

DC Power Transmission Systems
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Lecture - 25

2 and 3 valve conduction mode of 6 pulse LCC: Fundamental and harmonic components of AC side current

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α to $\alpha + \mu$ — 1, 2, 3
 $\alpha + \mu$ to $\alpha + 60^\circ$ — 2, 3
 $\alpha + 60^\circ$ to $\alpha + \mu + 60^\circ$ — 2, 3, 4
 $\alpha + \mu + 60^\circ$ to $\alpha + 120^\circ$ — 3, 4
 $\alpha + 120^\circ$ to $\alpha + \mu + 120^\circ$ — 3, 4, 5
 $\alpha + \mu + 120^\circ$ to $\alpha + 180^\circ$ — 4, 5
 $\alpha + 180^\circ$ to $\alpha + \mu + 180^\circ$ — 4, 5, 6
 $\alpha + \mu + 180^\circ$ to $\alpha + 240^\circ$ — 5, 6
 $\alpha + 240^\circ$ to $\alpha + \mu + 240^\circ$ — 5, 6, 1
 $\alpha + \mu + 240^\circ$ to $\alpha + 300^\circ$ — 6, 1
 $\alpha + 300^\circ$ to $\alpha + \mu + 300^\circ$ — 6, 1, 2
 $\alpha + \mu + 300^\circ$ to $\alpha + 360^\circ$ — 1, 2

$i_b = i_3 - i_4 \quad | \quad i_b = i_3 \quad \text{or} \quad i_b = -i_4$
 $i_b(\omega_s t) = i_b(\omega_s t - 120^\circ), \quad i_c(\omega_s t) = i_b(\omega_s t - 120^\circ)$
 $i_2(\omega_s t) = i_1(\omega_s t - 60^\circ), \quad i_3(\omega_s t) = i_2(\omega_s t - 60^\circ), \quad i_4(\omega_s t) = i_3(\omega_s t - 60^\circ), \quad i_5(\omega_s t) = i_4(\omega_s t - 60^\circ), \quad i_6(\omega_s t) = i_5(\omega_s t - 60^\circ)$

If you look at the circuit ok, let me draw the circuit. So, I will come to the expression of i_b , so I have three legs. So, I have the current i_a shown as leaving the positive terminal of e_a , then i_b, i_c . So, this is 1, 3, 5, 4, 6, 2, V_d is here. So, i_b is a current that flows I mean or it has a nonzero value if and only if valve 3 is conducting or valve 6 is conducting say it is either equal to i_3 or

Student: Minus i_6 .

Minus i_6 ; one can say that it's i_3 minus i_6 say by Kirchhoff's current law, it is i_3 minus see the current through the valve 3 is i_3 , current through the valve 6 is i_6 . So, i_b I am not worried about i_a or i_c right now. So, if I just look i_b , it is i_3 minus i_6 ok. Now, we also saw that there are 6 intervals and 12 subintervals.

So, if you look at the table, the first subinterval is from α to $\alpha + u$, $\alpha + u$ to $\alpha + 60$ degrees, say these are the values of ωt . $\alpha + 60$ degrees to $\alpha + u + 60$, $\alpha + u + 60$ to $\alpha + 120$, $\alpha + 120$ to $\alpha + u + 120$, $\alpha + u + 120$ to $\alpha + 180$, $\alpha + 180$ to $\alpha + u + 180$, $\alpha + u + 180$ to $\alpha + 240$, $\alpha + 240$ to $\alpha + u + 240$, $\alpha + u + 240$ to $\alpha + 300$, $\alpha + 300$ to $\alpha + u + 300$, $\alpha + u + 300$ to $\alpha + 360$. So, these are the 6 intervals and in which there are 12 subintervals.

So, we know what are the valves that conduct. So, if you take the first subinterval, the valves that conduct are 1, 2, 3, the second subinterval it is 2, 3, then 2, 3, 4; then 3, 4, 5, 3, 4, 5, 4, 5, 4, 5, 6, we already form this table I mean I am just trying to again use this information. Say the table had some more information that actually we know we do not need for analyzing the AC side current, then 5, 6; 5, 6, 1, 6, 1, 6, 1, 2, 1, 2 ok.

Now, there is one type of symmetry on the AC side I mean on the AC side, if you look at the currents the currents are identical except for a phase shift of 120 degrees. So, if you take i_b of ωt , then it is nothing but i_a which is delayed by.

Student: 120.

120. So, it is ωt minus 120, i_a of ωt minus 120 will give me i_b . Similarly, if you take i_c of ωt , it is i_b delayed by 120. So, i_c of ωt is i_b of ωt minus 120. Now, if you look at the currents through the valve say if you take any current say I

can have a current through valve 1, which is i_1 current through valve 2 which is i_2 current through valve 3 is i_3 current through valve 4 is i_4 current through valve 5 is i_5 .

Now, I will try to use one fact which I think we are all familiar with, I mean what do we expect for these 6 currents i_1, i_2, i_3 up to i_6 , I mean are they same similar identical with phase shift I mean I mean can we say anything about that or we cannot say anything, are they are different, do they satisfy some condition, $i_1, i_2, i_3, i_4, i_5, i_6$?

See please note we derived this from a very general circuit say. This circuit is not obvious, this is the great circuit say 6 legs sorry 3 legs 6 devices and 3 AC side terminals 2 DC side terminals is something which is not an obvious circuit ok, it was derived in fact from something which was more obvious. So, this is known as the great circuit.

So, here there are 6 devices and I all I take the all the currents which are flowing from anode to cathode, all the 6 currents are flowing from shown as flowing from anode to cathode. So, what do you say? If you go back to the derivation, do you see that there is some pattern in these currents, are they identical except for phase shift, do you see that? Because if you go back to the derivation, these devices are connected in series with voltage sources, so there are 6 voltage source connected in series with these 6 devices, and these 6 voltage sources are actually identical with the phase shift of 60 degrees.


So, if you take the 6 voltages, they are all identical voltages, and phase shift between them is 60 degrees. So, these currents are also actually identical with a phase shift of 60 degrees. Now, you see that the sequence of turning on is 1, 2, 3, 4, 5, 6, see the numbering is in such a way that they are in the order of turning on ok. So, that means, i_1, i_2 up to i_6 are identical except that there is a phase shift between the any two currents. If I take i_2 it is identical to i_1 except that there is a delay of 60 degrees; similarly i_3 is identical to i_2 except for a delay of 60 degrees. So, if I take i_1 , it is related to i_2 . So, if I take i_2 for example, i_2 of ωt , can I say that its equal to i_1 of ωt minus 60 degrees?

And if I take i_3 , it is nothing but i_2 minus 60 degrees, i_2 of ωt minus 60 degrees. Then i_4 of ωt is i_3 of ωt minus 60 degrees. Then i_5 of ωt is i_4

4 of omega o t minus 60 degrees, then i 6 of omega o t is i 5 of omega o t minus 60 degrees. And of course, i 1 of omega o t will be i 6 of omega o t minus 60 degrees ok.

So, what we have is identical currents in the valves except for a phase shift of 60 degrees. And of course, I can also relate in each leg the valve currents and the current on the AC side just as I related i 3, i 6, and i b; I can relate i 1, i 4 and i a; I can also relate i 5, i 2 and i c ok. So, but I am not going to do that I mean that is just application of Kirchoff's current law. What I will do is, I will just restrict myself to this i b, one of the phase currents.

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$$i_b(\omega t) = \begin{cases} I_s [\cos \alpha - \cos(\omega t)], & \alpha \leq \omega t \leq \alpha + u \\ I_s, & \alpha + u \leq \omega t \leq \alpha + 120^\circ \\ I_s - I_s [\cos \alpha - \cos(\omega t - 120^\circ)], & \alpha + 120^\circ \leq \omega t \leq \alpha + u + 120^\circ \\ 0, & \alpha + u + 120^\circ \leq \omega t \leq \alpha + 180^\circ \\ -I_s [\cos \alpha + \cos(\omega t)], & \alpha + 180^\circ \leq \omega t \leq \alpha + u + 180^\circ \\ -I_s, & \alpha + u + 180^\circ \leq \omega t \leq \alpha + 300^\circ \\ -I_s + I_s [\cos \alpha + \cos(\omega t - 120^\circ)], & \alpha + 300^\circ \leq \omega t \leq \alpha + u + 300^\circ \\ 0, & \alpha + u + 300^\circ \leq \omega t \leq \alpha + 360^\circ \end{cases}$$

i_b has half wave symmetry

For $\alpha \leq \omega t \leq \alpha + u$, $i_a(\omega t) = I_s - i_b(\omega t)$

For $\alpha + 180^\circ \leq \omega t \leq \alpha + u + 180^\circ$, $i_b(\omega t) = -i_c(\omega t) = -i_s(\omega t - 180^\circ) = -i_b(\omega t - 180^\circ)$
 $= -I_s [\cos \alpha - \cos(\omega t - 180^\circ)] = -I_s [\cos \alpha + \cos(\omega t)]$

For $\alpha + 300^\circ \leq \omega t \leq \alpha + u + 300^\circ$, $i_b(\omega t) = -i_c(\omega t) = -i_s(\omega t - 180^\circ) = -i_b(\omega t - 180^\circ)$
 $= -I_s [\cos \alpha + \cos(\omega t - 120^\circ)]$



So, I am interested in the expression of i b; so i b as a function of omega o t ok. Let us try to get the expression in all the 12 subintervals. So, we are interested in all the 12 subintervals ok. So, the first subinterval is alpha to alpha plus u. So, what is i b from alpha to alpha plus u? See from alpha to alpha plus u 1, 2 and 3 are conducting, valves 1, 2 and 3 are conducting.

So, i_b is dependent only on the current through either 3 or 6. So, whether one or two conduct does not matter, so i_b is equal to i_3 ; i_6 is 0, because i_6 is not conducting. So, i_b is i_3 in the first subinterval. And we got the expression for i_3 ok. So, we derived the expressions for i_3 , it is $I_d \cos \alpha \sin(\omega t - \alpha)$. So, this is the expression for i_b in the first subinterval α to $\alpha + \mu$ ok.

Student: I_s .

Oh, sorry, I am sorry, I am sorry, please correct this, it is I_s , sorry it is $I_s \sin(\omega t - \alpha)$ into $\cos \alpha \sin(\omega t - \alpha)$. I_s is the short circuit current.

Then if I take the second subinterval $\alpha + \mu$ to $\alpha + \mu + 60^\circ$, the current i_b is equal to the current i_3 . Now, please note that in the next subinterval $\alpha + \mu + 60^\circ$ to $\alpha + \mu + 120^\circ$ also, I have only valve 3 conducting in the upper commutation group. See upper commutation group is 1, 3, 5. Say when only 3 is conducting among 1, 3, 5, i_b is equal to i_3 ok.

So, please note in any of if you look at this 12 subintervals, is there any subinterval where both 3 and 6 conducts, there is no subinterval where both 3 and 6 conduct. So, it is i_b is either equal to i_3 or equal to $-i_6$ ok. So, based on this information, I can say that i_b is either equal to i_3 or i_b is equal to $-i_6$. I can say easily.

Of course, this also covers the case of i_3 being equal to 0 as well as i_6 being equal to 0, say there are some subintervals where neither is there a subintervals, see there is an subinterval where only 4 and 5 conduct. So, when 4 and 5 conduct neither 3 is conducting nor 6 is conducting, that means, both i_3 is 0, i_6 is also 0. So, I can still use this relation that i_b is either equal to i_3 or equal to $-i_6$ ok.

So, if you look at the subintervals 2, 3 and 4; subintervals, 2, 3 and 4, there is only one valve that conducts in the upper commutation group that is? Valve 3.

Student: valve (Refer Time: 14:43)

Valve 3; valve 3 is the only one which is conducting among 1, 3, 5; from $\alpha + u$ to $\alpha + 120$ ok, so that means, for $\alpha + u$ to $\alpha + 120$ i_b is equal to?

Student: i_d .

i_d . So, it is equal to i_d for $\alpha + u$ to $\alpha + 120$. Now, one can easily observe one fact that unlike the previous case where L was 0, here L is nonzero, L is nonzero, i_b cannot have discontinuities. So, when i_b cannot have discontinuities, then I can easily say what happens at ωt equal to α what happens at ωt equal to $\alpha + u$?

So, I can replace the strict inequality by less than or equal to. Now, this was not possible in the previous case where L was 0, see there were discontinuities in the current. Now, the i_b will never be discontinuous because of the presence of L – nonzero L ok, so that is the expression for i_b up to $\alpha + 120$.

Then in order to get the next expression say the next subinterval is $\alpha + 120$ to $\alpha + u + 120$. So, in this case, what is the expression for i_b how to get the expression? So, we saw that, so I mean just in the previous page i_b of ωt is actually i_a of ωt minus 120. So, if I know what happens to i_a 120 degrees ago, I can find i_b now that is what it means ok.

So, I know what happens for α to $\alpha + u$, see I am interested in let me tell, I am interested in the expression for i_b from $\alpha + 120$ to $\alpha + u + 120$. Now, this subinterval is nothing but the first subinterval shifted to the right by 120 degrees ok; shifted by 120 degrees, that means, you get the take the expression for i_a in the subinterval α to $\alpha + u$, shift, I mean if you shift that by 120 degrees you get the expression for i_b . I think I need to use one more equation.

So, what is I mean what is i_a ? Say I do not have the expression for i_a here in the interval α in the subinterval α to $\alpha + u$. What I have is the expression for i_b from α to $\alpha + u$. So, if I know i_a from α to $\alpha + u$ shift it by 120, I get the expression for i_b . So, what is the expression for i_a from α to $\alpha + u$?

Student: (Refer Time: 17:53).

Yeah. So, for $\alpha \leq \omega t \leq \alpha + u$, i_a of ωt is nothing but $I_d \sin(\omega t - \phi)$. So, I know the expression for i_a . Now, I use this equation i_b of ωt is equal to i_a of $\omega t - 120$. So, if I do that I get the expression for i_b as $I_d \sin(\omega t - \phi - 120^\circ)$. So, is that ok. So, we got the expression for i_b up to $\alpha + u + 120$.

Then what happens after that? So, go come back here $\alpha + u + 120$ after $\alpha + u + 120$ the next subinterval is the one where only 4 and 5 conducts. When 4 and 5 conducts i_b is 0. So, when 4 and 5 conducts i_b is 0. So, the that 0 value of i_b holds up to $\alpha + u + 120$ what?

Student: (Refer Time: 19:21).

180. So, it is equal to 0 for $\alpha + u + 120 \leq \omega t \leq \alpha + 180$, then after that what happens? So, the next interval is $\alpha + 180$ to $\alpha + u + 180$, $\alpha + 180 \leq \omega t \leq \alpha + u + 180$. So, what should be the expression for i_b ?

Student: Minus of that which was 140 (Refer Time: 20:15).

Yeah, what is that equation that we use to arrive at that? How do you say it is minus of ok. So, if you take this subinterval $\alpha + 180$ to $\alpha + u + 180$.

Student: In the circuit.

So, which valve is conducting?

Student: 4 and 5.

4, 5?

Student: 4, 5, 6.

4, 5, 6. So, i_b is equal to minus i_6 ok, let me first write that. So, for $\alpha + 180$ less than or equal to ωt less than or equal to $\alpha + \pi + 180$ degrees, i_b of ωt is equal to just now we saw, so in this subinterval, 4, 5 and 6 conduct. So, when 4, 5 and 6 conduct, i_b is equal to? See in general it is i_3 minus i_6 , but i_3 is 0, 3 is not conduct. So, it is minus i_6 . So, it is minus i_6 of ωt . Now, what is the use of having minus i_6 , I mean, what does I mean is there any purpose served in having minus i_6 ?

Student: (Refer Time: 21:38).

Yeah, i_6 is related to i_3 . So, i_6 is identical to i_3 except for a phase shift of?

Student: (Refer Time: 21:43).

Yeah, go back to the, say in the last line I have the phase relationship between i_1 i_2 , i_3 i_2 , i_4 i_3 , i_5 i_4 , i_6 i_5 . So, from that I can I get the relationship between i_6 and i_3 . So, i_6 is identical to i_3 except for a phase shift of?

Student: 180.

180 degree, 60 into 3, so 180 degrees. So, what does that mean? It is minus i_3 . So, or in another words ok, I can write it as minus i_3 of $\omega_o t$ minus 120° minus 180° .

Student: Yes.

i_3 and i_6 are identical except for a phase shift of 180 degrees ok. Now, do I have the expression for the now I need the expression for i_3 for which subinterval, see I am current subinterval of interest is α plus 180 to α plus u plus 180. So, I want to know what happen to i_3 180 degrees ago.

Student: Yes.

That means which subinterval?

Student: α to α plus.

Yeah, you just subtract 180 degrees from the upper and lower limits of $\omega_o t$. So, from α to α plus u , what happened to i_3 , we should know do you have the expression for i_3 from α to α plus u it is nothing but.

Student: i_b .

i_b , it is nothing but i_b . So, what I have to do is just take the expression for i_b from α to α plus u . Yeah, it is not difficult, I mean, it just takes some it requires some concentration nothing more than that ok. So, let me write that also. So, can I say it is minus i_b of $\omega_o t$ minus 180 degrees; i_b is equal to i_3 is that or not?

Student: (Refer Time: 23:45).

Ok. So, now, we have this expression. So, this is equal to minus I_s into $\cos \alpha$ minus $\cos \omega t$ is there I should replace that by $\cos \omega t$ minus 180 degrees. So, this is nothing but minus $I_s \cos \alpha$ plus $\cos \omega t$. So, I will write just write this expression here minus $I_s \cos \alpha$ plus $\cos \omega t$. So, this expression is applicable from α plus 180 to α plus u plus 180, then is this clear, then we will go to the next subinterval α plus u plus 180. So, at α plus u plus 180 degree, valve 4 stops conducting, so 5 and 6 conduct. So, when just 5 and 6 conduct, then i_b is equal to.

Student: Minus (Refer Time: 25:19).

Minus i_d , i_b is minus i_d . Now, you see that even in the next subinterval, though there are three valves 5, 6, 1 conducting, in the lower commutation group only 6 is conducting. From α plus 240 to α plus u plus 240, 5, 6, 1 conduct. So, only 6 is conducting in the lower commutation group. The same thing happens even in the next subinterval α plus u plus 240 to α plus 300, 6 and 1 are conducting. So, as long as only 6 is conducting among 2, 4, 6, i_b is equal to?

Student: Minus i .

Minus i ok. So, that happens from α plus u plus 180 degrees to α plus 300 ok. So, the expression is minus I_d for α plus u plus 180 degrees to α plus 300 degrees, is that ok, because from α plus u plus 180 to α plus 300 only valve 6 conducts among the valves 2, 4, 6. So, anyhow valve 3 are not conducting. So, i_b is minus i_c which is minus I_d right.

Now, let us take the next subinterval. The next subinterval is α plus 300 less than or equal to ωt ; less than or equal to ωt sorry less than or equal to α plus u plus 300. So, in this subinterval, so if you look at the subinterval α plus 300 to α plus u plus 300, valves 6, 1 and 2 are conducting. So, when valves 6, 1 and 2 are conducting, then what is i_b ?

Student: (Refer Time: 27:40).

Of course, it is minus i_6 ; i_b is minus i_6 , but how do I get that I mean what is the use of that? Ok, let me write here for $\alpha + 300$ to $\alpha + u + 300$ i_b of $\omega o t$ is equal to minus i_6 of $\omega o t$. Now, again we use the same result that i_6 of $\omega o t$ is equal to i_3 of $\omega o t$ minus 180 degrees. So, it is minus i_3 of $\omega o t$ minus 180 degrees. Now, this can be written in terms of i_b . So, can I say that this is minus i_b of $\omega o t$ minus 180 degrees?

So, we know the expression for i_b in the, so which sub which sub interval we have to look at for i_b , see the current subinterval of interest is $\alpha + 300$ to $\alpha + u + 300$. So, for this subinterval, we are getting an expression for i_b . So, this is in terms of i_b which was obtained for a subinterval which was 180 degrees ago. So, which one, it is α plus.

Student: 120.

120 to $\alpha + u + 120$. So, we have the expression for i_b from $\alpha + 120$ to $\alpha + u + 120$. So, this is equal to minus I_d plus $I_s \cos \alpha$ minus \cos in place of $\omega o t$, I have $\omega o t$ minus 180 degrees. So, this can be simplified. So, this can be written as minus I_d plus I_s into $\cos \alpha$. So, minus $\cos \omega o t$ minus 180 minus 120 is plus $\cos \omega o t$ minus 120, is that ok. So, this is the expression up to $\alpha + u + 300$. Then if I go to the next subinterval, it is $\alpha + u + 300$ less than or equal to $\omega o t$ less than or equal to $\alpha + 360$ degrees.

So, in this subinterval, $\alpha + u + 300$ to $\alpha + 360$ degrees, valves 1 and 2 are conducting. So, neither three is conducting nor 6 is conducting. So, i_b is 0. So, this is 0. So, we have the expression for i_b for one full cycle from α to $\alpha + 360$ degrees. Of course, though there are 12 subintervals, some expressions are applicable for multiple subintervals that is why we have only 8 expressions; of course, some of them are say it is zero for two of these subintervals also. Now, if I want to find the fundamental component RMS

value or harmonic component RMS value, I have to do Fourier series, but any simplification is possible. Do you see any symmetry in $i b$?


Student: Half wave.

It has.

Student: Half wave.

Half wave symmetry. So, $i b$ of ωt plus 180 degrees is equal to minus $i b$. So, you see that this has half wave symmetry. So, $i b$ has half wave symmetry. So, what is that mean I need not use the entire expression from α to α plus 360, I can just use the expressions applicable to one half of the cycle, say α to α plus 180 that is sufficient. So, I can just use say for example, these four expressions do Fourier analysis, and get the RMS value of the fundamental as well as harmonics. So, I will leave that to you. So, I will give the answer.

(Refer Slide Time: 32:53)




RMS value of fundamental component of AC side currents,

$$I_1 = \frac{\sqrt{6} I_d}{2\pi} \sqrt{[\cos\alpha + \cos(\alpha+u)]^2 + \left[\frac{2u + \sin(2\alpha) - \sin(2\alpha+2u)}{2\cos\alpha - 2\cos(\alpha+u)} \right]^2}$$

The harmonic components in the AC side currents are of order $h = 6k \pm 1$, $k = 1, 2, 3, \dots$

For $h = 6k \pm 1$, $k = 1, 2, 3, \dots$, the RMS value of h^{th} order harmonic component in AC side currents,

$$I_h = \frac{\sqrt{6} I_d}{\pi h} \sqrt{\frac{\sin^2 \left[\frac{(h+1)\pi}{2} \right]}{(h+1)^2} + \frac{\sin^2 \left[\frac{(h-1)\pi}{2} \right]}{(h-1)^2} - \frac{2 \sin \left[\frac{(h+1)\pi}{2} \right] \sin \left[\frac{(h-1)\pi}{2} \right] \cos(2\alpha+u)}{h^2-1}}$$


RMS value of fundamental component yeah this is a very good example to know that how laborious it can be to apply Fourier analysis ok, this actually this particular example, of course, I took some long time to get this RMS value of fundamentals component of AC side current.

So, I use the notation I with the subscript 1. So, the expression is $\sqrt{6} I_d$ by 2π into square root of $\cos \alpha$ plus $\cos \alpha$ plus u whole square plus $2u$ plus $\sin 2\alpha$ minus $\sin 2\alpha$ plus $2u$ divided by $2\cos \alpha$ minus $2\cos \alpha$ plus u .

Say the main point here is if you apply Fourier series for such a waveforms you get an expression which is 2 page or 3 page longer, I mean the I mean only the main work involved is simplification, and do some trigonometric manipulation and simplify that is all. Say once

you integrate after integration your expression will be very long I mean may be 1 or 2 pages long. So, after simplification you get this ok, so that is the idea.

So, if this is the fundamental component now what are the harmonic components, I mean what is the order of the harmonic components that are present? See there is half wave symmetry. So, due to half wave symmetry, you will not have even harmonics, you will not have even harmonics due to half wave symmetry, second harmonic, fourth harmonic, sixth harmonic are not there, any other harmonic is not there?

Student: Third harmonic.

Third harmonic?

Student: Triplen.

Triplen harmonics, why?

Student: Therefore, balanced.

Because $i_a + i_b + i_c = 0$. So, triplen harmonics are also not there. So, the harmonic components are of order 5, 7, 11, 13, 17, 19. So, the harmonic components in the AC side currents are of order h equal to $6k \pm 1$, where k takes all positive integer values ok. So, if you put k equal to 1, you get 5 and 7, k equal to 2, you get 11 and 13 so on. So, these are the order of that.

So, what is the expression? I mean you have to apply Fourier analysis to get the expression for the RMS value of the harmonic component. So, for h equal to $6k \pm 1$, k equal to 1, 2, 3 so on, the RMS value of h th order harmonic component in AC side currents; of course, for other values of h , it is 0. So, I will use the notation I_h . So, it is $\sqrt{6} I_d$ by πh into $\frac{\sin^2 h + 1}{2} \div (h + 1)^2 + \frac{\sin^2 h - 1}{2} \div (h - 1)^2 - 2 \sin h \div (h + 1) \div (h - 1) \cos 2$

$\alpha + u$ divided by $h^2 - 1$, its entire thing is taken under root, this is divided by $\cos \alpha - \cos \alpha + u$. So, that is the expression.

Of course, there can be one obvious question why I am writing separate expression for I_1 and for I_h where h is not equal to 1. See, Fourier series does not distinguish between h equal to 1, and other values of h . Now, the purpose of writing two expressions is to say that I cannot use the general expression for I_h for I_1 . Why I cannot do that? I mean that is for you to answer. So, you can try say instead of trying to get first I_1 and then I_h , why do not you see the I mean in the expression for I_h you actually it is obvious there is $h - 1$, so that is why I cannot use that.

So, there is some problem in using this expression for I_h when h is equal to 1 ok. So, this expression is applicable only when h is not equal to 1. So, for I_1 you have to do a separate derivation.