

DC Power Transmission Systems
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Lecture – 42

6 pulse LCC with resistance, inductance and voltage source on the DC side: Part 2

(Refer Slide Time: 00:20)

$$A_1 = \begin{bmatrix} -L & 2L \\ 2L+L_d & -L \end{bmatrix}^{-1} \begin{bmatrix} R & -2R \\ -2R-R_d & R \end{bmatrix}, u_1 = \begin{bmatrix} -L & 2L \\ 2L+L_d & -L \end{bmatrix}^{-1} \begin{bmatrix} e_a - e_b \\ e_b - e_c - V_d \end{bmatrix}$$

$$2^{nd} \text{ subinterval}$$

$$(2R+R_d)i_d + (2L+L_d)\frac{di_d}{dt} + V_d = e_b - e_c$$

$$A_2 = -\frac{2R+R_d}{2L+L_d}, u_2 = \frac{e_b - e_c - V_d}{2L+L_d}$$

$$x_1\left(\frac{s}{\omega_0}\right) = F x_0\left(\frac{s}{\omega_0} + T_1\right) + G \rightarrow x_1\left(\frac{s}{\omega_0}\right) = \begin{bmatrix} i_d\left(\frac{s}{\omega_0}\right) \\ i_1\left(\frac{s}{\omega_0}\right) \end{bmatrix}, x_2\left(\frac{s}{\omega_0} + T_1\right) = i_d\left(\frac{s}{\omega_0} + T_1\right)$$

$$i_d\left(\frac{s}{\omega_0}\right) = i_d\left(\frac{s}{\omega_0} + T_1\right)$$

$$i_1\left(\frac{s}{\omega_0}\right) = i_d\left(\frac{s}{\omega_0}\right) = i_d\left(\frac{s}{\omega_0} + T_1\right) \Rightarrow F = \begin{bmatrix} 1 \\ 1 \end{bmatrix}, G = \begin{bmatrix} 0 \\ 0 \end{bmatrix}$$

I will write the expression for A 1. So, I will straight away write the expression, please check whether it is true minus L 2 L, 2 L plus L d minus L inverse into R minus 2 R, minus 2 R minus R d R. So, this is A 1, is this and of course, so u 1. So, u 1 is minus L 2L, 2L plus L d minus L inverse e a minus e b, e b minus e c minus V d.

So, if I want A 2 and u 2, I should consider the second sub interval of this 2 and 3 valve conduction mode. So, if I take the 2nd sub interval then I have an equivalent circuit; we just

shows only those elements that conduct on 0 current. So, 2 and 3 valves conduct. So, this is valve 3, this is valve 2. And I have R_d , L_d and V_d on the DC side $R_L R_L$.

So, I have e_b and e_c , the two voltage sources e_c . So, if I denote the DC side current by i_d , the equation that I get by applying Kirchhoff's voltage law is. So, there are 2 resistances with value R and 1 resistance R_d . So, $2R$ plus R_d into i_d plus $2L$ plus L_d into $\frac{di_d}{dt}$ plus V_d is equal to e_b minus e_c . So, if I write this in the standard form, I have $\frac{di_d}{dt}$ on the left hand side and the remaining terms on the right hand side.

So, I get A_2 as $-\frac{2R + R_d}{2L + L_d}$, I am straight away writing it. So, A_2 is nothing, but the coefficient of i_d when I write this equation in the standard form. See the standard form is the derivative of the state variable on the left hand side; that is $\frac{di_d}{dt}$ on the left hand side, rest of the terms on the right hand side. And u_2 is just the remaining term on the right hand side. So, that is e_b minus e_c minus V_d divided by $2L + L_d$. So, we have got everything except F and G .

So, if I want F and G then I have to relate state variables at the beginning of the first subinterval to the state variable at the end of the second sub interval. So, the 2 state variables or i_d . So, what are the state variable in the first sub interval i_d and?

Student: i_1 .

i_1 . Now in the second sub interval it is i_d . So, this is the general equation. So, if I take x_1 x_1 , the first element of x_1 is i_d . So, what is i_d at α by ω_o ? So, can I write it in terms of x_2 ? So, how to write it in this form? See, what I need to do is; I write, I have to write an expression for i_d and I have also have to write an expression for i_1 at α by ω_o .

Student: (Refer Time: 05:40).

No. So, how to get it in this form? See here, in this equation; x_1 at α by ω_o is nothing but, i_d at α by ω_o , i_1 at α by ω_o . So, that is x_1 at α by ω_o

i_0 and i_2 at α by ω_0 plus T_1 is, what? i_1 at α by ω_0 plus T_1 . Can I relate i_1 at α by ω_0 and i_1 at α by ω_0 plus T_1 ?

Student: (Refer Time: 06:30).

They are.

Student: Same.

Same, why?

Student: Because it is periodic.

i_1 is periodic with period T_1 . Say i_1 is a DC side current. So, the period of i_1 is T_1 . So, i_1 at α by ω_0 is same as i_1 at α by ω_0 plus T_1 then what about i_2 at α by ω_0 ok. Now can I relate i_2 at α by ω_0 and i_1 at α by ω_0 , I mean; why i_1 should do this becomes clear shortly, can I relate these 2?

Student: (Refer Time: 07:17) both are equal.

Hmm?

Student: (Refer Time: 07:23) at α by ω_0 i_2 is 0.

So, $i_2 = 0$, so.

Student: (Refer Time: 07:26).

They are equal right.

Student: Yes.

They are equal.

Student: Hm.

See α by ω_0 is the instant at which 3 is turned on.

Student: Yeah.

So, it just before 3 is turned on i_1 and i_d are same. So, just at the instant of turning on i_3 is 0. So, i_1 is equal to i_d . Now from the previous equation this is also equal to i_d by i_d at α by ω_0 plus T_1 . So, from this can I get F and G? So, from this I get F and G, both are of size 2 cross 1. So, what is F? What is G?.

Student: F is 1 plus 1.

F is?

Student: 1 1.

1 1, G is?

Student: 0.

So, G was actually not required in this case. Now why I use G is that is a general solution, so there are cases where G is non zero. So, that is why we need that G. So, far this case, G is actually not required at all because it is 0 ok. So, this is as far as 2 and 3 valve conduction mode is concerned. So, if this is clear we will move on to. See essentially we are trying to find $x_1, x_2, A_1, u_1, A_2, u_2, F$ and G that is all.

So, given any circuit, if I know these things I can go ahead and solve the equation get the lowercase T 1 and the solution ok. So, the solution can be obtained in a closed forms. So, we have an expression for the solution, but that requires the knowledge of T 1, the lower case T 1. So, that one can get only by solving a non-linear algebraic equation ok. If this is clear then we will consider the same circuit, but 3 and 4 valve conduction mode.

(Refer Slide Time: 09:18)

3 and 4 Valve Conduction Mode

1st Subinterval

$x_1 = \begin{bmatrix} i_d \\ i_1 \\ i_6 \end{bmatrix}, x_2 = \begin{bmatrix} i_d \\ i_1 \end{bmatrix}$

$Ri_1 + L \frac{di_1}{dt} + L \frac{d}{dt}(i_6 - i_d + i_1) + R(i_6 - i_d) = e_a - e_b$

$-R(i_6 - i_d + i_1) - L \frac{d}{dt}(i_6 - i_d + i_1) + L \frac{d}{dt}(i_d - i_6) + R(i_d - i_6) = e_b - e_c$

$R_d i_d + L_d \frac{di_d}{dt} = -V_d$

$A_1 = \begin{bmatrix} -L & 2L & L \\ 2L & -L & -2L \\ L_d & 0 & 0 \end{bmatrix}^{-1} \begin{bmatrix} R & -2R & -R \\ -2R & R & 2R \\ -R_d & 0 & 0 \end{bmatrix}$

$u_1 = \begin{bmatrix} -L & 2L & L \\ 2L & -L & -2L \\ L_d & 0 & 0 \end{bmatrix}^{-1} \begin{bmatrix} e_a - e_b \\ e_b - e_c \\ -V_d \end{bmatrix}$

So, again what we will first do is try to take the first sub interval and draw an equivalent circuit showing only those elements that conduct non zero current. So, there is one loop current i_d flowing through R_d , L_d , V_d and we consider one of the elements of x_1 as the current through the outgoing valve that is i_6 . So, i_6 becomes 0 at the end of the first sub interval and of course, the other current that I consider as a state variable is i_1 . So, the current

through valve 3 is i_d minus i_1 and the current through e b is suppose I showed this in this direction.

So, it is i_6 minus i_d plus i_1 . So, there are 3 loops and I have to apply Kirchhoff's voltage law to this 3 loops. So, x_1 is the state vector for the first time sub interval. So, I have to take i_6 of the last element of x_1 ok. So, the other two elements of x_1 are i_d and i_1 , i_d and i_1 . So, this also gives x_2 straight away. So, x_2 is same as x_1 without the last element; that is i_d i_1 . Of course, x_2 is applicable for the second sub interval.

So, let us apply the Kirchhoff's voltage law to the 3 loops; the first loop consisting of e a eb R L and the valves 1 and 3. So, it is $R i_1$ plus $L \frac{d i_1}{dt}$ plus $L \frac{d}{dt}$ of i_6 minus i_d plus i_1 plus $R i_6$ minus i_d plus i_1 . So, this is equal to e_a minus e_b , that is the first equation. Now if I apply Kirchhoff's voltage law to the loop consisting of e b, e c, R, L and the valves 2 and 6, then R into i_6 minus i_d plus i_1 .

Student: i_d minus.

Sorry.

Student: i_d minus (Refer Time: 14:33).

$T_1 i$ will go in this direction fine.

Student: (Refer Time: 14:44).

Then this is minus $L \frac{d}{dt}$ of i_6 minus i_d plus i_1 . So, if I take the current through valve 2 it is i_6 sorry, i_d minus i_6 plus $L \frac{d}{dt}$ of i_d minus i_6 , plus $R i_d$ minus i_6 . So, this is equal to e_b minus e_c . Then there is one more loop consisting of this valves 3, 6 $R_d L_d V_d$. So, by Kirchhoff's voltage law; $R_d i_d$ plus $L_d \frac{d i_d}{dt}$ is equal to V_d , is equal to. In fact, minus V_d .

So, I will leave it to you to write these equations in the standard form. See if I will repeat what is standard form standard form of the first order differential equation, see all these are first order differential equations. So, in the standard form we get the derivative of the state variables on the left hand side the remaining terms on the right hand side.

So, from that I get A 1 and u 1. So, I will straight away give the answer. So, please verify that; A 1 is minus L, 2 L, L, 2 L, minus L, minus 2 L, L d, 0, 0 inverse into A 1 is of size 3 by 3. R, minus 2 R, minus R, minus 2 R, R, 2 R and minus R d, 0, 0, this is A 1. And u 1 is the same of first factor that i is appearing in A 1; that is minus L, 2 L, L, 2 L, minus L, minus 2 L, Ld, 0, 0 inverse into ea minus eb, eb minus ec, minus Vd ok. Now, this is for the first sub interval.

(Refer Slide Time: 17:53)

2nd subinterval

$A_2 = A_1$ for 1st subinterval of 2 and 3 valve conduction mode

$u_2 = u_1$

$$x_1\left(\frac{k}{\omega_0}\right) = F x_2\left(\frac{k}{\omega_0} + T_1\right) + G$$

$$x_1\left(\frac{k}{\omega_0}\right) = \begin{bmatrix} i_d\left(\frac{k}{\omega_0}\right) \\ i_i\left(\frac{k}{\omega_0}\right) \\ i_c\left(\frac{k}{\omega_0}\right) \end{bmatrix}, \quad x_2\left(\frac{k}{\omega_0} + T_1\right) = \begin{bmatrix} i_d\left(\frac{k}{\omega_0} + T_1\right) \\ i_i\left(\frac{k}{\omega_0} + T_1\right) \end{bmatrix}$$

$$\left. \begin{aligned} i_d\left(\frac{k}{\omega_0}\right) &= i_d\left(\frac{k}{\omega_0} + T_1\right) \\ i_i\left(\frac{k}{\omega_0}\right) &= i_i\left(\frac{k}{\omega_0}\right) = i_i\left(\frac{k}{\omega_0} + T_1\right) \\ i_c\left(\frac{k}{\omega_0}\right) &= i_c\left(\frac{k}{\omega_0} + T_1\right) \end{aligned} \right\} \Rightarrow F = \begin{bmatrix} 1 & 0 \\ 0 & 1 \end{bmatrix}, \quad G = \begin{bmatrix} 0 \\ 0 \end{bmatrix}$$

NPTEL

If I want the second subinterval should I again try to get the equation. So, R I have already got this. See the second sub interval is nothing, but the first subinterval of 2 and 3 valve

conduction mode. So, I have already got x_2 x_2 is already written. What is A_2 and what is u_2 ? So, A_2 is equal to A_1 which was obtained for first subinterval of 2 and 3 valve conduction mode.

Similarly, u_2 is nothing but, the u_1 for the first subinterval of 2 and 3 valve conduction mode. So, the only things that remain are finding F and G . So, if I go by the general equation, x_1 by x_1 at α by ω o is equal to F into x_2 α by ω o plus T_1 plus G . So, now we have x_1 , what is x_1 at α by ω o ?

So, it is i_d at α by ω o , i_1 at α by ω o and i_6 at α by ω o . And the first time on the right hand side as x_2 at α by ω o plus T_1 . So, this is i_d at α by ω o plus T_1 and i_1 at α by ω o plus T_1 .

So, to get F and G what I should do is; take one element of x_1 at a time and try to get some relations. So, based on what happened in the first sub interval I can I say that i_1 i_d at α by ω o see based on sorry, what happened in the 2 and 3 valve conduction mode. So, what is i_d at α by ω o ?

Student: (Refer Time: 20:30) equal to i_d (Refer Time: 20:32).

i_d at α by ω o plus T_1 , because i_d is periodic with T_1 . Then the second element of x_1 is i_1 at α by ω o . So, that is again i_d at α by ω o . So, which is nothing but, i_d at α by ω o plus T_1 . Then finally, i_6 at α by ω o . So, what should this be what is i_6 at α ?

Student: (Refer Time: 21:14).

Student: (Refer Time: 21:15).

i_6 is 0 at α by ω .

Student: (Refer Time: 21:21).

Student: (Refer Time: 21:23).

It is not into i_1 at.

Student: (Refer Time: 21:26).

So, see i_1 and i_6 are identical except for a phase shift of 60 degrees which is nothing but T_1 .

Student: T_1 .

So it is i_1 at α by ω_0 plus T_1 . So, from these 3 equations can I say what is F . what is a size of F ?

Student: 3 cross (Refer Time: 021:47).

3 cross?

Student: 3 (Refer Time: 21:50).

Size of F .

Student: (Refer Time: 21:52).

3 cross 2, 3 cross 2. So, first row, what are the elements?

Student: 1 0.

1 0, second row?

Student: (Refer Time: 22:04).

1 0, third row?

Student: 0 1.

0 1. So, you we get everything in the first term itself. So, again when you look at G, what is the size of G?

Student: 3 cross.

3 cross.

Student: 1.

1. Size of G is same as $x \times 1$. So, it is same as this size of $x \times 1$ and all elements are 0. This general solution is something which will be very helpful and of course, 1 as to use a computer to solve for T 1 otherwise calculator cannot be used for solution of such non-linear equations, but there is before we using a computer there is 1 integration that you have to do manually. Please note there is an integration.

So, if you recall in the solution for the scalar T 1, lowercase T is the subscript 1 there is a non-linear equation involving an integral. So, only after simplifying this integral, you can solve the non-linear equation. Now, how to do the integration? See if that integration will involve u_1 and u_2 , see if you look at u_1 .

(Refer Slide Time: 23:14)

$u_1 = k_1 + l_1 \cos(\omega_0 t) + m_1 \sin(\omega_0 t)$
 $u_1, k_1, l_1, m_1 : (n+1) \times 1$
 k_1, l_1, m_1 are constants.
 $u_2 = k_2 + l_2 \cos(\omega_0 t) + m_2 \sin(\omega_0 t)$
 $u_2, k_2, l_2, m_2 : n \times 1$
 k_2, l_2, m_2 are constants.
 $\int e^{-A_1 t} u_1(t) dt, \int e^{-A_2 t} u_2(t) dt.$

$\sin(\omega_0 t + \phi)$
 $\sin(\omega_0 t) \cos \phi + \cos(\omega_0 t) \sin \phi$

NPTEL

Now, in general this u_1 depends on what is there on the DC side and what is there on the AC side. Now on the AC side, what you have is only sinusoidal voltage sources on the DC side you have either a constant current source or a constant voltage source. So, if you look at all the cases that we have considered so far, whether it is u_1 or u_2 . It is dependent on some constant or sinusoidal terms. Constant can be due to the DC side voltage source and the sinusoidal quantity can be due to the AC side voltage source.

Can I say that it is sum of 3 column vectors; where, the first column vector is a L_1 which is having the same size as u_1 let me say, k_1, k_1 which is having the same size of as u_1 , then $L_1 \cos \omega_0 t$ plus $m_1 \sin \omega_0 t$. In general, see many times you come across this expressions in terms of e, b, e, c .

So, you have this $\sin(\omega_0 t + \text{some angle } 150, 90, 150, 30 \text{ minus } 90)$. So, in general this can be written as $\sin(\omega_0 t) \cos \phi + \cos(\omega_0 t) \sin \phi$. Where, this $\cos \phi$ and $\sin \phi$ are constant because ϕ is a constant, but the other terms other factor $\sin(\omega_0 t)$ $\cos(\omega_0 t)$ are functions of time. So, what I am trying to say is I can in general write u_1 as a constant plus a constant factor times $\cos(\omega_0 t)$ plus a constant factor times $\sin(\omega_0 t)$. Can I do that? Because, I will get terms like $\sin(\omega_0 t + \phi)$.

Of course there is a coefficient to that which is a constant. So, that gets absorbed in this l_1 and m_1 . So, size of k_1 or L_1 or m_1 is same as that of u_1 ok. So, k_1, l_1, m_1 , so if I take k_1 . So, if I take either u_1 or k_1 or l_1 or m_1 . What is the size? What is the size of these? It is same as x_1 which is nothing but, $n \times 1$ cross 1 . Size of x_1 is $n \times 1$ we use the notation n for the size of x_2 . So, is this clear?

So, these are all constants k_1, l_1, m_1 are constants they are constant column vectors. Similarly if you take u_2 it can be written as $k_2 \cos(\omega_0 t) + l_2 \sin(\omega_0 t) + m_2$. So, again we are the size of u_2 , k_2, l_2 and m_2 are $n \times 1$ they are column vectors and k_2, l_2 and m_2 are constants.

So, when you look at that equation non-linear equation which has to be solved for that scalar T_1 . There are integrals of the type exponential of minus $A \tau u_1$, see there you come across this type of integral exponential minus $A_1 \tau, u_1$ of $\tau, d\tau$ exponential of minus $A_2 \tau u_2$ of $\tau, d\tau$ being integrated. So, these are the integrals that you are come across.