

Analog Electronic Circuits
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Lecture – 97
Applications of Feedback in Amplifier Circuits (Part-A)

Dear participants, so, welcome back to our online certification course on Analog Electronic Circuit. Myself Pradip Mandal from E and EC department of IIT Kharagpur. Today's topic of discussion it is Feedback it is rather continuation of feedback system. And specifically we are going to talk about Application of Feedback circuit in amplifier. So, on the amplifier may have transistor level circuit as well as op-amp based circuit.

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Flow of Discussion (Bottom-up)
– Sub-systems/Modules

- **System / Sub-systems** (for specific application)
 - **Modules** (performing specific tasks)
 - Building blocks (having specific characteristics) - Bias circuits
 - Components (devices/circuit elements)
- **Week 10 (Course Module 9):**
 - Feedback System: Basic feedback theory
 - Four different feedback configurations and their characteristics
 - Effects of feedback on frequency response of an amplifier
 - Application of feedback in practical circuits

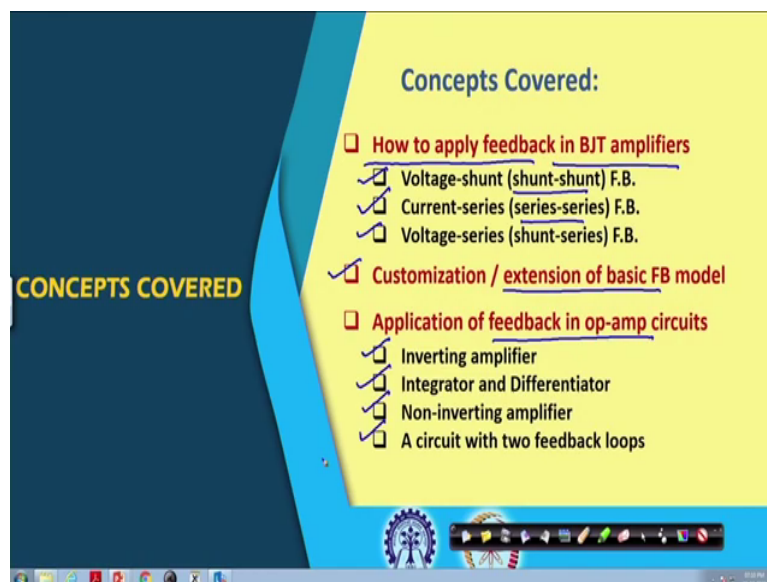
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According, to our overall flow we are in a week 10 and we are in module 9. And we have discussed about basic four configurations feedback configurations and their characteristic we

also have discussed about effect of feedback on a frequency response of an amplifier. And today's discussion it is more like continuation of the basic four configurations and specifically how those configurations can be deployed on practical circuits. The practical circuit can be either transistor level the example. So, we will be talking about is primarily BJT. And then also we will be talking about deployment of feedback system on op-amp circuit.

So, we can say that we are at module levels as well as at subsystem levels.

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So, the concept, so, we are planning to cover today it is listed here. So, we shall see how we can deploy or how do we decide different feedback configuration in BJT circuits BJT amplifiers. And there we will be talking about specifically three different configurations, which you will be giving us fair idea how to deploy the feedback configuration these are the

three possible configurations we are talking about of course, one more configuration it is skipped due to the shortage of time.

So, we will be talking about voltage sampling and shunt feedback referred as shunt-shunt feedback. And then current sampling and a series mixing referred as series-series feedback and then the third one it is voltage series feedback or shunt-series feedback. And then we shall also talk about a little bit extension of the basic feedback models, which we need to discuss before we go into the feedback circuit using op-amp. And for feedback configuration around op-amp we do have different possible examples; namely inverting amplifier, then integrator and differentiator and then, non inverting amplifier. And then also we can discuss about a circuit which is having two feedback loops.

So, these are the these are the enlisted items we do have for this lecture. So, to start with we let us summarize whatever the things we have discussed in our basic four configurations.

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Summary of effects of negative feedback loop in amplifier

Configuration names	S_{in}	S_o	A	R_{in}	R_{out}	Unit of β
Voltage-Shunt (Shunt-Shunt)	I	V	Z_m	↓	↓	Mho Ω^{-1}
Current-Shunt (Series-Shunt)	I	I	A_v	↓	↑	-
Voltage-Series (Shunt-Series)	V	V	A_v	↑	↓	-
Current-Series (Series-Series)	V	I	G_m	↑	↑	Ohm Ω

$$A_v = \frac{A}{1 + \beta \cdot A} \approx \frac{1}{\beta}$$

$$D = (1 + \beta \cdot A)$$

$$A_v \approx \frac{1}{\beta}$$

So, yeah. So, here we have four different configurations, so the name of those configurations are given here; namely voltages shunt, current shunt, voltage series and current series or you may say shunt-shunt, series-shunt and then shunt-series and series-series.

So, you may recall that now, depending on these configurations we also can say what type of signals we do have at the input. And also we can see what type of signals we do have at the output of the system. Here we do have the basic model of the feedback system negative feedback system. The input either we may call this is the primary input or just by observing this input we can tell that what kind of amplifier we do have or rather this the input type and the output signal type it will decide what kind of amplifier we do have and that also decides that what kind of feedback we do have or feedback network we do have.

Say for example, if we consider the first one it is the signal here it is current and signal here it is voltage. So, the amplifier the forward amplifier it is essentially trans impedance amplifier or we can say that A is Z_m . So, then of course, we know that once we are deploying the negative feedback system, according to this formula the main the forward amplifier gain A it is getting reduced by this factor, which is referred as a desensitizing factor $1 + \beta$ into A . Where this β is the feedback factor here and A depending on the type of signal it may vary from Z_m then A is the current gain voltage gain and trans conductance G_m .

So, whatever the configuration we do consider essentially this is the formula by which we can say that A it is getting reduced. So, the arrow we are putting here indicating that the feedback effect of the negative feedback it is reducing this A by a factor desensitization factor of the circuit. So, if I on the other hand, if I if I consider say this configuration then the input is current output is also current and A is current gain. And once we have the proper feedback connection, we are expecting that this current gain it will get reduced.

So, likewise if we consider the third configuration the voltage gain it will be getting reduced, likewise the fourth one trans conductance it will be getting reduced. So, whatever the configuration we do have if based on that configuration once we know that what is A and then we can say the corresponding A it is getting reduced by this factor. And the factor here what is the basic purpose of reducing this A what you can say that if I assume that β into A it is much higher than 1.

Then we can approximate this A_f feedback system gain A_f is equal to β , which means that the system transfer function or primary input to primary output it can be decided by the feedback network. So, if we want to stabilize the specific parameters say Z_m then we should be selecting the first configuration. On the other hand if we say want to stabilize say voltage gain. So, if we want to stabilize the voltage gain, then we should be selecting the corresponding configuration here. So, then we can say that A_v that corresponding A_v of the feedback system if I call $A_v f$. So, this $A_v f$ it is getting converted into A_v divided by $1 + \beta$ the corresponding β into A_v . And again if I consider this is much higher than 1. So, this can be well approximated by $1/\beta$.

So, the basic objective of having this negative feedback system it is to stabilize this A whether it is Z_m , A_i , A_v or G_m . And it should be stabilized to a value which is defined by the feedback network, which can be decided by a designer based on the requirement. So, for every configuration while A is getting reduced the resistance input resistance and the output resistance, on the other hand they may have a different changes. Say for example, if I consider shunt-shunt configuration then input resistance it is expected to decrease by the same desensitization factor and also the output resistance it is getting decreased by the same factor.

So, while we are trying to stabilize this Z_m , you we should be aware that the corresponding input and output resistance they are also getting decreased. So, there may be different objective to follow this configuration or to get this configuration one of them it is of course, to stabilize the Z_m . The other objective on the other hand it can be reducing the input resistance and or reducing the output resistance.

So, this combination; however, this combination is fixed reducing Z_m and then reducing R_{in} and R_{out} it is fixed. And if we are reassured that we are looking for this characteristic then we can add the negative feedback system in this shunt-shunt configuration. And so, likewise if you if you are very clear that which parameter you liked to stabilize, namely defined by the parameter or the feedback network based on that you can select the corresponding circuit configuration. And also, you should be aware that what maybe its corresponding consequences. And the consequences as I said that for this case both R_{in} and R_{out} they are getting reduced.

On the other hand, for the second case for the second case the R_{in} it is getting reduced, but then R_{out} it is getting increased. So, likewise if I consider the third case excuse me, likewise if I consider the third case, we do have the third case here and for this third case the input resistance it is getting increased and output resistance on the other hand it is getting decreased.

So, likewise the final one the for series-series configuration feedback configuration both R_{in} and R_{out} they are getting increased. So, this table this summary it is very handy and this will be helping us to decide which configuration we are looking for to achieve some requirement. Namely to change the input and our output resistance or probably either current gain, voltage gain, trans impedance or trans conductance we like to stabilize defined by the feedback network. And while we do have the A it is having different possibilities, the corresponding feedback factor β_{FB} we are calling this β_{FB} to avoid confusion with the β of BJT transistor.

So, if A it is say Z_m the unit of β_{FB} it is more. And on the other hand, if the A it is trans conductance or the unit of β_{FB} if it is ohm. And on the other hand, if A is either current gain or voltage gain then β_{FB} it is unitless. So, now, we should also be aware that suppose if I decide one specific configuration and we know that the corresponding changes are happening then we should also be aware that what will be its consequences namely what will be the variations on the on the other parameter.

So, in the next slide we are also having one important table along with this table, which tells us that what may be the corresponding consequences on the other parameter.

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Summary of effects of negative feedback loop in amplifier (contd.)

Configuration names	S_{in}	S_o	A	R_{in}	R_{out}	Unit of β_{FB}
Voltage-Shunt (Shunt-Shunt)	I	V	$Z_m \downarrow$	\downarrow	\downarrow	Mho
Current-Shunt (Series-Shunt)	I	I	A_I	\downarrow	\uparrow	-
Voltage-Series (Shunt-Series)	V	V	A_V	\uparrow	\downarrow	-
Current-Series (Series-Series)	V	I	G_m	\uparrow	\uparrow	-

	A_I	A_V	G_m	Z_{in}
A_I	1	R_{in}/R_{out}	R_{in}	$1/R_{out}$
A_V	R_{out}/R_{in}	1	R_{out}	$1/R_{in}$
G_m	$1/R_{in}$	$1/R_{out}$	1	$1/(R_{in} \cdot R_{out})$
Z_m	R_{out}	R_{in}	$(R_{in} \cdot R_{out})$	1

$A_f = \frac{Z_m \downarrow}{R_{out} \downarrow}$ (No change)
 $A_f = \frac{A}{(1 + \beta_{FB} A)}$
 $G_m = \frac{Z_m \downarrow}{R_{in} \downarrow \cdot R_{out} \downarrow}$ (No change)
 • Which configuration?
 • Consequences!

So, here we do have the same table, which will be helping us to decide basic configuration. And then, we do have the other table here which it will be helping us to understand that what may be the consequences on the other parameter. So, say for instance if I consider this configuration and I know that Z_m got reduced by the desensitization factor like this one $1 + \beta_{FB} A$ or whatever you say $\beta_{FB} A$ into A . And R_{in} also is getting reduced by the same factor same thing for the R_{out} .

Now, suppose we like to know what maybe the what kind of changes are happening on the other parameter; namely current gain, voltage gain or trans conductance for this configuration. Then we need to know that how do we express those parameters in terms of this Z_m and R_{in} and R_{out} . Here we do have a table which is representing the other parameters say current gain in terms of Z_m and R_{in} and R_{out} .

So, if I see this column that gives an indication that the current gain of this circuit this configuration which is Z_m divided by R_{out} . So, we can say that this is indicating that current gain of the circuit A_I is equal to Z_m divided by R_{out} . And this table suggests that both Z_m and R_{out} they are getting reduced by the same factor. So, we can say that this A_I the current gain will not be having any change. So, we can say that it will be having no change.

Now, we can also work out on the other parameter say for example, if I consider the voltage gain. And the voltage gain its expression it can be given by this factor multiplied by Z_m . So, we can say that this A_v equals to Z_m divided by R_{in} . And again both the Z_m and R_{in} are getting reduced by the same factor desensitization factor and as a result here also there will not be any change. So, I should say here also we do not have any change.

On the other hand, if I consider say trans conductance. So, the trans conductance of the circuit under this configuration we can say that it can be expressed by in terms of Z_m and R_{in} and R_{out} by this or we can say that trans conductance of the circuit G_m equals to Z_m divided by R_{in} and R_{out} in the denominator. And as this table suggests that both R_{in} and R_{out} are getting reduced by the same factor and of course, Z_m is also getting reduced, but since we in the denominator we do have two factors.

So, we can say that the net effect here the denominator is getting reduced; that means, it is getting increased by the desensitization factor. So, I should say that by looking into by combining this table and combining this table we can also see the changes in the other parameter by considering the corresponding parameter here. Now, let you consider other example say let me clear it. Let you consider say the circuit in this configuration voltage-series or shunt-series configuration, which indicates that A_v it is getting stabilized or reduced by the desensitization factor.

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Summary of effects of negative feedback loop in amplifier (contd.)

Configuration names	S_{in}	S_o	A	R_{in}	R_{out}	Unit of β_{FB}
Voltage-Shunt (Shunt-Shunt)	I	V	Z_m	↓	↓	Mho
Current-Shunt (Series-Shunt)	I	I	A_I	↑	↑	-
Voltage-Series (Shunt-Series)	V	V	A_V	↑	↓	-
Current-Series (Series-Series)	V	I	G_m	↑	↑	Ohm

	A_I	A_V	G_m	Z_m
A_I	1	R_{in}/R_{out}	R_{in}	$1/R_{out}$
A_V	R_{out}/R_{in}	1	R_{out}	$1/R_{in}$
G_m	$1/R_{in}$	$1/R_{out}$	1	$1/(R_{in} \cdot R_{out})$
Z_m	R_{out}	R_{in}	$(R_{in} \cdot R_{out})$	1

$A_f = \frac{A}{1 + \beta A}$

• Which configuration?

• Consequences!

$A_f = \frac{A_V R_{in}}{R_{out}}$

So, we can say that this A it is A_v and appropriately you have to see what is the corresponding beta of course, it will be unitless and this is also A_v . And we suggest that after having the negative feedback configuration the system gain voltage gain it will be reduced by this factor. And while we are making this configuration as this table also suggests that the input resistance is getting increased by the desensitization factor. And the output resistance on the other hand it is getting decreased by that factor.

So, we are clear that this configuration it is having impact on voltage gain input resistance and output resistance. So, we can say that A_v we know for this configuration now we like to know what will be its effect on the current gain. So, to look at the effect on the current gain now, we will see this column which represents that the expression of all the parameters in terms of A_v and input resistance and output resistance.

So, if I see the current gain which is A_v times R_{in} divided by R_{out} . So, we can say this is equal to A_v divided by R_{in} and R_{out} sorry, let me let me write here A_I is equal to A_v times R_{in} divided by R_{out} . And as this table suggests that A_v it is getting reduced R_{in} on the other hand it is getting increased and R_{out} on the other hand it is getting decreased. So, in effect this A_I it is getting increased by this factor desensitization factor because this decrease and this increase they are getting canceled we do have the denominator is getting reduced and hence the net effect it is the A_I it is getting increased.

So, I should say that before we make the feedback connection whatever A_I we are having that A_I after making the feedback connection is getting increased by this desensitization factor. So, likewise if I consider say G_m . So, if I consider G_m here for this configuration and the G_m it is its expression in terms of A_v it is given here. So, this is equal to A_v divided by R_{out} and as this table suggests that both A_v and R_{out} are getting decreased and hence this G_m it is not having any change.

So, G_m remains unchanged. And then if you look into the trans impedance Z_m . So, if you look into Z_m . So, Z_m it is A_v into A_v into R_{in} . And this A_v it is getting decreased and R_{in} it is getting increased. So, again here also this Z_m is not having any change. So, both G_m and Z_m are not having any changes, but the A_I it is getting increased and A_v of course, it is getting decreased.

So, like that you can look into the other configurations namely series-shunt and maybe series-series and you can see what kind of changes are happening in the main parameters. And what kind of corresponding effect it is falling on the other parameters by looking into either the first column for the series-shunt connection or for series-series connection you can look into say third column to see what kind of changes are happening in other parameter.

So, I think this summary this summary table it is very useful to deploy the feedback configuration and deciding what configuration you are looking for to achieve some objective and also it will it is giving us the information about the changes or consequences on the other parameter. Now, let us look into more towards the actual circuit then.

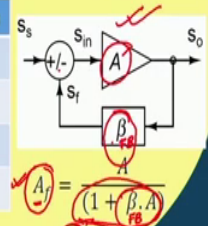
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Procedure to incorporate feedback loop in amplifier

Configuration names	S_{in}	S_o	A	A_{in}	R_{out}	Unit of β_{FB}
Voltage-Shunt (Shunt-Shunt)	I	V	Z_m	↓	↓	Mho
Current-Shunt (Series-Shunt)	I	I	A_I	↓	↑	-
Voltage-Series (Shunt-Series)	V	V	A_V	↑	↓	-
Current-Series (Series-Series)	V	I	G_m	↑	↑	Ohm

Steps to follow:

- ✓ Select the right feedback configuration
- ✓ Be aware of consequences
- ✓ To make the loop effective and intuitive
 - Consider the loading effect on "A" (i.e., use A')
 - Find useful range of β_{FB} providing $A' \approx A$, $\beta_{FB} \approx \beta_{FB}$ and $(A' \beta_{FB}) \gg 1$



$$A_f = \frac{A}{1 + \beta_{FB} \cdot A}$$

So, what we will be looking for it is. In fact, let me also summarize some other aspect namely. So, we do have the table we do have table, which gives us the information about how to select the configuration after that what you do?

So, rather what maybe the overall procedure to incorporate feedback loop in an amplifier. So, here we do have the list of the activities we have to do first thing is that we have to select the right circuit configuration. And also we need to be aware about the consequences what are the changes are happening, not only in input and output resistances, but also in other parameter such as transconductance or voltage gain and so and so.

And the third one is very important that, if we consider the practical application. And if you really want to make use of this feedback connection to create some effect. And if you really want to know what is the effect and intuitively if you want to calculate what is the

corresponding changes, then definitely we need to have a fair understanding of a suitable range of the parameters or rather feedback resistance or feedback network.

So, here we do have some guidelines which helps us to make the loop really effective according to this formula also we can intuitively say that what kind of changes are happening. So, what are the guidelines we do have? The first thing is that whenever we are considering say this feedback system model we assume that in case if there is any load and the effect of the load it has been considered in A which means that we need to consider A dash instead of A or at least we make sure that the effect of the external load it has been taken care if it is possible, to do so.

And then next important thing is that we need to find the meaningful feedback network or other feedback factor β FB. So, that the loading effect of this feedback network on A . And loading effect of the mixer circuit on feedback network you can say it is it can be ignorable. Or we can say that this A double dash it should be approximately equal to A dash A dash is the load external load effected gain. And also the β FB dash should be approximately equal to β FB. And if we follow this follow this appropriate range of β FB to satisfy these two condition then you can intuitively say that what kind of changes it is going to happen in the circuit.

Now, in case if you if these two approximations are still not valid, then also the circuit it will be working, but whatever the simplified expression whatever the equation it is giving us in intuition that what kind of changes it will happen that may not be really effective. And they are maybe a significant amount of deviation from the simplified theory the apart from this two approximation we also need to say that β into A or we can say that A dashed into β FB if it is much higher than 1, then only we can say that this is approximately 1 by β FB. And then only you can say that the feedback system characteristic it is solely or predominantly defined by the feedback networks parameter.

So, to achieve this property namely the A f solely defined by the feedback network we need to have meaningful selection of this β F B. And then only whatever the changes we are we

have summarized in this table, namely increase or decrease of the resistances defined by this desensitization factor it is directly applicable.

But of course, even if you are not satisfying these conditions then also the R_{in} and R_{out} will increase or decrease according to this table for this different configuration. Only thing is that their increase and decrease may not be defined by this same desensitization factor, we have to consider the corresponding deviation to get the more accurate change in the input and output resistance and also the change in A .

So, for practical circuit as I said it is better to have a meaningful range of β_{FB} . So, in the next slide let me discuss about what are the guidelines to really get a range of β_{FB} rather going little detail of whatever the guidelines we are discussing now.

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Procedure to incorporate feedback loop in amplifier (contd.)

- To make the loop effective and intuitive :
 - Consider the loading effect on "A" (i.e., use A')
 - Find useful range of β_{FB} providing
 - $A'' \approx A'$ and $\beta_{FB}' \approx \beta_{FB}$
 - $R_{in-\beta} \gg R_{out}$ for voltage sampling
 - $R_{out-\beta} \gg R_{in}$ for current mixing
 - and
 - $A' \cdot \beta_{FB} \gg 1$
 - $\beta_{FB} \gg \frac{1}{A'}$

$A_f = \frac{A'}{1 + \beta_{FB} A'} \approx \frac{1}{\beta_{FB}}$

$R_{out-\beta}$ $R_{in-\beta}$

So, yeah so, to make the loop really effective and intuitive, first thing is that let you consider the loading effect on A. So, we should say that instead of A, it is better to consider A dash after considering the external load effect.

So, in case if you have external load R_L and if you consider that R_L on the circuit. Then we can get load effected A and then we can proceed further. Namely we can try to calculate what may be the A f in terms of this A dash divided by $1 + \beta_{FB}$ and then A dash.

Now, next thing is that we need to find the suitable range of the β_{FB} of course, based on the nature of A β_{FB} it is complimentary in nature. So, that this product it becomes unitless rather you may say that loop gain minus of loop gain it becomes unitless. And that is once you once you know that what maybe the nature of this β_{FB} next thing is that what is the meaningful value of it.

And to get that to get a suitable range we do have two things to satisfy as just now I was talking about. A double dashed it is approximately A dashed. And what is A double dash? It is the loading effect of the input resistance of the feedback network say $R_{in\beta}$, if it is much higher than the R_{out} of the amplifier particularly for voltage sampling then we can say that this A double dash it is approximately equal to A dash.

So, if I if I ensure that this condition is getting satisfied, then you can say that loading effect of the feedback network on the forward amplifier it can be ignored. So, pictorially you may say that suppose this is the amplifier and it is having R_{out} and suppose we are making a voltage sampling, which means it is a parallel connection and we do have the input resistance of the feedback network which is $R_{in\beta}$. And so, this $R_{in\beta}$ if this $R_{in\beta}$ it is a much higher than this resistance then you can say that the loading effect on the amplifier or this output voltage hardly changes even if I consider this $R_{in\beta}$.

So, this is specifically true for voltage sampling and of course, for current sampling the condition it will be the other way. On the other hand if I consider the input resistance of the amplifier R_{in} and then, we do have say current mixing. So, if we have a current mixing here.

So, this is shunt configuration and then we do have R_{out} of the feedback network β . So, if I consider this shunt mixing or current mixing then if we satisfy this condition.

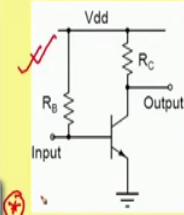
If I say that this R_{out} β it is much higher than this input resistance here. Then we can say that the loading effect on the feedback network from the input resistance of the amplifier it is ignorable. And hence, if I satisfy this condition then we can say that this β_{FB} dash it is approximately equal to β_{FB} .

So, this is giving us a good range of or it is helping us to define what may be the suitable value of R_{in} of the feedback network R_{in} β and R_{out} β . And then also if you consider that this equation, if it is giving us giving us the expression of A_m sorry A_f in terms of β_{FB} to get this we want this part should be much higher than 1. So, we can say that A_{dash} into β_{FB} it should be much higher than 1 and this gives us the β_{FB} it is much higher than 1 by A_{dashed} .

So, this two condition here along with this condition, it will be helping us to find what is the suitable range of for the feedback network circuit components and that will be helping us to get very effective feedback connection. I think this will be very clear once you consider one practical circuit. Probably, I do have the practical circuit in the next slide yeah.

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Application circuit-1

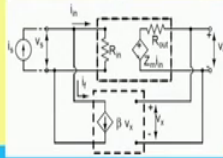


Configuration names	Sin	So	A	Rin	Rout	Unit of β_{FB}
Voltage-Shunt (Shunt-Shunt)	I	V	Z_m	↓	↓	Mho
Current-Shunt (Series-Shunt)	I	I	A_I	↓	↑	-
Voltage-Series (Shunt-Series)	V	V	A_V	↑	↓	-
Current-Series (Series-Series)	V	I	G_m	↑	↑	Ohm

We want stable Z_m defined by feedback network

Feedback configuration: **Voltage-Shunt (Shunt-shunt) feedback**

Input signal:
 Output signal:
 Forward amplifier gain:
 T.F. of F.B. Network :
 Rin: Rout:



So, here we do have one application circuit shown here, which is a common emitter amplifier. So, we do have common emitter amplifier. In fact, this is fixed by us common emitter amplifier. And we will be talking about its feedback connection and our main target it is that we want a stable Z_m defined by the feedback network. So, this is our main objective. And then we will be discussing how to decide the configuration and then how to select the component value; but before that let me take a short break and then I will come back. 2 minutes.