

DC Power Transmission Systems
Prof. Krishna S
Department of Electrical Engineering
Indian Institute of Technology, Madras

Lecture - 63
Design of single tuned filter: Part 1

In the last class we were trying to see the requirement of a filter because of the problems of harmonics. So, we will study very simple design of what is known as a single tuned filter.

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Single Tuned Filter

$\frac{1}{C}$
 \downarrow
 L
 \downarrow
 R

$\delta = \frac{\omega_k - \omega_{ho}}{\omega_{ho}}, \omega_{ho} = \frac{1}{\sqrt{LC}}$
 $G_f + \left(B_f + \sqrt{\frac{L}{4s}} \right)^2 = \left(\sqrt{\frac{L}{4s}} \right)^2$
 $\delta_{min} \leq \delta \leq \delta_{max}, \delta_{max} > 0$

B_f
 G_f
 $\delta = \delta_{max}$

So, as the name suggests single tuned filter is designed for minimizing one particular harmonic frequency. So, single means one frequency. So, it is tuned for one harmonic frequency. So, it is a series combination of a capacitance, inductance and resistance C, L, R. So, we saw that there are some situations where the values of L and C chosen may not meet

the requirement. So, the that is actually quantified by defining a quantity called delta. So, the original definition of delta is $\omega_h - \omega_{h0}$ divided by ω_{h0} .

So, ω_h is the actual angular frequency sorry, ω_h is the angular frequency ω_{h0} by definition is $1/\sqrt{LC}$. So, let me rewrite that particular equation. So, I will not go through all the steps. The last equation that we got was $G^2 f^2 + B f + \sqrt{C/L} = 1/4 \Delta^2$ whole squared is equal to $\sqrt{C/L} = 1/4 \Delta^2$ whole square ok.

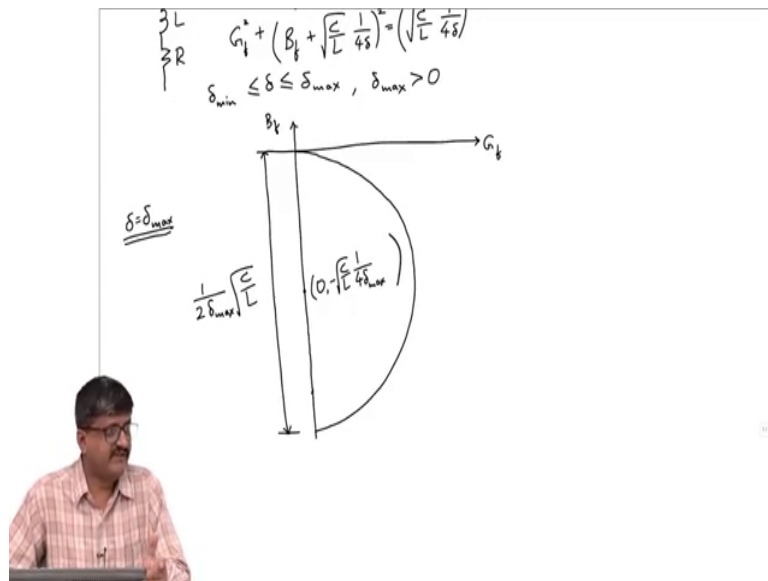
So, for a given value of delta, this appears to be I mean; this actually an equation of a circle in the complex plane with on the real axis I have $G f$, on the imaginary axis I have $B f$ ok. Now, if you look at delta, delta actually lies in a range, Δ_{min} is the lower limit and Δ_{max} is the upper limit ok. So, delta is within a certain range. Suppose, I take Δ_{max} Δ_{max} is greater than 0.

Now, if I try to plot the curve given by this equation in this plane where I have an one axis $G f$ and the other axis is $B f$. Now, when it comes to showing the where I mean the graph of this equation. So, for what I will do is, I will try to take delta equal to Δ_{max} . See there are two extreme values of delta Δ_{min} and Δ_{max} I mean two extreme values of Δ_{min} and Δ_{max} these are the worst case values.

So, I will take the one on the higher side Δ_{max} . So, if delta is equal to Δ_{max} which is greater than 0, then this is an equation of a circle ok. But one thing to notice I mean let me take the circle. So, this centre of the circle is $-\sqrt{C/L} = 1/4 \Delta$ so, it lies on the $B f$ axis. And the radius is $\sqrt{C/L} = 1/4 \Delta$ ok.

So, it appears as if the circle is in the third quadrant and fourth quadrant, but $G f$ is positive. So, $G f$ is positive to be more precise $G f$ is non negative; $G f$ is non negative ok. So, what I can do is I mean I can just show the relevant part of the circle which is just a semicircle.

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So, if I take this length, so this length is the diameter of the circle. So, the diameter of the circle; please note I am trying to consider one particular value of delta which is delta max. So, this is 1 by 2 delta max under root C by L so, this is the diameter. Radius is root C by L 1 by 4 delta max.

So, the centre of the circle is somewhere here. So, centre is 0, the value of G f is 0 there at the centre and the value of B f is minus root C by L 1 by 4 delta max. So, C and L are positive, we are taking the positive square root and there is a minus sign and delta max is positive. So, the filter admittance at the harmonic frequency it should lie at some point on the semicircle that is the point.

So, we have to design the filter. So, we do not have the exact value of G f or B f may be that is how is designed. So, getting the value of R L and C or in other words getting value of G f

and B f is designed. Now, for the sake of filter design, what we will do is; we will consider an equivalent circuit.

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Design of Single Tuned Filter

I_h (Current Source) \parallel Y_{fh} (Filter Admittance) \parallel Y_{nh} (Network Admittance) \rightarrow V_h (Voltage)

Converter Filter Network
 The objective is to minimize V_h

$$V_h = \frac{I_h}{|Y_{fh} + Y_{nh}|}$$

The quantities not under the control of filter designer are chosen pessimistically
 i.e. to maximize V_h or minimize $|Y_{fh} + Y_{nh}|$

Network admittance

susceptance

conductance

Net admittance angle is between $-\phi_m$ and ϕ_m

So, let us do the design of single tuned filter. So, the model considered here is for the converter, we just take the harmonic frequency which has to be minimized. So, the harmonic is in the current. So, the converter is represented by a current source, I mean; it has a current source I_h . Then there is a filter which is represented by an admittance and there is a network, the external network see this network is the network on the AC side ok.

So, I have converter here represented by a current source, I have between the network and the converter, there is a filter represented by an admittance and this is the network ok. So, let the admittance of the filter. So, we have already given a notation for this, the admittance of the filter at the harmonic frequency for which it is designed is Y_{fh} .

And let the admittance of the network Y_n , n for network and since it is at the harmonic frequency Y_{nh} . So, the current that actually flows through the filter has a magnitude say I_{fh} . And the voltage across the converter or filter or network at the harmonic frequency has a magnitude say V_h by magnitude I mean the RMS value ok.

Now, when we want to design something of course, we try to take some parameters and try to minimize or maximize a few quantities you know. So, that is what is all about design of one of the parameters I mean one of the quantities that we minimize is of course, cost. See when it comes to design there are two things that matter our performance and cost. So, we need to somehow have good performance at the same time we want a least cost, which we will get that performance ok.

Now, when it comes to performance; the objective is to minimize, see please note the converter has a harmonic current source I_h . So, due to the converter there is a harmonic current. Now, if that should not affect the network, then it means V_h ; V_h is the effect of I_h . See if I_h is not there only fundamental is there then V_h is 0. See V_h means it is the RMS voltage at the harmonic frequency. So, if only fundamental is there V_h is 0.

So, essentially we want to minimize V_h , the objective is to minimize V_h . So, what is V_h ? So, if I look at the expression for V_h , I can write V_h as the converter current I_h divided by the admittance of the parallel combination of filter and network. See V_h is the voltage across network or filter or converter. So, I can write this as I_h divided by the magnitude of Y_{fh} plus Y_{nh} .

Say when I have two admittance in parallel the affective admittance in some of the admittances ok. The magnitude of the admit affective admittance into the magnitude of the current gives mag into magnitude of the voltage gives the magnitude of current ok. So, now, let us see how this Y_{nh} takes values. So, network admittance.

So, when I take network admittance, that is Y_{nh} . So, again I take the complex plane. So, the complex plane the real part is the conductance of the network admittance and the imaginary

part is the susceptance. Now the question is where will this network admittance lie which quadrant or which quadrants? It is possible to have values in all the 4 quadrants.

Student: (Refer Time: 12:08).

First and?

Student: Second.

Second.

Student: Sorry first and forth.

First and forth because. So, conductance is?

Student: (Refer Time: 12:19).

Positive ok. Now, susceptance can be positive or negative now why?

Student: Mostly inductor.

Now, if it is only inductive then where it will lie?

Student: Forth.

Forth, but the network consists of transmission line transformers. If we take transmission line, it is not just inductive there is a shunt conductance also. So, there is a shunt sorry not shunt capacitance as well. So, whenever there is a capacitance, there is a possibility of positive susceptance. So, it can lie in the first quadrant and the fourth quadrant.

So, it does not lie in the entire first or fourth quadrant, it can be shown that this lies in this sector. So, there are two straight lines passing through the origin. So, if I take the intersection of the areas to the right of these two straight lines, then the network admittance will lie in this area. So, this angle is called ϕ_m . Similarly, the angle here is also ϕ_m . So, there are 2 straight lines make an angle of ϕ_m with respect to the conductance axis. So, it is an infinite region.

So, essentially the network admittance is having a phase having an angle which is between minus ϕ_m and plus ϕ_m . So, network admittance or in fact, impedance both have the same phase angle, see both have the same phase angle range ok. One is the reciprocal of the other. So, network admittance angle is between minus ϕ_m and plus ϕ_m ok.

So, we just saw that the objective is to minimize V_h as far as the performance is concerned. Now, when we try to minimize V_h , please note what is and under the control of the designer. So, when I say design of single tuned filter, the only values which the designer will decide are?

Student: $L C$; $L C$.

$L C$ and R , nothing more than that ok. When it comes to network; the designer has no control over the network. Designer has of course, has no control over I_h , I_h is known we know what is the harmonic current in the converter ok. So, when it comes to the quantities which are not under the control of the designer, but they are not fixed as well, they keep varying. Then one has to choose a value many a times, so we cannot just take the range as it is for some of the quantities. We have to take 1 particular value ok. So, if that quantity which is not under the control of the designer is within a range, which value do you take?

Student: The one which corresponds to the most usual case.

That is a one possible answer. Do you do that will you talk? Student: Worst case.

When you design, always design for worst case. So, when it comes to I mean maximizing performance, you want to see that it performs very well even in the worst case ok. So, worst case is something which is chosen if you have the performance in mind. So, right now, I am talking about performance ok. So, objective is to minimize V_h means it is somehow maximizing performance. So, we take the worst case for all the quantities which are not under the control of the designer, but with which vary over a certain range ok.

So, the quantities not under the control of the designer; designer means just filter designer. So, we are not doing any other design, only filter design filter designer are chosen pessimistically; that means, we are choosing the worst case pessimistic. So, that means, to maximize V_h . So, see our objective is to minimize V_h , pessimistically means? Ok, I will remove the comma here to maximize V_h .

So, maximizing V_h is actually equivalent to minimizing the denominator in the expression for V_h , for a given I_h is constant ok. So, here what I am trying to say is Y_{nh} , I have not given the value of Y_{nh} . Y_{nh} , I have just said it lies somewhere in the first quadrant or fourth quadrant, I have shown the region also. So, which value to be taken in order to design ok. So, to maximize V_h or minimize the absolute value of Y_{fh} plus Y_{nh} .

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$V_k = |\vec{Y}_{fh} + \vec{Y}_{nh}|$

The quantities not under the control of filter designer are chosen pessimistically
 i.e. to maximize V_k or minimize $|\vec{Y}_{fh} + \vec{Y}_{nh}|$

To minimize $|\vec{Y}_{fh} + \vec{Y}_{nh}|$ for a given \vec{Y}_{fh}

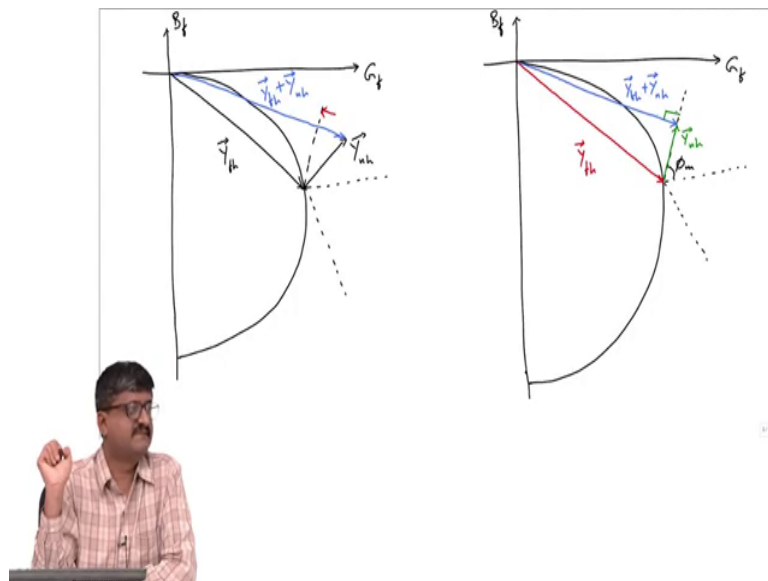
- ① The angle of \vec{Y}_{nh} should be ϕ_m
- ② The magnitude of \vec{Y}_{nh} should be such that $\vec{Y}_{fh} + \vec{Y}_{nh}$ is perpendicular to the boundary at which angle of \vec{Y}_{nh} is ϕ_m .

Net admittance angle is between $-\phi_m$ and ϕ_m



So, if I want to do this. So, let us say how to minimize this, how to minimize the absolute value of Y_{fh} plus Y_{nh} ? Now, what I will do is, we will try to take the worst case of Y_{nh} , but Y_{fh} is yet to be designed. Now, suppose I take the worst case for Y_{nh} for a given value of see please note we have not yet decided Y_{fh} . So, for a given Y_{fh} , I will take this next page.

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So, G_f this is B_f , so I have this semicircle ok. So, Y_{fh} is given; that means, this Y_{fh} first of all should lie on this semicircle. So, it is somewhere on the semicircle. We do not know where it is. So, let us assume that a some value is given. So, if Y_{fh} is given suppose, this is Y_{fh} ok; this is Y_{fh} . Please note G_f and B_f are real and imaginary parts of Y_{fh} .

Now, to this, I have to add Y_{nh} . Now what I will do is; I will just take this region see the network admittance is lying in the first or fourth quadrant. So, I will take the origin of this network admittance and shift it to this point Y_{fh} . So, that is essentially saying that so, to Y_{fh} I am adding Y_{nh} . Suppose, Y_{nh} ; I have to take between these two these dashed line which makes an angle ϕ_m and another dashed line which makes an angle minus ϕ_m .

Suppose, I take Y_{nh} to be this ok, then Y_{fh} plus Y_{nh} . So, I will try to use different colour so, that it will not cause confusion. So, this blue complex number is Y_{fh} plus Y_{nh} . So, my

intention is for a given Y_{fh} , I should minimize Y_{fh} plus Y_{nh} magnitude, magnitude of Y_{fh} plus Y_{nh} .

So, is it clear that Y_{nh} should be on the boundary? See the boundary is this dashed line and it should be on the boundary which makes an angle ϕ_m with respect to the conductance axis, not the minus ϕ_m . See what I am trying to say is; is it clear that it should lie on this boundary.

Student: Yes.

Ok, but where at which point on this boundary, this is I mean school geometry. I have to take a point on this line which is having the shortest distance from the origin.

Student: Passing that G_{fs} where it cuts (Refer Time: 22:18).

Is it?

Student: Draw perpendicular.

Drop a perpendicular. See I have a point I have a straight line, I want the point on the straight line which is having the minimum distance with from the given point. So, I have to drop a perpendicular from that point to the straight line that is all ok. So, it is essentially like this ok, let me re draw it. So, suppose this is Y_{fh} .

Now, in order to find the least magnitude of, I mean; in order to find Y_{nh} of that it results in least magnitude of Y_{fh} plus Y_{nh} , what I should do is; first drop a perpendicular from the origin to the boundary which makes an angle ϕ_m ok. So, the boundary is this which makes an angle ϕ_m . So, that should give the least value of the magnitude of Y_{fh} plus Y_{nh} yes.

Student: Sir if Y_{nh} is 0 then (Refer Time: 24:41).

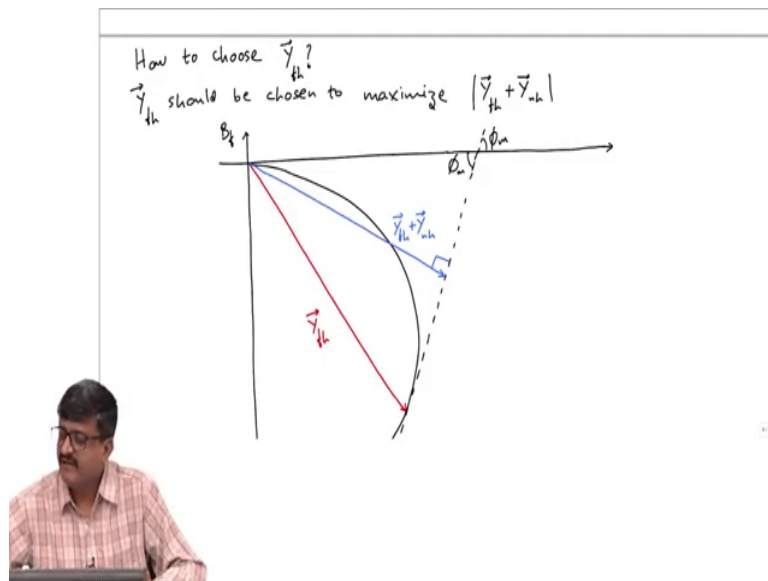
If Y_{nh} is 0.

Student: (Refer Time: 24:44).

Then it will result in least magnitude of Y_{fh} plus Y_{nh} . See we are adding two complex numbers, Y_{fh} and Y_{nh} . So, we want to minimize the absolute value of this sum of the two complex numbers. So, if Y_{fh} itself, see it is possible that I can have the sum of these two complex numbers smaller in magnitude compared to the just the magnitude of Y_{fh} ok.

So, I can choose the Y_{nh} in order to get a value which is smaller than Y_{fh} . So, if this is Y_{fh} blue complex number is Y_{fh} plus Y_{nh} and the red 1 is Y_{fh} so; that means, the difference between these two is Y_{nh} . So, if I take this is Y_{nh} . So, here this sum of Y_{fh} and Y_{nh} is perpendicular to this boundary which makes an angle ϕ_m , right ok. Now, please note what we have done here is chosen the value of Y_{nh} pessimistically, that is a worst case value.

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Now, how to choose Y_{fh} ? Now, Y_{fh} is under the control of the designer, how to choose Y_{fh} ? How to choose Y_{fh} ? Yeah as far as the performance is concerned I want to maximize the performance that is minimize the value of V_h or its essentially saying mini maximize the value of the denominator in the expression for V_h .

So, how to choose Y_{fh} ? See in the previous case for some arbitrary value of Y_{fh} we know how to choose Y_{nh} . Now, how to choose Y_{fh} itself. I do not think, I am asking a very tough question. See Y_{nh} is not under the control we take worst case, Y_{fh} is under the control of the designer, so we take the best case. So, how to get the best case? Worst case means; the one with that minimizes the absolute value of Y_{fh} plus Y_{nh} .

So, the best case is the one that maximizes the absolute value of Y_{fh} plus Y_{nh} . So, Y_{fh} should be chosen to maximize Y_{fh} plus Y_{nh} , absolute value ok. Now, how should I choose

Y_{fh} ? So, please note in the previous the last figure that I got Y_{fh} was taken to be some arbitrary value. Now, the question is how to take this? So, how to find Y_{fh} which actually maximizes the absolute value of Y_{fh} plus Y_{nh} . See the same rule holds as far as Y_{nh} is concerned.

So, when it comes to Y_{nh} ok. So, let me summarize how I have chosen Y_{nh} . To minimize Y_{fh} plus Y_{nh} for a given Y_{fh} what I should do is the angle of Y_{nh} should be ϕ_m . Then, the magnitude of Y_{nh} should be such that; should be such that; Y_{fh} plus Y_{nh} is perpendicular to the boundary.

So, perpendicular to the boundary means; which boundary there are two boundaries, there are two boundaries; one which corresponds to the angle of the admittance being equal to ϕ_m . So, the boundary at which I you are answering the other question ok. So, the boundary at which angle of Y_{nh} is ϕ_m . So, that is how we chose Y_{nh} . So, we still maintain this method of choosing Y_{nh} , but how to choose Y_{fh} is the question now.

Again we have the objective here the objective is to maximize Y_{fh} plus Y_{nh} yeah. Any answer? How to choose Y_{fh} ? Now first I have to choose Y_{fh} from then I can show Y_{nh} . Once I know Y_{fh} then, I know how to choose Y_{nh} that is what we discussed just now, but the question is how to choose Y_{fh} in order to satisfy this objective, maximize the magnitude of Y_{fh} plus Y_{nh} .

Student: (Refer Time: 31:57).

See one point to notice this complex number Y_{fh} plus Y_{nh} is always perpendicular to the boundary, is always perpendicular to the boundary. Now, as the boundary goes further from the origin, we get a higher value of the absolute value Y_{fh} plus Y_{nh} . So, what is the maximum distance to which the boundary can move, so that I get a maximum value of this magnitude Y_{fh} plus Y_{nh} ?

Student: (Refer Time: 32:44) and this is tangent to (Refer Time: 32:46).

When it when the when the boundary is tangent to the semicircle.

Student: Semi circle.

Is that clear? Is that obvious or not? Simple I mean; simple geometry nothing more than that. So, once the rule is fixed for using Y_{nh} , it should be always the sum of these two complex number is Y_{fh} plus Y_{nh} should be always perpendicular to the boundary. So, I have to choose the position of the boundary itself such that it this perpendicular distance is maximized ok.

So, that means; I have to choose the boundary perpendi I mean which choose the boundary as a tangent to the semicircle. So, of course, there are many many tangents, I mean which see tangents can be taken anywhere. So, which tangent has to be taken.

Student: Y_{fh} which tangent following that Y_{fh} which (Refer Time: 33:49).

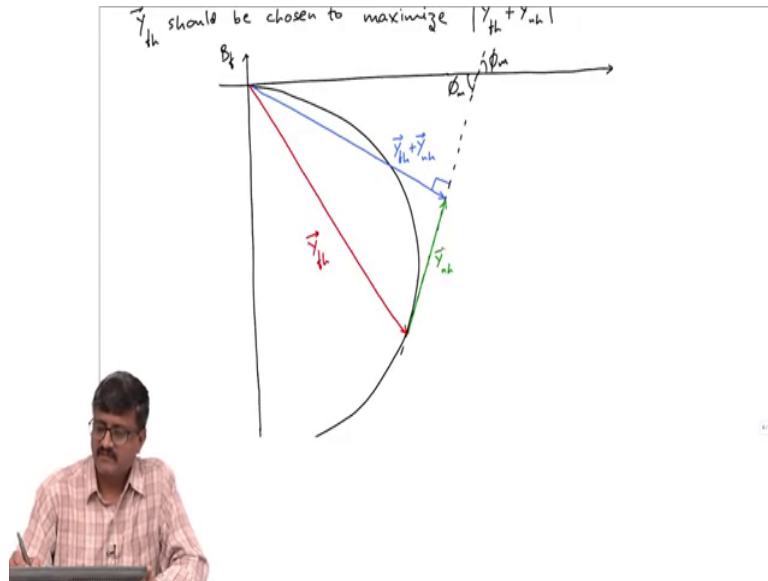
Y_{fh} makes yes. So, the boundary should make an angle ϕ_m with respect to the G_f axis ok. So, if I extend this tangent, so it intersects G_f and it makes an angle ok, let me show this. So, first I should take the tangent. So, the tangent should be the one which is chosen like this. So, what is this angle?

Student: ϕ_m .

ϕ_m , this is ϕ_m . See, the idea is very clear here. If I take this angle this is ϕ_m . So, this is also ϕ_m . yeah I chosen the tangent. Now, where is Y_{fh} ? It is point common to the semicircle and the tangent. So, what I used red, so, I will show Y_{fh} . So, this is Y_{fh} ok, then getting Y_{fh} plus Y_{nh} is very simple drop a perpendicular from the origin to this boundary that is all.

So, I have used what colour blue. So, just drop a perpendicular. So, this will give Y_{fh} plus Y_{nh} . So, once I know Y_{fh} plus Y_{nh} and also Y_{fh} I can find easily what is Y_{nh} . So, this is the worst case value of Y_{nh} that I am taking green. So, this is Y_{nh} ok.

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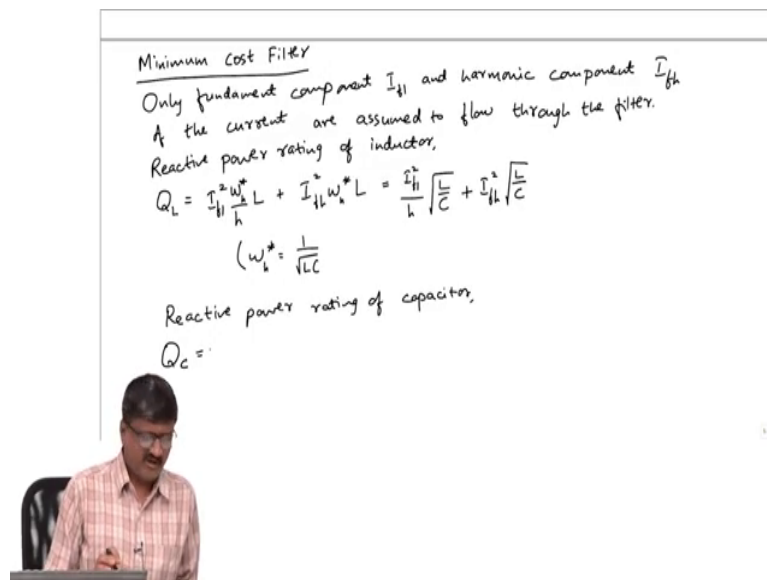


Now, please note just by choosing Y_{fh} will not give me the values of the parameters of filter, there are three parameters of the filter; R , L and C ok. Y_{fh} will give me only two parameters. So, essentially I am not getting the parameters of the filter see Y_{fh} will give me what is G and what is B_f . It will not give me what is the resistance, what is inductance, what is capacitance, it is still not given me. So, see please note even if you take impedance, if I know the resistance and the effective reactance it does not mean I know what is L and what is C . I just know what is X which is ωL minus 1 by ωC that is all.

I still do not know what is L what is C. Now, there are infinite values of L and C which can be chosen to get a effective x for a given value of effective x. So, the same thing is here. So, just by knowing the value of Y fh, I do not have the parameter values. So, how to get the parameter values? So, so far we considered performance. So, these are the things which have to be done in order to meet the performance or maximize the performance.

Now, we will see how to actually do further design, I mean; we are not completed the design see design is completed only when we have the value of R L C ok.

(Refer Slide Time: 38:33)



Minimum Cost Filter

Only fundamental component I_{f1} and harmonic component I_{fh} of the current are assumed to flow through the filter.

Reactive power rating of inductor,

$$Q_L = I_{f1}^2 \frac{\omega^*}{h} L + I_{fh}^2 \omega^* L = \frac{I_{f1}^2}{h} \sqrt{\frac{L}{C}} + I_{fh}^2 \sqrt{\frac{L}{C}}$$

$$(\omega^* = \frac{1}{\sqrt{LC}})$$

Reactive power rating of capacitor,

$$Q_C =$$

So, for that, we will minimize the cost and get the values of R L and C, minimum cost filter ok. Now, when it comes to the filter, what is the, what are the frequencies that will flow

through the filter? What is the frequency of the currents that will flow through the filter? It is designed for?

Student: (Refer Time: 39:10).

A particular harmonic frequency I_h , I_h will flow then, any other current will flow. Actually, it is not I_h please note we have used a different notation here I has to be careful while see if you look at this figure the current through the filter is not I_h the current through the converter is I_h , the current through the filter is I_{fh} ok. So, the two are not same ok, I_{fh} is a current which will flow through the filter. Any other current any other harmonic current will flow.

Please note, it may not offer infinite impedance to other frequency though it is very large impedance to other frequencies, it is not infinite so, it may flow. So, what about fundamental? It will not offer even infinite impedance to fundamental frequency also, but in practice what happens is; the harmonic current for which it is designed will flow in addition to that the fundamental will be significant. Whereas, the other harmonics for which it is not designed, I mean; there the magnitude of the current will be negligible.

So, then the significant components of the current that will flow through a filter are the harmonic frequency current for which it is designed and the fundamental. The remaining harmonics I mean the filter will offer a very large impedance. So, it is insignificant. So, we will make an assumption that only fundamental component. So, I will use a notation I_{f1} , f for filter 1 for fundamental.

Please note this fundamental component is not the fundamental component of current through the converter, this is the current through the filter. Only the fundamental component I_{f1} and harmonic component I_{fh} of the current are assumed to flow through the filter. Now, when it comes to cost, cost is dependent on what? If you take any electrical equipment, can I say the cost is almost proportional to one particular rating of that equipment. What rating?

Student: (Refer Time: 42:02).

Let me take for example, transformer. If I say the cost is proportional to some rating of the transformer, what rating? Voltage rating, current rating.

Student: (Refer Time: 42:13).

It is volt ampere rating, it is actually volt ampere rating. Now, when it comes to filter, what rating? Again so, filter is having electrical equipment it is again the volt ampere rating. Now, when you if you see the filter it is essentially L and C, R is something which comes for some reason. So, R is not a very significant part of the filter. So, it is only L and C, when it comes when it has only L and C, there is only reactive power.

So, it is proportional to the reactive power rating. The cost of the filter is proportional to the reactive power rating. So, what is the reactive power rating? So, there is an inductor there is a capacitor. So, let us try to take the reactive power rating of the inductor and capacitor separately, reactive power rating of inductor. So, I will use a notation for this Q_L , L for inductor.

So, can I get an expression for the reactive power rating? See we have made some assumptions that we are neglecting the other harmo harmonic components. So, only I_{f1} and I_{fh} flows ok. So, there is only the fundamental current and the harmonic current for I mean for which the filter is designed. So, based on this, can we get an expression for the reactive power. Now, please note reactive power is something which is difficult to define in the presence of, see reactive power has a well known definition in the I mean when there is only fundamental component.

Of course, there have been attempts to generalize the definition of reactive power in machine theory they use I mean the Perkins transformation can be used. But, when it comes to steady state, there are attempts to give other definitions. One particular definition is the one given by a person called Budeanu. I do not know if you have studied power quality, you may and how many of you studied power quality. Have you heard of this Budeanu's definition of reactive power?

Student: Yes.

There are many other definitions Budeanu is one particular. So, he I mean there are many ways in which we can define reactive power. So, one of them is Budeanus definition. So, what is the reactive power according to Budeanu in this case? What will, what is that in that particular definition? You take each frequency find the reactive power and add them that you say that is the total reactive power, that is what is the Budeanu's definition ok.

So, if I take only the fundamental and harmonic, there are only two when it comes to filter there is only the fundamental and harmonic, there are only two frequencies. So, find the reactive power for fundamental, find the reactive power for the harmonic frequency and add them. So, what is the reactive power corresponding to fundamental? See the current is $I f$. So, how do I get reactive power from current?

Student: $I f$ (Refer Time: 45:49).

No no I it is not necessary to get into complex

Student: $I f$ square.

$I f$.

Student: Square (Refer Time: 45:55).

Yeah $I f$ square into, into reactance. The square of the current into reactants gives reactive power right ok. So, what is the reactance? Now please note we are calculating the reactance depends on frequency. So, we are calculating at fundamental. So, what is the fundamental reactance?

Student: (Refer Time: 46:18) 1.

In terms of the quantities that we have used.

Student: Ok.

L is the inductance ok.

Student: Yeah.

There is inductance L, what is fundamental angular frequency?

Student: $1/\sqrt{LC}$.

We have not used any specific value of frequency. Using the notations that we have used. We have used notations ω_h divided by ω . See ω_h is the harmonic frequency for which the filter is designed divided by ω , this is the fundamental, is that is that plus, now please note I am just taking the ideal value of ω_h . So, ideal value is ω_h . So, in practice ω_h will deviate. So, because of that the reactive power rating will slightly be within a band. So, I am I am trying to take the ideal value of the frequency and compute the reactive power.

Then if I take the harmonic frequency it is $I^2 \omega_h^2$ into reactance. So, in this case it is ω_h into L ok. Now this can be written as $I^2 \omega_h^2$ by ω_h , ω_h is $1/\sqrt{LC}$, $I^2 \omega_h^2$ is I^2 by \sqrt{LC} . ω_h is $1/\sqrt{LC}$. So, please note ω_h is $1/\sqrt{LC}$. So, using this I can write this as $I^2 \omega_h^2$ by \sqrt{LC} , the first term. Similarly, the second term is $I^2 \omega_h^2$ into \sqrt{LC} .

Student: (Refer Time: 48:17).

Go back to.

Student: (Refer Time: 48:21).

So, we are doing a very simple design, this is a very simple design where we are ignoring the effect of chain variation in the inductance and capacitance, we are taking only one. So, if we consider that it will become even more complicated ok. So, similarly, I can define the reactive power rating of capacitor. So, reactive power rating of capacitor Q_c is a notation.

So, again I can use the Budeanu definition of reactive power and write the reactive power rating as sum of two reactive powers; one for fundamental, one for harmonic. So, I will stop here continue from this point in the next class then complete the design.