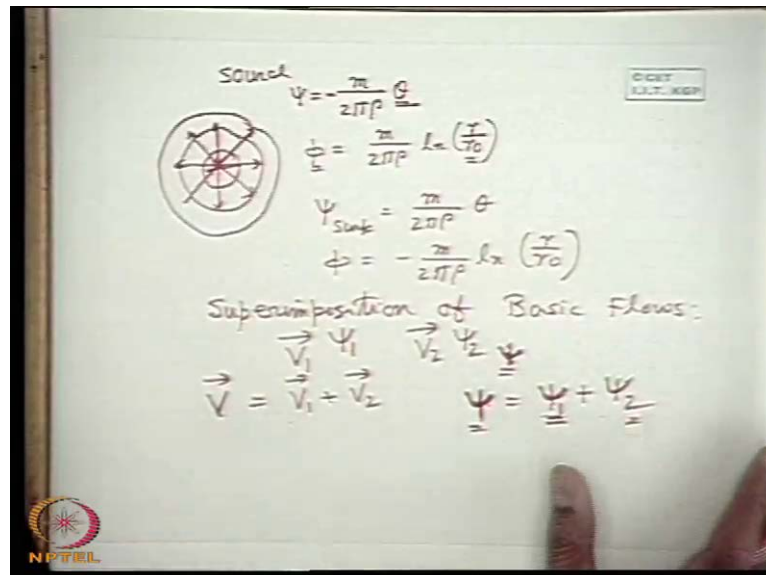


Fluid Mechanics
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Lecture - 40
Flow of Ideal Fluids Part – II

Good morning, I welcome you all to this session of fluid mechanics. Today, we will be continuing the discussion on ideal fluids; it is ideal fluids part 2. Now last class if you recall, we discussed about the stream functions, and the velocity potential functions and the stream lines and the velocity potential lines, equipotential lines for source and sink flow.

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If you recall that; now we can see here, that is source flow is a flow which in a two dimensional plan can be thought of as a line source, which is seen in done as a point where from the fluid is coming out uniformly in all radial location. This is a source and sink is the reverse of these at the fluid is approaching towards a point uniformly from all radial directions. So, in this kind of flow we derived earlier the stream function was given by m ; where m is the strength of the source, which is the mass flow rate. Total mass flow rate coming out from the source, by twice π rho into theta with a minus sin and the velocity potential function was recognized as m by twice π rho, \ln , r by r_0 , so where this r_0 .

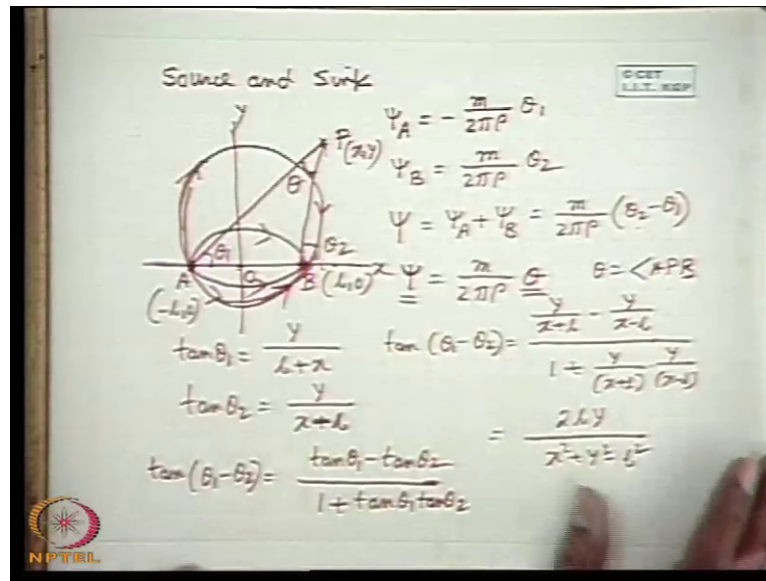
So, therefore, first of all let us see that the constant value that is the stream lines, is ψ is equal to constant where θ is constant; that means, the radial lines. So, radial lines are the stream line, similarly equipotential lines are the lines where r is constant if you make ψ is equal to constant. So, these are concentric circles. And $r = 0$ implies a radius where, we are considered an arbitrary value of 0 for the ψ function. Now for a sink, this is for a source. So for a sink, the stream function for sink is just with a negative sign because source and sink are physically same; only with a negative sign similarly ψ for a sink will be that velocity potential function, for a sink will be like this.

Now today we will see the superimposition of certain basic flows. Now superimposition may, let me write superimposition of basic flows, superimposition of basic flows. Now one thing you must know that when two flow fields are superimposed, if the velocity vector of one flow field is V_1 and the velocity vector of another flow field is V_2 ; that means, V_1 and V_2 are the velocity field of the two flows which are superimposed on one another, when the velocity vector the result and velocity of the flow field will be the vector addition of these two velocity vectors.

Since ψ is a linear function of the velocity vector, then if ψ_1 represents this stream function for one flow and ψ_2 for another flow. Then the resulting flow will have a ψ function or a stream function of this stream function of the resulting flow will be the sum of the stream function of the two flows. This is because stream function is a first order derivative of, not first order other I will tell first power; we are say first power relationship with the velocities, because it is simply the derivative of the velocities, velocity gradient. So, therefore, the basic conclusion is that if ψ_1 is this stream function for one flow and ψ_2 is this stream function for other flow; if these two flows are superimposed the result and flow ψ function can be obtained by the addition of the ψ function of these two.

Now with this method of, with this basic we can now, see first the combination of source and sink, source and sink, combination of source and sink. Now let us consider a flow where a source and sink located like that, let A is the source and B is the sink, A is the source B is the sink; now if we consider a point P in the flow field which is generated by the combination of source and sink, now we can write like this that if we just join these two points, let this is θ_1 ; θ_2 ; in a polar coordinate system we can write that for source this ψ , that is ψ_1 , that is ψ_A is minus m by 2π ρ θ_1 .

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Now for the sink at B, ψ_B is equal to negative of that. So, therefore, it will be twice $\rho \theta_2$. So, therefore, we see the ψ function for the resulting flow, that is the flow which resulting due to the combination of the source and sink will be ψ_A plus ψ_B ; which can be written as m by $2\pi\rho$ into θ_2 minus θ_1 . So, this θ_2 minus θ_1 from geometry is this end. So, therefore, we see ψ is equal to θ where θ is the angle APB , where θ is angle APB .

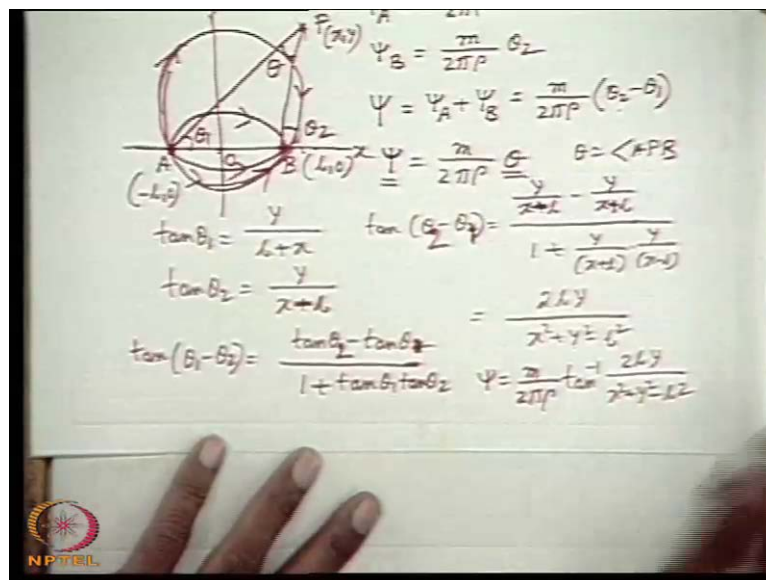
Now here we see one interesting thing that the constants ψ function line; that means, stream lines are those lines along with θ is constant; because if we put ψ is equal constant which will give θ is constant, which means these will be the circular arcs; that means, the stream lines will be the circular arcs with AB as the base cord. So, that this angle will always remind constant; that means, this will be the, this will be the for example, this is one circle which called is AB , this is source, this is sink. So, this will be the stream lines. So, other circular arcs can be thought up this stream lines like this. Now we can develop the expression for stream function in a Cartesian coordinate system; let us consider this x let us consider the y axis, let the co ordinate of any point is (x, y) .

That Therefore, we can write \tan , this θ_1 and θ_2 is there. Now we can write $\tan \theta_1$ is what y , the y coordinate of the point divided by b plus x , b plus x where we take distance thus B ; that means, the coordinate of A where the source is kept is minus b

0 and the coordinate of B on the positive x axis this where the sink is kept is b 0; which means if this be the origin O A is equal to b, O B is equal to b, so b plus x.

Similarly tan theta 2 is equal to theta 2 is this angle we drop a perpendicular from the point P on the axis, we will get y is e into x plus b I am sorry x minus b, x, this is x minus b; it is x plus b, it is x minus b. So, therefore, we can write 10 theta 1 minus theta 2 which is equal to, you know the formula; for this. Tan theta 1 minus tan theta 2 divided by 1 plus tan theta 1 tan theta 2. So, therefore, we can write tan theta 1 minus theta 2 is equal to if you replace this y x plus b minus y x minus b divided by 1 plus y x plus b into y x minus b. So, if you simplify it, it will come 2 b y divided by x square plus y square minus b square.

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So, therefore, we can write with this that the psi, here we can write therefore, psi is m by 2 pi rho theta 2 minus theta 1. So, well it is theta 2, I am sorry will have to make it theta 2 minus theta 1. So, theta 2 is x plus b. So, theta 2 is x theta 2 is x minus b; it is x plus b. So, it as to be theta 2 minus theta 1, I am sorry theta 2. So, if you see theta 2 minus theta 1 is tan inversely; that means, tan inverse x square plus y square minus b square.

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Handwritten derivation on a whiteboard:

$$\Psi = \frac{m}{2\pi\rho} \tan^{-1} \frac{2by}{x^2 + y^2 - b^2}$$

As $2b \rightarrow 0$, $m \times (2b) = \text{constant} = c$, $x \rightarrow 0$

Doublet or Dipole

$$\Psi = \frac{c}{2\pi\rho} \frac{y}{x^2 + y^2}$$

Diagram showing flow field for a doublet (dipole) with streamlines forming closed loops.

$$c = \frac{lm}{\pi\rho} = \frac{lm}{\pi\rho} \frac{y}{x^2 + y^2}$$

$$c = \frac{lm}{\pi\rho} \frac{r \sin\theta}{r^2}$$

$$\Psi = \frac{c \sin\theta}{r}$$

Logos: CCET U.T. KOP and NPTEL are visible on the whiteboard.

So, therefore, in Cartesian coordinate we get this stream function ψ is equal to m by $2\pi\rho$, \tan inverse in terms of the Cartesian coordinates $2by$ by $x^2 + y^2 - b^2$; where $2b$ is the distance between the source and the sink, m is the strength of both the sources and the sink. Now we will consider a case, where source and sink are plus it such a way that the distance between them tends to 0 with the condition that, the strength times the distance remains finite or constant; that means, the sources and strength are kept that a distance and ultimately they are approaching towards each other the distance between them tending to 0; with the constraining in equation that the product of this strength and the distance of separation is constant.

So, these type the flow field which is arrived, this known as Doublet or Dipole; the flow field which is arrived by this way, combining source and sink in this way is known as a Dipole. So, what we can do this is the combine stream function for a combination of source and sink; from here we can see that if $2b$ tends to 0; that means this tends 0. So, \tan inverse of a quantity which is tending to 0 can be written as the quantity itself; which means that \tan inverse x , at x tending to 0 is equal to x itself.

So, therefore, we can write under that limiting conditions for a Doublet or Dipole ψ is equal to m by $2\pi\rho$ with this mathematics into $2by$ divided by $x^2 + y^2 - b^2$. So, limit of this as b tends to 0. Now when b tends 0, but bm is constant. So, that we can write bm by $\pi\rho$ can selling this, $2bm$ by $\pi\rho$ into y b tending to 0;

that means, y by x square plus y square or simply we can write in terms of Polar coordinate; $b m$ by $\pi \rho$ into $r \sin$ in θ divided by r square. Considering this as a constants C , we defined a constant C as $b m$ by $\pi \rho$ because $b m$ is constant according to the definition of this type of problem.

So, therefore, we can write $C \sin \theta$ divided by r , this is the stream function of a Dipole. So, Dipole will be like that when you see this source and sink will approach each other, this angle will become 0 and ultimately this circular arcs with $A B$ as the base cord will become tangent, will become circles with tangent at the x axis at the origin; that means, this will be the nature of the, this will be the nature of the, this will be the nature of this, now this we will be the nature of this Dipole; where Dipole is at the origin. Because they are plus symmetrically have from the original they are tending to that distance of separation tending to 0 . This is the Dipole or Doublet stream lines of the Dipole or Doublet constant stream function.

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Superimposition of Rectilinear Flow and Doublet parallel to x axis

$$\Psi = -uy + \frac{C \sin \theta}{r}$$

$$\Psi = -u r \sin \theta + \frac{C \sin \theta}{r}$$

at $\Psi = 0$ $\sin \theta = 0^\circ$ or 180°

$$ur = \frac{C}{r}$$

$$r^2 = \frac{C}{u}$$

$$r = \sqrt{\frac{C}{u}} = a$$

NPTEL

Now we will come to a very interesting phenomena or very interesting situation by superimposition of, superimposition of, superimposition of rectilinear flow, which we have discussed earlier rectilinear flow and doublet, and doublet.

Now, the superimposition of this two flow give this stream function for the result and flow, it is a some of this stream functions square rectilinear flow and that are doublet. Rectilinear flow if you recall thus stream function is given by $u y$; where u is the velocity

of the rectilinear flow, but here rectilinear flow parallel to x axis. So, it is the superimposition of a rectilinear flow parallel to x axis and the doublet; that means, here if we see that there is a rectilinear flow parallel to x axis; if you take this as x this as y this is u. So, stream function for this rectilinear flow u y, we have already discussed.

And this is the stream function for the doublet. So, if you superimpose rectilinear flow with the doublet, then what you get? u y plus C as defined earlier for the doublet $\frac{C \sin \theta}{r}$. Now if I write y in terms of r and theta in Polar coordinate system. So, it will be r sin theta plus $\frac{C \sin \theta}{r}$. This the typical stream function for the combination of rectilinear flow parallel to x axis and the doublet.

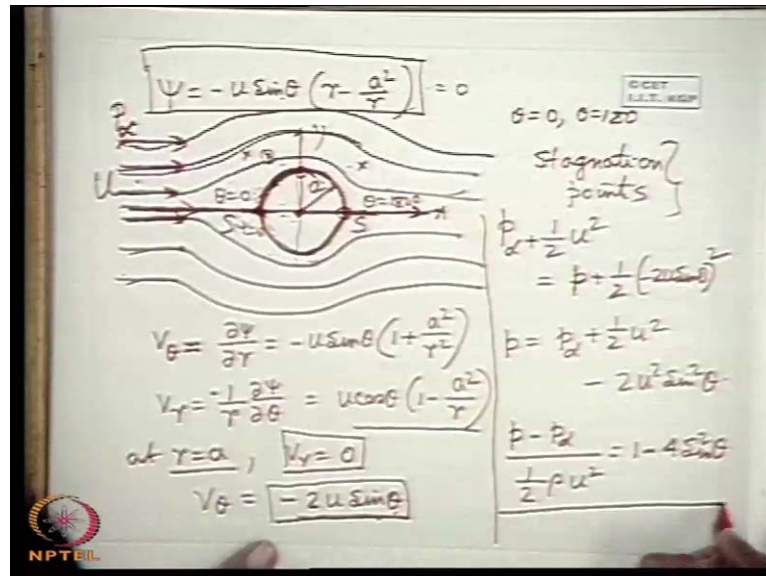
Now you see that in this type of stream functions, we get some interesting thing that as psi is equal to 0; that means, if we consider one value of this stream function arbitrary to 0; that means, along a stream line where psi is equal to 0, we get some conclusion; that sin theta is either 0 degree or 180 degree; that means, if sin theta at sin theta is equal to 0 and 180 is the value of stream function is 0. We can ascribe the value of stream function of 0; another solution is that for any theta we can get a value of psi 0, provided u r is equal to c by r or simply r square is c by u or r is equal to root over c by u.

Let this root over c by u be denoted by a; that means, for all values of theta psi is equal to 0 is obtain along points whose radial coordinate are radius vector r is constant, because c is constant, for the doublet and u is the constant because rectilinear flow the velocity u is constant, it is parallel to the x axis. So, this is constant. So, if you replace now mathematically, root over c by u is equal to a then we get psi is equal to minus u sin theta into r minus a square by r; because c is x square u minus u sin theta r minus a square by r. So, this is the stream line which is obtained.

Now, if we write this stream line again, that psi is equal to minus u sin theta into r minus a square by r. This is the stream line which is obtained if a cylinder is placed at the origin; that means, this is the axis x this is the y. In an infinite expands of a parallel flow of an ideal fluid; that means, other way we can tell if in the if a parallel flow in infinite expands of an ideal fluid is cylinder is placed, the where this stream line will be deflected by the cylinder will be given by this similar functions; that means, this psi functions; that means, if we make this is equal to constant the low cos given by this theta and r coordinates will be similar to the case, when an parallel flow parallel to the x axis for an

ideal fluid will be deflected by a cylinder which is placed at the origin to the axis is at the origin; that means, it is the ideal flow passed a circular cylinder.

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So, therefore, the stream functions or stream lines for an ideal parallel flow passed is cylinder like this can be generated by combination by the combination of doublet and a rectilinear flow. Let us find out two velocity component, one is the tangential velocity component; that means, we define for example, this is the direction. So, with this direction we define this is theta is equal to 0. Now another very interesting thing is that psi is equal to 0 is along the line theta is equal to 0 and this is theta is equal to 180 degree or pi and for all theta this is the surface of the cylinder where radius is constant.

So, a here in this equation will represent the radius of this cylinder. So, this is the stream function for a parallel flow passed parallel flow of ideal flow its passed a circular cylinder whose radius is a. So, therefore, the this line; that means, the fluid particle flow in this line theta is equal to 0 along the cylinder and then going by this line and another is diverted in this way this is corresponds to size equal to 0; these are the lines corresponding other values of sin.

Let us find out V_θ and V_r at any point here are any point here what is the definition of tangential velocity in terms of the stream function if you recollect this is $\frac{\partial \Psi}{\partial r}$; that means, this becomes is equal to minus $u \sin \theta$ if you differentiated $1 + \frac{a^2}{r^2}$ by r^2 . Similarly if we find out the radial velocity which is connected with

this stream function as $1/r \frac{\partial \psi}{\partial \theta}$ and with a negative sign; this is positive, this is negative.

So, this becomes is equal to $u \cos \theta$ into $1 - a^2/r^2$. Now at this surface of this cylinder r is equal to a . So, at r is equal to a , we clearly see V_r is equal to 0; which is obvious. At this solid surface they are cannot be in a radial velocity of the fluid because solid surface is impervious to the fluid flow of fluid until then unless it is porous surface. So, is solid surface they are cannot be any component normal to the surface. This is one of the very important and universal boundary condition, that for an ideal flowing this it flow, they are cannot be even for a real fluid, they are cannot be any normal component of flow velocity on a solid surface until and unless solid surface is porous. So, therefore, this is 0.

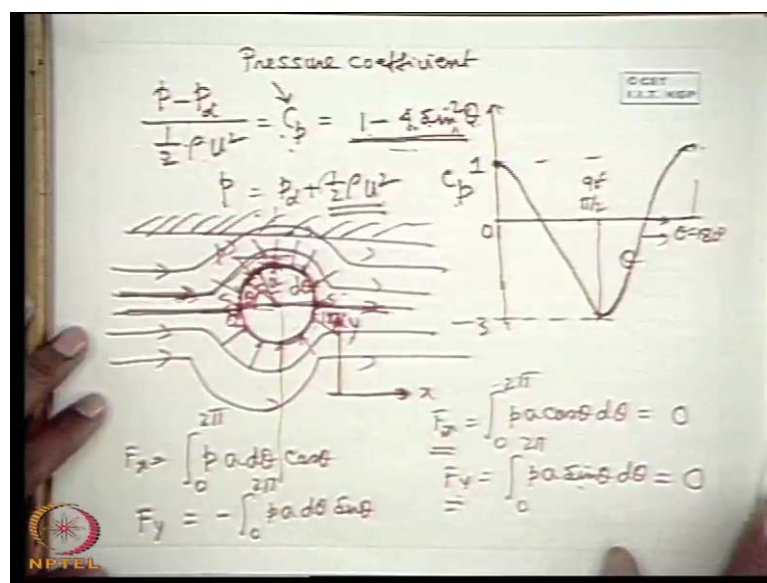
Whereas V_θ r is equal to a , we get if you put it there we get $-2u \sin \theta$. So, there is a tangential velocity. So, no slip condition will not prevail here because the fluid is ideal there is no viscosity; so fluid slips or flows pass this cylinder in a direction surface of this cylinder in a direction along this surface. So, it is $-2u \sin \theta$; now from here one thing is very clear. So, this function is symmetrical, this function is symmetrical about this axis; that means, the velocity over this zone from 0 to 180 is same as 180 to 360, but it is not symmetrical about this axis, if you seeing this the velocity first become 0 here. θ is equal to 0, then it goes on increasing at θ is equal to $\pi/2$; because the sin function attend this maximum value they are and then again it is reducing from $\pi/2$ to 180 and the same continue in this are into negative sin; that means, the numerical value of the velocity is 0 here, and then increases to the maximum again comes to the 0 and same thing is repeated here. So, therefore, velocity field is symmetric about this axis.

Now at this two point θ is equal to 0 and θ is equal to 180 degree, this two point the velocities are 0 and this two points are known as S; stagnation point that you know, we have discussed earlier. Where the velocity there in a particle approaching along this line θ is equal to the straight this surface and is velocity totally destroyed means it is converted only into the pressure energy because there is no other destructions; that means, the kinetic energy cannot be convert into inter molecular energy because fluid is frictionally. So, velocity is converted into pressure and they are the fluid particles at rest.

Similarly, fluid particle is at rest it reaches the maximum velocity, here this two points are known as stagnation, stagnation points. Where the in a flow fields stagnation points are those points where the flow velocities become 0, these are the points at theta is equal to 0 and theta is equal to 180 degree; this is known as forwards stagnation point and this point is known as rayers stagnation point. Now if you look the pressure field, what happens? Now if we describe the pressure at the for upstream or for downstream as the undisturbed pressure known as fresh stream pressure, P_{∞} ; then we can write the Bernoulli's equation at any point in the first stream at any point near the cylinder, where the flow flid is develop due to this cylinder in this fashion according to this stream functions or this velocity functions that the velocity expressions of the velocity.

Then we can write $P_{\infty} + \frac{1}{2} \rho U^2$; here the velocity field is only u , plus half u square is equal to pressure; that means, we are interested to find out the pressure, at any point the pressure, distribution equations $p + \frac{1}{2} \rho v^2$, but now if we take the point, any point that the cylinder surface then what will be the velocity at the cylinder surface? The radial velocity is 0. So, the only velocity is the V_{θ} . So, this is the velocity at the cylinder surface, minus $2u \sin \theta$ whole square. So, we can write p is equal to $p_{\infty} + \frac{1}{2} \rho U^2 - 2 \rho u^2 \sin^2 \theta$. So, therefore, this will be becoming minus half twice u this is 4 twice, $u^2 \sin^2 \theta$. Now, this is the pressure distribution equation.

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Now we make it in a conventional fashion express $p - p_{\infty}$ as difference of pressure at the surface from this free stream pressure divided by $\frac{1}{2} \rho u^2$ as $1 - \sin^2 \theta$. So, this is the pressure distribution equation. So, now, if we write the pressure distribution equation again, we see that the pressure distribution equation becomes $p - p_{\infty}$ in terms of this dimensionless quantity, this is the dynamic head based on the free stream velocity, this is the difference between the pressure at any point and the free stream pressure; this is known as C_p pressure coefficient, this is known as pressure coefficient, coefficient this becomes $1 - \sin^2 \theta$.

Now, if we plot this thing we will get a curve like this, if we plot this thing we see will better plot here we will get a curve like this, now here if we see that θ is equal to 0; this is θ , this is 0. The at θ is equal to 0 this is 1; that means, $p - p_{\infty}$ is $\frac{1}{2} \rho u^2$; that means, p is $p_{\infty} + \frac{1}{2} \rho u^2$; that means, this is the stagnation pressure. Here if you see here the V is 0; that means this velocity is 0. So, pressure here is stagnation pressure; that means, the dynamic head based upward this free stream parallel fluids convert into pressure. So, this is the stagnation pressure, so C_p is 1 here.

So, then pressure goes on decreasing as the velocity goes on increasing, I had shown you earlier velocity increases over this part. So, therefore, pressure continuously goes on decreasing and you see this function reaches if this is C_p in this direction, this is the θ this function reaches a minimum value at θ is equal to $\frac{\pi}{2}$ which is $1 - \sin^2 \frac{\pi}{2} = 1 - 1 = 0$. So, therefore, we see this reaches a minimum value at $\frac{\pi}{2}$. So, this is $\frac{\pi}{2}$ and this is $\frac{\pi}{2}$ or 90 degree. Then again it goes up and takes the value of 1 again this is 1 the same value, when θ is 180 degree.

So, this function you see is symmetrical about this axis, about this axis, but the variation takes place it is not symmetrical about this axis. So, we show only the variation from 0 to 180 degree. So, it shows that it is justify draw this thing again, this stream lines are like this, stream lines are like this. So, therefore, so this is the stream lines. So, this is the stream lines, so this is the stream lines. So, this is the axis. So, therefore, you see that this pressure distribution over this line from 0 degree to 180 degree; that means, this two stagnation point, this goes on decreasing. So, this for the fluid is accelerating and pressure is decreasing. So, this is the maximum velocity and minimum pressure point. So, this is C_p the pressure coefficient; again this for the fluid is retarding velocity is

decreased because we have seen earlier the velocity function; then the fluid pressure is increase then we recover here same pressure. There is no dispersion of pressure to the intermolecular energy because fluid friction is absent.

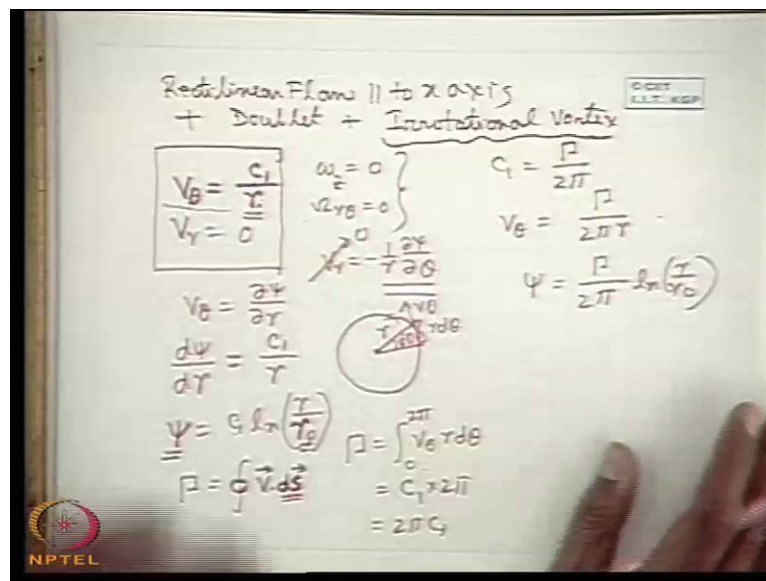
So, this part is the accelerating flow, this part is the retarding flow. This can be well understood that if we consider a surface here, as certain distances away from the cylinder you will see that for flow in this part this gives a convergent duct. So, curvatures is such as if it is flowing through a convergent duct whereas, flow in this per the curvature is here it is flowing through a divergent duct and the pressure is therefore, increase and velocity is decrease. Now one important thing comes that if we consider the force net force acting on the cylinder. So, it is an ideal fluid. So, cylinder surface the only force acting is the pressure force, this is the pressure force only force acting is the pressure force because there is no force along the tangent to the cylinder at it surface because there is no viscous force. So, this is only force p.

Now if we want to evaluate the force acting on the cylinder along x and y direction, x is the direction that is the direction of the flow the axis flow, axis parallel flow and y is the transverse direction, the direction perpendicular to this parallel flow direction. Then we can write if F_x is equal to, if we take a small element here at an angle theta of radius this radius is a, and this subtended angle is $d\theta$; the radius is a. So, we can write the force on this element is p if the pressure is p . So, the $a b \theta$, this is the length of this r . $a d\theta$ per unit length of this cylinder in this direction that is in a direction perpendicular to this plain of paper, so per unit length this is the force on this element $p a \theta$. So, if you take its component $\cos \theta$, $\cos \theta$ will be its component, in this x direction because this is the angle theta. So therefore, $\cos \theta$ if we integrate it over the entire cylinder, you will get similarly F_y will be y is taken positive upwards minus 0 to 2π $p a d\theta$, $\sin \theta$.

That means simply we can write F_x is $p a \cos \theta d\theta$ integrated over 0 to 2π and F_y is integration of $p a \sin \theta d\theta$, integration of 0 to 2π . Now this you see if the pressure in involves a function like this, then if you multiply this is an even function of theta $\sin \theta$. So, this is independent of the sin of the $\sin \theta$. So, therefore, the pressure variation is symmetric about this axis. Now if we multiply this function with $\cos \theta$ and $\sin \theta$ and if you integrate to 0 to 2π in both the cases we will get 0 .

That means in this case what happens is that, the entire cylinder does not experience any force in x and y direction; which means the pressure distribution is symmetrical over the entire cylinder. So, that it gives neither a, neither a force in x or y direction because here you see the $\sin p$ minus p infinity by half rho is the independent of the sin of the sin theta. So, that it is almost symmetrical; that means, it is symmetrical about both this and this axis. So, therefore, no force is exacted in neither in either x are y directions.

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So, alright next we will discuss a combination of, a combination of rectilinear flow, we will discuss the combination of rectilinear flow, rectilinear flow the same flow parallel to y axis parallel to sorry x axis plus Doublet plus a irrotational vertex plus and irrotational vertex. You have already seen, let us first before that discussed little bit of irrotational vertex; we have already seen, that an irrotational vertex flow, that a vertex flow which is irrotational, the tangential velocity is describe by some constant by r, C by r; let this constant we denoted by c_1 by r, because we are already handling with one constant c in the stream function of Doublet and V_r is 0; that means, vertex flows that the flows whose stream line are concentric circulars; that means, it has got only tangential velocity, where the velocity here say, functional relationship with the radius like this c_1 by r radial co ordinate and there is no radial velocity, this we have already seen and for this type of vertex flow the rotation is 0; that means, ω_z is 0, the rotation component is 0, ω_z is 0; that means, the vorticity in r theta plane is 0, that we have already recognized. So, this flow is known as irrotation vertex flow.

So, the irrotational vortex flow, if you want to derive this stream function, who can you derive this stream function? You can write, V_θ is $\frac{1}{r} \frac{d\psi}{d\theta}$ and V_r is $-\frac{1}{r} \frac{d\psi}{dr}$. Since we are in irrotational flow so ψ is not a function of θ . So, ψ is a function of r only; that means, we can write $d\psi$ instead of $\frac{d\psi}{dr} dr$ and V_θ can be written as some constant by r , if we integrate it you get ψ is equal to $c \ln r + r_0$. So, r_0 is a constant comes after the integration, which physically signifies that at $r = r_0$ ψ is equal to 0; that means, we define an arbitrary value of ψ is equal to 0 at $r = r_0$ and also you know that, if V vortex motion can never we describe of to the centre are the origin of the coordinate system where $r = 0$, because here v_θ is undefined in finite that gives a point of singularity.

Now, if you recall the definition of circulation Γ , we now this is defined as the closed contour integral of $\mathbf{V} \cdot d\mathbf{s}$ where $d\mathbf{s}$ is the elemental, $d\mathbf{s}$ is vector if you take along the element along an elemental length, along a path and closed contour integral, along a closed contour \mathbf{v} is the velocity vector. So, in a free vortex flow in that way, if we define the if we evaluate this circulation, we will get that $d\mathbf{s}$ means, let the radius is r at over any circular part and this is, this is the θ so this $d\mathbf{s}$ is $r d\theta$ and $\mathbf{V} \cdot d\mathbf{s}$ \mathbf{V} is only in the tangential direction V_θ . So, $V_\theta r d\theta$ and V_θ is c/r ; that means, it will be 0 to 2π along the closed contour it will 0 to 2π .

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Handwritten mathematical derivation on a whiteboard:

$$\psi = -u \sin \theta \left(r - \frac{a^2}{r} \right) + \frac{\Gamma}{2\pi} \ln \left(\frac{r}{r_0} \right)$$

$$V_\theta = \frac{\partial \psi}{\partial r} = -u \sin \theta \left(1 + \frac{a^2}{r^2} \right) + \frac{\Gamma}{2\pi r}$$

$$V_r = \frac{u \cos \theta}{r} \left(-\frac{a^2}{r} \right) + 0$$

at $r = a$ V_r at $r = a = 0$

$$(V_\theta)_{r=a} = -2u \sin \theta + \frac{\Gamma}{2\pi a}$$

$$V_\theta = 0$$

$$\sin \theta = \frac{\Gamma}{4\pi a u}$$

The diagram shows a circular flow with radius a and angular position θ . The origin is at the center of the circle.

So, c_1 by r are canceled it is c_1 and $d\theta$ is 2π into 2π . So, therefore, $2\pi c_1$ therefore, this constant in the velocity function defining the tangential velocity in a vortex flow is nothing but $\frac{\Gamma}{2\pi}$. So, therefore, the θ can be written usually is value written in terms of the circulation constant like this and ψ also can be written as $\frac{\Gamma}{2\pi}$. So, because c_1 is $\frac{\Gamma}{2\pi}$ this we have to $\ln r$ by r^0 .

So, if we know now this thing the now the combination of the rectilinear flow parallel to x axis is Doublet and irrotational flow gives a stream function, which is first of all the rectilinear flow and Doublet gives this stream function which already we are derived as, $u \sin \theta$ into r minus a square by r only with this we add $\frac{\Gamma}{2\pi} \ln r$ by r^0 . Now here we will notice always that when we add a circulation term r in irrotational flow vertex, irrotational vertex motion are a free vertex motion, then what we get, we get an asymmetric because of separate ambivalent functional add a deity.

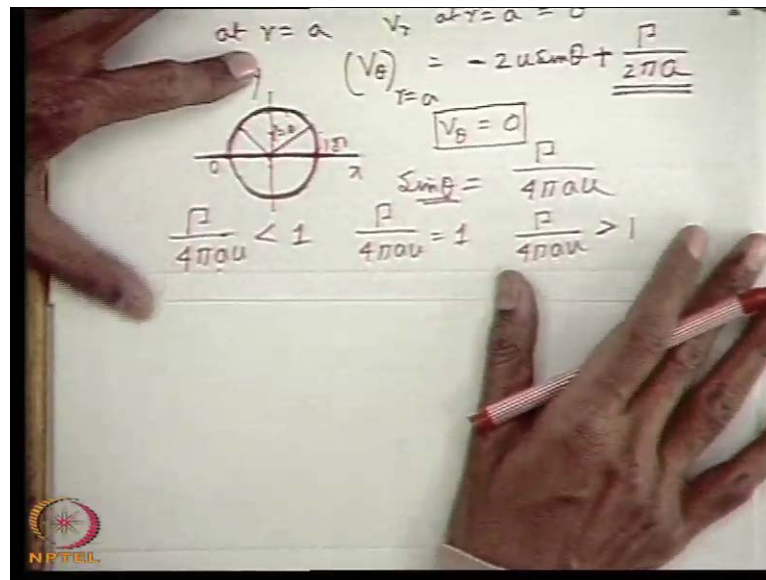
Let us see now, if we just try to find out the v_θ is $\frac{d\psi}{dr}$; let us see, what is V_θ ? That is $\frac{d\psi}{dr}$; that means, $u \sin \theta \frac{1}{r^2}$ plus a square by r^2 , if you differentiate this we get $\frac{\Gamma}{2\pi} \frac{1}{r}$ and if you write V_r it will be $u \cos \theta$ same thing $\frac{1}{r}$ by r $\frac{d\psi}{d\theta}$; that means, it is $1 - \frac{a^2}{r^2}$ and this part will be 0 this is independent of θ . So, therefore, on this surface of the cylinder; that means, mathematically at r is equal to a ; that means, if we plot the cylinder.

Here on the surface of the cylinder r is equal to a V_r is 0, but what is V_θ ? V_θ V_r at r is equal to a as usual 0, but V_θ at r is equal to a does not give fully minus $2u \sin \theta$ in this case, because this first star will give the similar term the same term minus $2u \sin \theta$, but added with another term twice $\frac{\Gamma}{2\pi} a$, so minus $2u \sin \theta$ plus twice $\frac{\Gamma}{2\pi} a$. So, therefore, it is distinct that this term $2s$ and azimuthally; that means, velocity vector now, is not symmetric about this axis about this x axis; which is because $\sin \theta$ changes it \sin from 0 to 180 degree and 0 to, so 0 to 180 degrees $\sin \theta$ is got one \sin and the \sin of $\sin \theta$ changes from 180 degree to 0. So, therefore, this \sin is changing and this is superimposed with a constant term $\frac{\Gamma}{2\pi} a$.

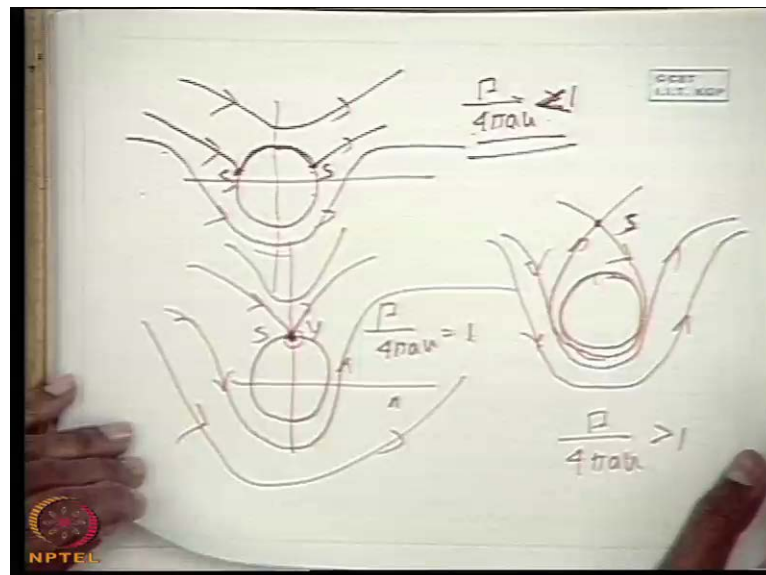
So, therefore, V_θ is never symmetric about this axis so; that means, of flow field becomes a symmetric; that means, flow field about this up and flow field about this up will be different. Now let us find out then this stagnation point, where are the stagnation

point, where v_θ is 0, where are the stagnation point; that means, V_θ is 0; if we put here we get $\sin \theta$, then we do not get θ is equal to 0, then we get $\sin \theta$ is equal to $\frac{\Gamma}{4\pi a u}$, now they are may appear, now Γ then we get $\sin \theta$ is equal to here if we keep it here.

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So, they are may appear three condition, when $\frac{\Gamma}{4\pi a u}$ less than 1; it may appear $\frac{\Gamma}{4\pi a u}$ is equal to 1 and they are may case $\frac{\Gamma}{4\pi a u}$ greater than 1. Now it is less than 1; that means, it will occur on this cylinder surface, because $\sin \theta$

is define for less than 1 and it will displaced up; that means, in that case, in this is the case when $\gamma \text{ by } 4 \pi u$ less than 1.

So, the stream lines will be like this. So, this will be this stagnation point. So, this will be this stream line. So, these are these stagnation points, this are this stagnation point. This is $\gamma \text{ by } 4 \pi a u$ less than 1, when $\gamma \text{ by } 4 \pi a u$ is 1; that means, $\gamma \text{ by } 4 \pi a u$ is equal to 1, then this stream function, stream lines is like this. Then this stagnation point, just margins here at $\pi \text{ by } 2$ line here x and y. So, this will be the stream lines, this will be the direction of this stream lines so this is the stagnation. But $\gamma \text{ by } 4 \pi a u$ greater than 1 gives an impossible case for $\sin \theta$; which means, physically that the stagnation point is never occur, is never occurs on this cylinder surface; that means, in that case there is no stagnation point in the cylinder surface, the flow velocity is like this and this stagnation point in that case, this is this stagnation point; in that case, this will be this stream lines pattern.

So, this is the case when in $\gamma \text{ by } 4$ three situation are their greater than 1. So, stagnation point will not occur on this cylinder surface, this is the case $\gamma \text{ by } 4 \pi u$ is equal to 1 and $\gamma \text{ by } 4 \pi a$ less than 1; sorry this is the case when, this is less than 1, sorry this is the less than 1. So, three distingue cases are there, the pattern of stream line depending upon the values of $\gamma \text{ by } 4 \pi a u$ is less than 1, that is stagnation points on the cylindrical surface it is lifted up; then it is equal to 1 it is at this point and it is greater than 1 and this source a stagnation point will not be occurring on the cylindrical surface. So, today I have to end here; so next time I will just complete it another part, that the velocity distributions and the pressure distribution for this type of flow, that is the combination of rectilinear flow the doublet and the irrotational vertex.

Thank you.