


DC Power Transmission Systems
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Lecture - 31


Analysis of 3 and 4 valve conduction mode of 6 pulse LCC: Part 3

So, in the last class we formed a table for 3 and 4 valve conduction mode. So, we got the expression for v_d and voltage across valve 1 for all the twelve subintervals. So, if I want to know the voltage jumps. So, here the purpose of knowing voltage jumps is to ensure that the thyristor valves are rated for the required dv by dt values. So, if I try to look at the. So, I will not again rewrite the table.

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Subinterval	Voltage across valve 1	Voltage jumps
α to $\alpha + u - 60^\circ$	0	
$\alpha + u - 60^\circ$ to $\alpha + 60^\circ$	0	$-\sqrt{\frac{3}{2}}V \sin(\alpha + u + 30^\circ)$
$\alpha + 60^\circ$ to $\alpha + u$	$-\frac{3}{2}e_b$	$\sqrt{\frac{3}{2}}V \sin(\alpha + 150^\circ)$
$\alpha + u$ to $\alpha + 120^\circ$	0	$\sqrt{\frac{3}{2}}V \sin(\alpha + u - 150^\circ)$
$\alpha + 120^\circ$ to $\alpha + u + 60^\circ$	$\frac{3}{2}e_a$	$\sqrt{\frac{3}{2}}V \sin(\alpha - 30^\circ)$
$\alpha + u + 60^\circ$ to $\alpha + 180^\circ$	0	$-\sqrt{\frac{3}{2}}V \sin(\alpha + u + 30^\circ)$
$\alpha + 180^\circ$ to $\alpha + u + 120^\circ$	$-\frac{3}{2}e_c$	$\sqrt{\frac{3}{2}}V \sin(\alpha + 150^\circ)$
$\alpha + u + 120^\circ$ to $\alpha + 240^\circ$	0	
$\alpha + 240^\circ$ to $\alpha + u + 180^\circ$	0	
$\alpha + u + 180^\circ$ to $\alpha + 300^\circ$	0	
$\alpha + 300^\circ$ to $\alpha + u + 240^\circ$	0	
$\alpha + u + 240^\circ$ to $\alpha + 360^\circ$	0	



So, I will just say what are the different sub intervals in which, I get the different expressions for voltage across valve 1 and directly write the expression for voltage jump. So, if I take


alpha to alpha plus u minus 60. So, there are many sub intervals where the voltage across valve 1 is 0.

So, we have in the first sub interval 0, second sub interval 0, third sub interval 0. Then in the fourth sub interval it is minus 3 by 2 e b. Then, 0 then, 3 by 2 e a; then, 0 then minus 3 by 2 e c, then 0, 0, 0, 0. So, if I want to know, what are the voltage jumps? So, you see that there are how many jumps 1 2 3 4 5 6 jumps. So, from here to here, here to here, here to here, here this one and finally this one. So, the expression for the 6 voltage jumps. So, I will directly write the expression.

So, what you need to do is, take the value of take the expression for voltage across valve 1 and substitute the appropriate value of omega o t. You will get a voltage jump. So, I need to take for example, the first voltage jump is minus 3 by 2 e b evaluated at alpha plus c. Then the second jump is 3 by 2 e b evaluated at alpha plus 120. So, if I try to take this expressions and substitute the appropriate values of omega o t. So, I will get these expressions or voltage jump minus root 3 by 2 V sin alpha plus u plus 30 degrees that is the first voltage jump. So, I will leave it to you to verify this.

The second voltage jump is sorry 3 by 2 V sin alpha plus 150 degrees, then 3 by 2 under root V sin alpha plus u minus 150 degrees. Then root 3 by 2 V sin minus sin minus root 3 by 2 V sin alpha minus 30 degrees; minus root 3 by 2 V sin alpha plus u plus 30 degrees. Then root 3 by 2 V sin alpha plus 150 degrees. Now, we also founded I mean a more detail table with a column for v d as well. So, from the column for v d which gives expressions for v d in the 6 in the 12 sub intervals; we can get the average value of v d. So, if I want to find the average value of v d.

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Average value of V_d is

$$V_d = \frac{3}{\pi} \int_{\alpha+u-60^\circ}^{\alpha+60^\circ} \left(-\frac{3}{2} e_c\right) d(\omega t)$$

$$V_d = \frac{\sqrt{3}}{2} V_{do} [\cos(\alpha-30^\circ) + \cos(\alpha+u+30^\circ)] \quad \text{--- (1)}$$

$$I_d = \frac{I_s}{\sqrt{3}} [\cos(\alpha-30^\circ) - \cos(\alpha+u+30^\circ)] \quad \text{--- (2)}$$

$$V_d = \frac{\sqrt{3}}{2} V_{do} [\cos(180^\circ - \gamma - u - 30^\circ) + \cos(180^\circ - \gamma + 30^\circ)]$$

$$V_d = \frac{\sqrt{3}}{2} V_{do} [-\cos(\gamma+u+30^\circ) - \cos(\gamma-30^\circ)]$$

$$I_d = \frac{I_s}{\sqrt{3}} [-\cos(\gamma+u+30^\circ) + \cos(\gamma-30^\circ)]$$

From (1) and (2),

$$V_d = \frac{\sqrt{3}}{2} V_{do} [\cos(\alpha-30^\circ) + \cos(\alpha-30^\circ) - \sqrt{3} \frac{I_d}{I_s}] = \sqrt{3} V_{do} \cos(\alpha-30^\circ) - \frac{3 V_{do} I_d}{2 I_s}$$

$$V_d = \sqrt{3} V_{do} \cos(\alpha-30^\circ) - 3 R_c I_d$$

So, it is denoted by upper case V with the subscript d. So, what I can do is, I can I know that V d repeats after every 60 degree. So, I have to just take the expression for V d for the first interval. So, in the first sub first sub interval it is 0. So, I have to just take the expression for V d in the second sub interval. So, it is 3 by pi which is reciprocal of 5 by 3. So, I am just taking for 6 degrees. So, in the second sub interval, which is from alpha plus u minus 60 degrees to alpha plus u sorry alpha plus 60 degrees. The expression for V d is minus 3 by 2 e c d omega o t.

So what you need to do is just substitute the expression for e c and integrate and leave it to you I will again leave it to you to verify that this is equal to root 3 by 2 V d o cos alpha minus 30 degrees plus cos alpha plus u plus 30 degrees. So, this is the expression for V d. Now in the last class; we got the expression for I d in terms of I s alpha and u if we recall we derived

this equation sorry just rewrite that equation. I_d is I_s by say of course, the last step I did not go through all the manipulations I am asking you to do that.

Yeah, by the way I just want to let you know, whatever I have asked you to do so far are all simple ones except the expressions for the fundamental and harmonic component in for the DC side voltage and the AC side current in the case of 2 and 3 valve conduction mode. So, only those are laborious, all others are I mean if something which can be done in just a few minutes ok. So, only if you look at the 2 and 3 valve conduction mode; the fundamental and RMS expression for the AC side current and the RMS value of the harmonic say the sorry, the fundamental and harmonic component RMS of the AC side current. And the RMS value of the harmonic of the DC side voltage these two are a bit laborious all others are straightforward ok.

So, one should be able to do it in just a few minutes. So, this is I_s by $\sqrt{3} \cos \alpha - \cos(\alpha + 30^\circ)$. So, what we do is, we try to again get this expressions for V_d and I_d in terms of γ instead of α . We have defined an angle γ , I also said why we define that γ . See γ is actually called extinction angle and it happens to be the competition margin angle for normal inverter operation ok. So, if I want to write this instead of γ . What is γ ? γ is nothing but $180^\circ - \alpha - \mu$ ok. So, if I write the expressions. So, take the expression for V_d . V_d is $\sqrt{3} V_{do} \cos \alpha - \cos(\alpha + 30^\circ)$.

So, if I write α in terms of γ , it is $\cos(180^\circ - \gamma - \mu)$. See γ is just a definition; I mean γ is given by $180^\circ - \alpha - \mu$ that is all. Now, why I also said why you defined that. So, there is a purpose for each and every definition; plus $\alpha + \mu$ is $180^\circ - \gamma + 30^\circ$. So, I can write this as V_d is equal to $\sqrt{3} V_{do} \cos \gamma + \cos(\gamma - 30^\circ)$. Similarly, I try to write the expression for I_d in terms of γ instead of α .

So, if I take I_d sorry, I_d is I_s by $\sqrt{3} \cos$. So, can I straight away write the expression? I mean, if you look at the expression for V_d . So, you see that there is $\cos \alpha - \cos(\alpha + 30^\circ)$ in both expressions $\cos \alpha + \cos(\alpha + 30^\circ)$. So, I can write this as $\cos \gamma + \cos(\gamma - 30^\circ)$.

30 degrees minus $\cos \gamma$ minus 30 degrees. Yeah, only difference is this is plus because this there is a minus $\cos \alpha$ plus u plus 30. Now, if we recall, we related this V_d and I_d through R_c , we defined a commutation resistance R_c .

So, we can actually try to relate V_d and I_d in this case also. See what we are doing is in the case of 3 and 4 valve conduction mode it is an abnormal operation. So, if I take this expression V_d . So, what I am trying to do is ok. Let me instead of suppose I take this as equation 1 this as equation 2 ok. So, I use this 1 and 2 to get one more equation that is V_d is equal to $\sqrt{3}$ by 2 $V_{do} \cos \alpha$ minus 30 degrees.

Now what I do is; I replace this $\cos \alpha$ plus u plus 30 by an expression for that involving I_d and I_s and α from equation 2. So, from equation 2, I get $\cos \alpha$ plus u plus 30 as $\cos \alpha$ minus 30 degrees minus $\sqrt{3} I_d$ by I_s . So this can be written as $\sqrt{3} V_{do}$. So, there is $\cos \alpha$ minus 30 $\cos \alpha$ minus 30. I think, I made a mistake here. This is not the $\sqrt{3}$, this is $\sqrt{3}$ divided by 2 sorry. So, that 2 gets cancelled. The 2 in the denominator gets cancelled. So, we get $\sqrt{3} V_{do} \cos \alpha$ minus 30 degrees minus $\sqrt{3}$ into $\sqrt{3}$ is $3 V_{do}$, I_d by 2 I_s ok.

So, what is V_{do} by 2 I_s by definition of R_c ? R_c is defined as V_{do} by 2 I_s . So, we get V_d equal to $\sqrt{3} V_{do} \cos \alpha$ minus 30 degrees minus 3 times $R_c I_d$. Because, V_{do} by 2 I_s is given a notation R_c ; R_c is just a notation for V_{do} by 2 I_s that is all.

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$$\begin{aligned}
 V_d &= \frac{\sqrt{3}}{2} V_m \left[-\cos(\gamma-30^\circ) - \cos(\gamma+u+30^\circ) \right] \\
 I_d &= \frac{I_s}{\sqrt{3}} \left[\cos(\gamma-30^\circ) - \cos(\gamma+u+30^\circ) \right] \\
 V_d &= \frac{\sqrt{3}}{2} V_m \left[-\cos(\gamma-30^\circ) + \frac{\sqrt{3} I_d}{I_s} - \cos(\gamma+30^\circ) \right] \\
 V_d &= -\sqrt{3} V_m \cos(\gamma-30^\circ) + \frac{3 V_m}{2 I_s} I_d \\
 V_d &= -\sqrt{3} V_m \cos(\gamma-30^\circ) + 3 R_c I_d
 \end{aligned}$$




So, we have these two equations, the first equation relates V_d and γ and u . The second equation relates I_d and γ and u . Now I can write the first equation that is this equation as V_d is equal to $\sqrt{3} V_m \cos(\gamma - 30^\circ)$. Now the second term on the right hand side has $\cos(\gamma + u + 30^\circ)$. So, I use the next equation to eliminate $\cos(\gamma + u + 30^\circ)$. So, if I do that I get $\sqrt{3} V_m \cos(\gamma - 30^\circ) - \frac{3 V_m}{2 I_s} I_d$.

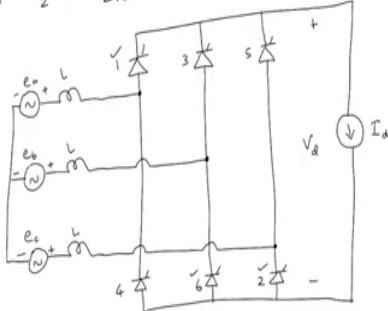
So, if I simplify this, I get $\sqrt{3} V_m \cos(\gamma - 30^\circ)$ with a negative sign. So, $-\sqrt{3} V_m \cos(\gamma - 30^\circ) + \frac{3 V_m}{2 I_s} I_d$. So, I can write this as $V_d = -\sqrt{3} V_m \cos(\gamma - 30^\circ) + 3 R_c I_d$. We have defined a quantity R_c which is $V_m / 2 I_s$. So, this is $3 R_c I_d$. So, this is an equation that relates V_d , R_c and I_d and γ .

These are the equations for the abnormal operation corresponding to 3 and 4 valve conduction mode ok. Now there is one thing about the range of alpha that is possible with for this abnormal operation. See, in the case of normal operation that is 2 and 3 valve conduction mode, we said that alpha can take any value greater than 0. Now let us see whether that is possible for abnormal operation ok. So, we are still continuing our discussion on the abnormal operation ok.

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Voltage across valve 3 when valves 6, 1, 2 are conducting
 $= -V_d = -\frac{3}{2}e_a = -\frac{3}{2}\frac{\sqrt{3}}{3}V\sin(\omega t + 150^\circ) = \sqrt{\frac{3}{2}}V\sin(\omega t - 30^\circ) \Rightarrow \alpha > 30^\circ$



So, if I take voltage across valve 3 when valves 6, see when valve 3 is turned on 6, 1, 2 are already conducting for this abnormal operation. So, valves 6, 1, 2 are conducting. Now what is this voltage when across valve 3 when 6 1 2 are conducting? So, when I sure look at this circuit I mean let me draw the circuit. So, this is a constant current I d e a, e b, e c, L, L, L

valves 1, 3, 5 valves 4, 6, 2. So, this is V_d . So, 6, 1 and 2 are conducting. What is the voltage across R_3 ?

Student: (Refer Time: 19:33).

Yeah say, in the table we did not actually get the expression for voltage across valve 3. We got the expression for voltage across valve 1. Again for getting voltage across valve 1 we used V_d , because V_d we had already got. So, it is better to write it in terms of V_d and we already know what is V_d . We know the expression for V_d . So, what is it in terms of V_d ? Voltage across valve 3, when valves 6, 1, 2 are conducting.

Student: minus (Refer Time: 20:08).

Minus V_d . So, it is minus v_d . Now, when 6, 1, 2 are conducting, what is V_d ?

Student: (Refer Time: 20:18).

That we make out from the table.

Student: 3 by 2 (Refer Time: 20:21).

3 by 2 e a. So, minus V_d is minus 3 by 2 e a ok. Now substitute the expression for ea. What is ea? ea is $\frac{\sqrt{2}}{3} V \sin(\omega t + 150)$. So, it is minus 3 by 2 $\frac{\sqrt{2}}{3} V \sin(\omega t + 150)$ degrees. Of course, I can better to write this as $\frac{\sqrt{3}}{2} V \sin(\omega t - 30)$. I have written just minus $\sin(\omega t + 150)$ or $\sin(\omega t - 30)$.

So, this is the voltage across valve 3, when valve 6, 1, 2 are conducting. So that means, if I want to turn on valve 3 so, the voltage across valve 3 is given by this expression. So, does I mean what is the inference? I gave a hint; we are talking about the range of alpha. So, can alpha take a value say 10 degrees 5 degrees what is alpha? Alpha is the instant at which valve 3 is stand on.

Student: Greater than 30.

So, it should be greater than 30. See when you want to turn on a valve first of all it should be.

Student: Positive.

Forward.

Student: Forward biased.

Forward biased. So, the voltage across valve 3 will not be negative sorry will not be positive before ωt will less than 30. So, this actually implies alpha should be greater than 30 degrees. See, there is no point in turning on a valve when it is not forward biased if it is reverse biased it would not turn on ok. So, if you want to turn on a valve. So, and make it I mean I mean allow it to conduct current, then it should be forward biased. So, it will be forward biased only when ωt is greater than 30. So, alpha should be greater than 30.