

DC Power Transmission Systems
Prof. Krishna S
Department of Electrical Engineering
Indian Institute of Technology, Madras

Lecture – 54
DC link control: Control variables

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The slide contains the following content:

Schematic Diagram: A DC link circuit connecting a rectifier on the left and an inverter on the right. The rectifier side has an AC source with RMS voltage E_r and turns ratio $T_r N_r : N_{2r}$. The DC voltage across the rectifier is V_{dr} and the current is I_d . The inverter side has an AC source with RMS voltage E_i and turns ratio $N_{2i} : N_{1i} T_i$. The DC voltage across the inverter is V_{di} .

Equations:

$$E_{Vr} = \frac{N_{2r}}{T_r N_r} E_r, \quad E_{Vi} = \frac{N_{2i}}{T_i N_{1i}} E_i$$

$$V_{dr} = E_{dr} - R_{cr} I_d$$

$$V_{di} = E_{di} - R_{ci} I_d$$

Equivalent Circuit: A circuit diagram showing the DC link with resistances R_{cr} , R_d , and R_{ci} . The DC voltage sources are E_{dr} and E_{di} .

$$E_{dr} = \frac{3\sqrt{2}}{\pi} n_b \frac{N_{2r}}{N_r} \frac{E_r}{T_r} \cos \alpha_r$$

$$E_{di} = \frac{3\sqrt{2}}{\pi} n_b \frac{N_{2i}}{N_{1i}} \frac{E_i}{T_i} \cos \gamma_i$$

Define: $A_r = \frac{3\sqrt{2}}{\pi} n_b \frac{N_{2r}}{N_r}$, $A_i = \frac{3\sqrt{2}}{\pi} n_b \frac{N_{2i}}{N_{1i}}$ $\Rightarrow E_{dr} = A_r \frac{E_r}{T_r} \cos \alpha_r$, $E_{di} = A_i \frac{E_i}{T_i} \cos \gamma_i$

So, this is the schematic diagram of the system. I have the rms value of line to line voltage of the AC bus on the rectifier side as E_r . And I have the turns ratio including the off nominal tap $T_r N_r$ is to N_{2r} and the rms value of the line to line voltage of the AC system bus on the inverter side is E_i and this is N_{2i} is to N_{1i} divide $N_{1i} T_i$.

So, the voltage at the DC bus on the rectifier side is V_{dr} , the current is I_d and the voltage at the DC bus on the inverter side is V_{di} . Now, we got some equations E_{dr} is a no; I mean

before that I will introduce a few things, E_{vr} is $N_2 r$ by $T r N_1 r$ into E_r . Similarly, E_{vi} the valve side voltage is equal to $N_2 i$ divided by $T i N_1 i$ into E_i .

So, we derived some relations V_{dr} can be written as E_{dr} minus did we derive this? We related V_{dr} E_{dr} i_d and R_{cr} minus R_{cr} I_d . Then we also derived the relationship between V_{di} E_{di} I_d E_{di} ?

Student: Minus R_c (Refer Time: 02:34).

Minus R_{cr} I_d ok. So, if we try to draw an equivalent circuit corresponding to these two equations, the last two equations. I have a voltage source in series with a resistance, the voltage source is E_{dr} ; the resistance is R_{cr} and the current is I_d .

Similarly, if I take the second equation and I call this voltage as E_{di} . Suppose, the voltage here is V_{dr} and the voltage here is V_{di} and the same current I_d flows here also, and corresponding to the line a transmission line suppose there is a resistance. So, let me call this resistance as R_d . So, if I have to satisfy the second equation what should be the resistance here?.

Student: Minus (Refer Time: 04:04).

Minus R_{ci} ok. So, if I have to please note this R_{cr} and R_{ci} are not actually physical resistances, there is no loss corresponding to R_{cr} and R_{ci} . Please note that they are due to leakage inductances, I mean if you look at the expression for R_{cr} and R_{ci} it is in terms of the leakage inductance or leakage reactance.

So, there is no loss corresponding to these two. So, we should not assume that there is a loss due to R_{cr} and there is a generation due to minus R_{ci} ok. So, the only loss is due to R_d R_d is the physical resistance, it is the resistance of the transmission ok. So, we got an expression for E_{dr} what is E_{dr} you recall E_{dr} 3.

Student: $3 \sqrt{2}$ (Refer Time: 04:59).

$2 \sqrt{2}$ by $\pi n b N_2 r$ by $N_1 r E_r$ by $T r \cos \alpha r$ is this ok? Did we derive this or not? See, I do not want to again go back to the ones which are already derived. So, how we derived this equation? Similarly, if I look at E_{di} no? No means I mean, maybe I would have.

Student: (Refer Time: 05:50).

I have written in terms of E_{vr} that is all. So, substitute the expression for E_{vr} . E_{vr} is $N_2 r$ by $\pi n b N_1 r$ into E_r that is all. So now, I am writing in terms of E_r instead of E_{vr} I am writing in terms of E_r . Similarly, E_{di} is $3 \sqrt{2}$ by $\pi n b N_2 i$ by $N_1 i E_i$ divided by $T i \cos \gamma i$. Now, if you look at this expression for E_{dr} or E_{di} you will note that $3 \sqrt{2}$ by $\pi n b$ is a constant $N_2 r$ $N_1 r$ are constants ok.

Similarly, in the expression for E_{di} , $3 \sqrt{2}$ by $\pi n b N_2 i$ $N_1 i$ they are all constants. So, I define a constant A_r , A is just a constant r subscript r means for rectifier as $3 \sqrt{2}$ by $\pi n b N_2 r$ by $N_1 r$. So, please note I put all the constants as 1 factor A_r that is all. So, then define one more constant A_i ; A is a constant i subscript i stands for inverter $3 \sqrt{2}$ by $\pi n b N_2 i$ by $N_1 i$.

So, if I make these 2 definitions then if you look at the expression for E_{dr} ; E_{dr} is A_r into E_r divided by $T r \cos \alpha r$ and E_{di} is equal to $A_i E_i T i \cos \gamma i$. Now, please note E_r is not a constant E_r is dependent on these AC system on the rectifier side. So, the voltage available on the AC system may change with time.

So, maybe at 1 point in time it has some rms value for the line voltage after a few hours it may change though way a small value. So, it is around nominal value, but it may slightly change. So, it is not a constant E_r is not a constant. Similarly, E_i is also not a constant. So, that is why I am not including that in the definition of A_r or A_i ok. Now come back to this circuit this is equivalent DC circuit.

So, if you look at the current in the circuit I_d , I_d can be written as the difference between the 2 voltage voltages of the sources E_{dr} and E_{di} divided by the effective resistance R_{cr} plus R_{ci} minus R_{ci} ok. So, I can write I_d as ok. So, in place of E_{dr} I will just straight away write the expression for E_{dr} just now I got the expression for E_{dr} $A_r E_r$ by $T_r \cos \alpha_r$ minus E_{di} is $A_i E_i$ by $T_i \cos \gamma_i$ I divided by the effective resistance is R_{cr} plus R_{di} minus R_{ci} .

Now, R_{cr} and R_{ci} will slightly depend on tap ok. But, if I ignore that variation in R_{cr} and R_{ci} due to the change in the tap position then the only variables that are there in the expression for I_d r. Sorry for the time being if I ignore the variations in R_{cr} and R_{ci} R_{cr} and R_{ci} are constants R_d is any how a constant A_r is a constant A_i is a constant.

So, E_r and E_i are something which depends on the AC system on the rectifier side and the inverter side. Then T_r is a control variable it is a tap. So, the user can decide the value of T_r the tap portion on load tap similarly the on load tap on the inverter side T_i is also a variable and there is another variable α_r the user can control α_r and γ_i is another variable which the user can control.

So, essentially there are four control variables. Now, please note there are two variable two more variables E_r and E_i . But, they cannot be controlled they depend on the system the AC system on the inverter side and the rectifier side. But, what can be controlled by the user or T_r , T_i , α_r and γ_i . So, four control variables.

So, the four control variables r T_r T_i α_r γ_i . Now, if you look at T_r and T_i they are the control variables due to the tap. So, if there are mechanical switches based tap then these are slow compared to α_r and α_r γ_i . Now, you know that I can use.

I mean a mechanical switch or a thyristor base switch. So, if you look at the power converter the electronics switches are thyristors which are very fast? See, hope you would have noticed that there is a large difference between a mechanical switch and a power electronic switch.

Mechanical switches are slow in operations you it may take a few seconds or at least a fraction of a second maybe, but to initiate the moment from on position to off position or off position on position. But, if you look at thyristor how many you know how many times in a second it can switches on a switches off? Take the converter 6 pulse line commutated converter any take any thyristor.

Student: 50 times.

50 times. It is now if you look at there are many other faster switches. In fact, so the slow switch that we are considering here the slow polytron switch itself is switching on and switching off 50 times. You can think about such a frequency of switching for mechanical switches. Imagine switching on and switching off the switch for 50 times in a second. No you cannot do that. It is not you are not just make mechanically use some automation to do it, you still cannot do ok.

There are limitations in the frequency and there are many other limitations of course, but the main point here is it is not fast. It takes some time to initiate and it is not as fast as the power electronics switches. So, essentially the among the 4 control variables 2 control variables are slow. So, it takes time to change the 2 control variables T_r and T_i because, they are based on the tap changing transformer control variables and which are based on the mechanical switches ok. So, T_r and T_i .

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$E_{vr} = \frac{N_{2r}}{T_r N_r} E_r$, $E_{vi} = \frac{N_{2i}}{T_i N_i} E_i$
 $V_{dr} = E_{dr} - R_{cv} I_d$
 $V_{di} = E_{di} - R_{ci} I_d$

$I_d = \frac{A_r \frac{E_r}{T_r} \cos \alpha_r - A_i \frac{E_i}{T_i} \cos \gamma_i}{R_{cv} + R_d - R_{ci}}$
 $E_{dr} = \frac{3\sqrt{2}}{\pi} n_b \frac{N_{2r}}{N_r} \frac{E_r}{T_r} \cos \alpha_r$
 $E_{di} = \frac{3\sqrt{2}}{\pi} n_b \frac{N_{2i}}{N_i} \frac{E_i}{T_i} \cos \gamma_i$

Define $A_r = \frac{3\sqrt{2}}{\pi} n_b \frac{N_{2r}}{N_r}$, $A_i = \frac{3\sqrt{2}}{\pi} n_b \frac{N_{2i}}{N_i} \Rightarrow E_{dr} = A_r \frac{E_r}{T_r} \cos \alpha_r$, $E_{di} = A_i \frac{E_i}{T_i} \cos \gamma_i$
 4 control variables: $T_r, T_i, \alpha_r, \gamma_i$
 Changing T_r and T_i are slow controls (5 to 6 s per step) since mechanical switches are involved.
 α_r and γ_i can be rapidly controlled in a fraction of a cycle (20ms for 50Hz)



So, changing this T_r or T_i are slow controls. So, it is essentially a changing the tap position from one step to another step. So, even if you want to change one step of the tap it takes 5 to 6 seconds per step. Because they are mechanical switches since mechanical switches are involved.

So, there are two slow variables and the α_r and γ_i can be rapidly controlled. α_r and γ_i can be rapidly controlled. So, here when we talk about controlling α_r γ_i we do not talk about the time required in terms of seconds.

It is a fraction of a cycle in fact. So, in a fraction of a cycle. So, cycle means if I take 50 Hertz it is 20 milliseconds. So, for 50 Hertz frequency it is 20 milliseconds. So, it is not of the order

of seconds it is of the order of 10s of milliseconds. So, it is much smaller and hence much faster.