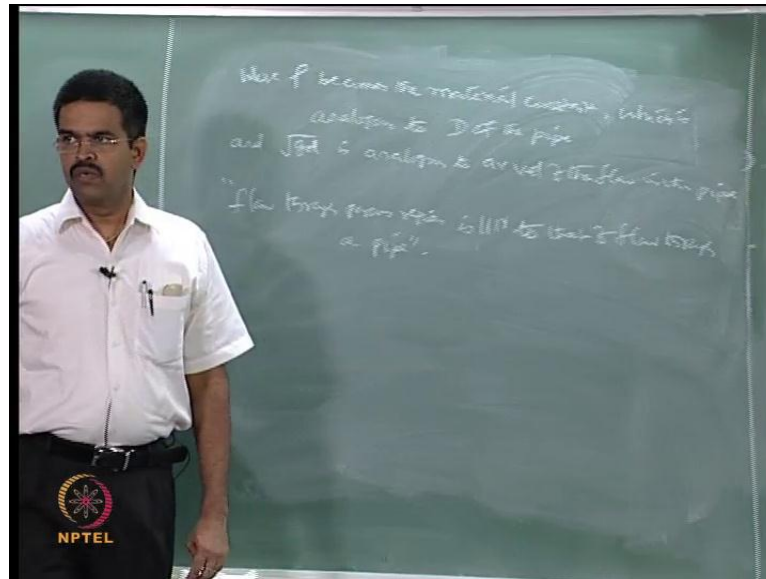


Now by using dispersion relation, the porosity effect parameter s can be defined as, call this equation number, what the equation number?

Student: 13.

Where R_e , this R_e is equal to $\rho \mu g d$ by μ , which is comparable to the Reynolds number, because Reynolds number is $\rho V D$ by μ .

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Where ρ becomes a material constant, which is analogous to D of the pipe and J is analogous to average velocity of flow in the pipe, so what does it mean is, once we can establish the porosity effect parameter as similar to that of Reynolds number which indicates that the fluid flow is similar to that of pipe. So, I can say now the flow through porous region is similar to that of flow through a pipe, so we stop here we continue this lecture in the next one, where you will continue to derive the other velocity potential components. And then, you will apply this on a floating platform. How I can compute the influence of these parameters on the force reduction in a floating system, which is having porous members?

Thank you.