

Analog Electronic Circuits
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Lecture - 94
Feedback System (Part- E)

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Numerical example on voltage amp. having Feedback
(Shunt-Series / Voltage-Series feedback system)

Given: $R_{in} = 1\text{ k}\Omega$, $R_{out} = 4\text{ k}\Omega$, $A_v = 200$ and $\beta = 0.095$, $V_s = 100\text{ mV}$

Find the values of A_{v-f} , R_{in-f} , R_{out-f} and V_o

Case I: With Ideal feedback network ($R_{in-\beta} \rightarrow \infty$ and $R_{out-\beta} = 0$):

Case II: With Ideal feedback network ($R_{in-\beta} \rightarrow 200\Omega$ and $R_{out-\beta} = 1\text{ k}\Omega$)

$A_{v-f} = \frac{V_o}{V_s} = ?$

So, welcome back after the break. So here we do have numerical example and what is our objective here? It is that we need to find the voltage gain of the feedback system, input resistance, output resistance of the feedback system and the output voltage for an input voltage or the signal voltage of 100 millivolt.

And the parameters of the feedback systems are given here input resistance and output resistance of the forward amplifier and the gain of the forward amplifier it is 200 feedback network, the feedback factor it is 0.095. So to start with, let me consider this relatively

simpler case, case 1 where we consider ideal feedback network having the input resistance it is infinite and its output resistance on the other hand it is 0 as we are generating voltage.

So 0 output resistance it creates the ideal Thevenin equivalent voltage. So let me clear the board, yes. So to start with, let we have the derivation of this A_v rather A_v dashed or rather A_v of the feedback system A_v -f.

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Numerical example on voltage amp. having Feedback
(Shunt-Series / Voltage-Series feedback system)

Given: $R_{in} = 1k\Omega$, $R_{out} = 4k\Omega$, $A_v = 200$ and $\beta = 0.095$, $V_s = 100\text{ mV}$

Find the values of A_{v-f} , R_{in-f} , R_{out-f} and V_o

Case I: With Ideal feedback network ($R_{in-\beta} \rightarrow \infty$ and $R_{out-\beta} = 0$):

Case II: With Ideal feedback network ($R_{in-\beta} = 200\Omega$ and $R_{out-\beta} = 1k\Omega$)

Handwritten calculations on the slide:

$$A_{v-f} = \frac{A_v}{(1 + \beta A_v)} = \frac{200}{(1 + 0.095 \times 200)} = \frac{200}{20} = 10$$

$$R_{in-f} = R_{in}(1 + \beta A_v) = 1k\Omega(20) = 20k\Omega$$

$$R_{out-f} = \frac{R_{out}}{(1 + \beta A_v)} = \frac{4k\Omega}{(20)} = 200\Omega$$

$$V_o = 10 \times V_s = 10 \times 100\text{ mV} = 1\text{ V}$$

As we know that this A_v -f it is the forward amplifier gain A_v divided by 1 plus beta into A_v . So the A_v it is given 200 and on the other hand, feedback factor it is 0.095 and A_v it is 200.

In fact, we have picked up these numbers such that we do have in the denominator this part it is becoming twin 19 and then we do have 1 here. So that is giving us in the denominator it is 20. So the gain of the feedback system it is 10. Now, to find the value of the input resistance

$R_{in f}$. As you can now guess that since we do have series connection here $R_{in f}$, it is getting amplified by the desensitization factor.

So that should be R_{in} multiplied by $1 + \beta A_v$. And R_{in} it is 1 k multiplied by this factor it is similar to whatever the calculation we have done. So this part it will be 20 and that gives us 20 kilo ohms.

So note that just by this feedback network the input resistance it is getting increased by a factor of 20 which means that if the main amplifier input resistance it was 1 k, the feedback system input resistance it is becoming 20 k. $R_{in f}$ it is 20 k. So whenever for some application, we have to increase the input resistance we should consider the series mixer and then we can enhance the input resistance.

Now to calculate the output resistance $R_{out f}$. So, now here we do have shunt connection. So the shunt connection it is reducing the resistance which means that the output resistance it will be R_{out} divided by $1 + \beta A_v$. And R_{out} it is 4 k divided by this factor which is 20. So that is giving us 20 rather, 200 ohms.

So now we obtained input resistance of the feedback system, output resistance of the feedback system and next thing is that what is the output voltage? It is very straight forward. From here to here, the gain we obtain it is $A_v f$. So, here to here the gain it is 10. So it is giving us very simple situation. So the output voltage V_o it is 10 times V_s . So that is giving us 10 into 100 millivolt. So that is equal to 1 volt.

So the case 1, it is relatively straightforward, we have used the whatever the formula we have obtained namely, the gain got decreased then and the voltage gain got decreased, input resistance got increased and then output resistance and got decreased. Now if I consider the IInd case, I should not say it is ideal. So this part may be ideal, but with finite resistance. In fact, we are considering relatively low input resistance.

So we are considering non-ideal rather non-ideal feedback, and input resistance it is 200 and output resistance coming in series. So, that is 1 kilo ohm. With that we need to find the

corresponding feedback system gain input resistance and output resistance. It is very clumsy I should say, we need to be little careful.

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Numerical example on voltage amp. having Feedback
(Shunt-Series / Voltage-Series feedback system)

Given: $R_{in} = 1k\Omega$, $R_{out} = 4k\Omega$, $A_v = 200$ and $\beta = 0.095$, $V_s = 100\text{ mV}$

Find the values of $A_{v,f}$, $R_{in,f}$, $R_{out,f}$ and V_o ← 655.73 mV

Case I: With Ideal feedback network ($R_{in,\beta} \rightarrow \infty$ and $R_{out,\beta} = 0$):

$$A_v = A_v \times \frac{R_{in,\beta}}{R_{in,\beta} + R_{out,\beta}} = 200 \times \frac{0.2}{4.2} = \frac{200}{21} = 9.5238$$

Case II: With Ideal feedback network ($R_{in,\beta} = 200\Omega$ and $R_{out,\beta} = 1k\Omega$)

$$\beta' = \beta \times \frac{R_{in}}{R_{in} + R_{out,\beta}} = 0.095 \times \frac{1k}{1k + 1k} = \frac{0.095}{2} = 0.0475$$

$$A_{v,f} = \frac{A_v}{(1 + \beta' A_v)} = \frac{200}{1 + 0.0475 \times 200} = \frac{200}{1 + 9.5} = \frac{200}{10.5} = 19.0476$$

$$A_{v,f} = \frac{9.5238}{1 + 0.095 \times 9.5238} = \frac{9.5238}{1 + 0.905} = \frac{9.5238}{1.905} = 5.00$$

(Note: The handwritten calculations in the image show a different path for $A_{v,f}$ resulting in 6.5573, which appears to be a miscalculation or a different interpretation of the feedback factor.)

So, before we start. So this should be non-ideal, I should have said it is non-ideal.

Before we start, let us consider since we do have finite input resistance and output resistance of the feedback network, the input resistance here it is affecting the output port. So the voltage will be getting here, it is not same as this internal voltage. Rather, we may say that load affected voltage, let me use different color here. So we need to be careful that A_v it is giving us 200, but $A_{v,dashed}$ it is different.

So, how do we find this $A_{v,dashed}$? So the way we define this $A_{v,dashed}$, it is A_v multiplied by whatever the load we do have here, it may be external or it may be internal part of the

feedback network. So in this case, R_{in} in beta it is loading. So, the loading factor it is R_{in} in beta divided by R_{in} in beta plus R_{out} . In fact, this is 200 multiplied by this is 200 ohm. So, 0.2 k and then we do have this is 4 k. So, that is 4.2 and that gives us 200 divided by 21. In fact, that is becoming 9 point something.

So, I have some calculation for you. So this is 9.523 right. So we have to keep this in mind. Likewise, when we see the feedback network, since we do have output resistance of 1 k. So whatever the voltage we are developing here, beta into V_x it is not directly coming there. In fact, if I consider R_s equals to 0, the corresponding load affected beta called beta dashed is equal to beta multiplied by R_{in} divided by R_{in} plus R_{out} of the feedback network. So this is 1 k this is also 1 k.

So, that gives us this part it is 0.5. So we can say this is equal to 0.095 by 2. So a priori we should keep these 2 parts, load affected A and load affected beta ready for our consideration. Now if we have to find what is the corresponding gain, voltage gain of the entire network. So, A_{vf} we can say load affected A_v divided by 1 plus load affected beta and then load affected A_v .

So we do have here it is 9.5238 here divided by 1 plus 0.95 by 2 into 9.5238. In fact, again I have done this calculation. In fact, in this case the desensitization factor this part it has drastically changed. So if you consider its value here and here the value here it is 1.45238. So the value here for this A_{vf} it is 9.5238 divided by 1.45238. And that is becoming 6.5573. So earlier the gain from here to here the gain it was 10 now it is 6.55.

So if we are applying say there is 100 millivolt. So what we are expecting this voltage the corresponding voltage here it will be 655.73 millivolt. As the gain of this entire circuit for this case it is 6.557. So, this is also obtained. So next thing it is that, what is the input resistance and output resistance of the feedback system? Again we have to keep this in mind that A_{vd} it is 9.5238 and beta dashed it is this one and the desensitization factor corresponding desensitization factor is given there.

So to start with let you consider input resistance, let me clear the board again.

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Numerical example on voltage amp. having Feedback
(Shunt-Series / Voltage-Series feedback system)

Given: $R_{in} = 1\text{k}\Omega$, $R_{out} = 4\text{k}\Omega$, $A_v = 200$ and $\beta = 0.095$, $V_s = 100\text{ mV}$

Find the values of A_{v-f} , R_{in-f} , R_{out-f} and V_o

Case I: With Ideal feedback network ($R_{in-\beta} \rightarrow \infty$ and $R_{out-\beta} = 0$):

Case II: With Ideal feedback network ($R_{in-\beta} \rightarrow 200\Omega$ and $R_{out-\beta} = 1\text{k}\Omega$):

Handwritten calculations on the slide:

$$A_v' = \frac{200}{1 + 0.095} = 183.238$$

$$\beta' = \frac{0.095}{2} = 0.0475$$

$$D' = (1 + \beta' A_v') = 1.45238$$

$$A_{v-f} = \frac{A_v'}{D'} = \frac{183.238}{1.45238} = 126.179$$

$$R_{in-f} = R_{in} (1 + \beta' A_v') = 1\text{k}\Omega \times 1.45238 = 1452.38\Omega$$

$$R_{out-f} = R_{out} (1 + \beta' A_v') = 4\text{k}\Omega \times 1.45238 = 5809.52\Omega$$

$$R_{in-f} = R_{in} + R_{out-\beta} = 1\text{k}\Omega + 1\text{k}\Omega = 2\text{k}\Omega$$

$$R_{out-f} = R_{out} + R_{in-\beta} = 4\text{k}\Omega + 200\Omega = 4200\Omega$$

$$A_{v-f} = \frac{A_v R_{out-\beta}}{R_{in-f} + R_{out-\beta}} = \frac{200 \times 1\text{k}\Omega}{2\text{k}\Omega + 1\text{k}\Omega} = 66.667$$

Let me also keep A_v dashed which just now we have obtained it is 9.5238 and beta dashed it is 0.095 by 2 and also 1 plus beta dashed and A_v dashed it is what we say, it is desensitization factor it was 1.45238. So, we need to find what will be the R_{in-f} . So we are knowing that the input resistance it will be getting increased. But should we consider R_{in} multiplied by 1 plus beta dashed A_v dashed? Should I be getting this value correct?

Now this R_{in} , it is representing only this resistance. In fact, there it is having 2 alternate approaches. So definitely this is not correct. We should consider what is the corresponding R_{in} dashed. And what do we mean by R_{in} dashed? It is we have to consider this $R_{out-\beta}$ also along with this R_{in} . So the R_{in} dashed. In fact, this R_{in} dashed, if I put R_{in} dashed

then it is of course, it is correct. Where these R_{in} is equal to the input resistance of this circuit in absence of this feedback signal.

So if I say this signal it is 0, the input resistance it is R_{in} and R_{out} is in series. So, R_{in} is equal to $R_{in} + R_{out}$. So that is equal to 200, sorry 2 kilo. So, we do have 1 k here and another k here. So it is basically 2000 ohms. So the input resistance it will be 2000 here multiplied by $1 + \beta$.

So, we do have this number 0.45238 and that is giving us a value which is 2.904 around 4, 7 kilo ohm. So earlier the input resistance it was 20 kilo ohm. Now that got drastically reduced to 2.9 only. In fact, whenever and also we already have obtained A_v . So, its value it was 6.5579.

So, for both this R_{in} and A_v it is having alternate way of calculating say to explain say this part, let me use the alternate expression R_{in} can also be considered as a R_{in} multiplied by $1 + \beta$ into A_v in series with R_{out} . So you might have seen here what are the things sorry A_v what are the things we do have different terms in this expression and this expression.

In fact, both of them are same first of all here we consider R_{in} only without dashed. So, here we do have 1 k and then here we do not have β . So we do have one plus 0.095 only, but then A already got affected by whatever the resistance we do have. So that is A_v we have to consider A_v . So that is multiplied by 9.5238 in series with 1 k. So if you calculate here, what we will be getting it is this part it is coming 1 k multiplied by 1 point.

In fact, I do have the calculation for you. This will be 1.9047 plus this 1 k. In fact, this part it is becoming 1.9047 k and this is 1 k. So that gives us 2.9047 k. It is same as whatever you do have. So we do have this alternate approach. In fact, same way you can find for this A_v also. In fact, we have used this expression of A_v where we considered A_v divided by $1 + \beta$.

So the alternate approach to calculate this A_{v_f} let me use this space it is we can consider A_{v_f} equals to A_v divided by $1 + \beta$ dashed into A_v multiplied by R_{out_f} if, I should consider not R_{out_f} rather R_{in} . R_{in} of the feedback network divided by R_{in} of the feedback network plus R_{out_f} ok.

So, this calculation I will be showing you once we get this R_{out_f} . So let me find this R_{out_f} first and then we will be discussing about the alternate approach of finding this A_{v_f} . Similar to R_{in_f} . So to, now next thing is that we are going to calculate R_{out_f} for this case. But before that, let me clear the board. Please keep the information in mind that A_v dashed and β dashed and those things.

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Numerical example on voltage amp. having Feedback
 (Shunt-Series / Voltage-Series feedback system)

Given: $R_{in} = 1k\Omega$, $R_{out} = 4k\Omega$, $A_v = 200$ and $\beta = 0.095$, $V_s = 100\text{ mV}$

Find the values of A_{v_f} , R_{in_f} , R_{out_f} and V_o

Case I: With Ideal feedback network ($R_{in_\beta} \rightarrow \infty$ and $R_{out_\beta} = 0$):

Case II: With Ideal feedback network ($R_{in_\beta} = 200\Omega$ and $R_{out_\beta} = 1k\Omega$)

Handwritten calculations on the slide:

$$A_v' = \frac{A_v}{1 + \beta} = \frac{200}{1 + 0.095} = 183.5$$

$$R_{out_f} = \frac{R_{out}}{1 + \beta A_v} = \frac{4k\Omega}{1 + 0.095 \times 200} = \frac{4k\Omega}{20} = 200\Omega$$

$$R_{in_f} = R_{in} \parallel R_{in_\beta} = 1k\Omega \parallel 200\Omega = 163.3\Omega$$

$$R_{out} = R_{out} \parallel R_{out_\beta} = 4k\Omega \parallel 1k\Omega = 800\Omega$$

Final results from the slide:

- $A_{v_f} = 183.5$
- $R_{in_f} = 163.3\Omega$
- $R_{out_f} = 200\Omega$
- $V_o = 100\text{ mV} \times 183.5 = 18.35\text{ mV}$

So to get the R_{out_f} what is the formula we can use? There are 2 formulas, one is we can consider R_{out} dashed divided by $1 + \beta$ dashed and A_v dashed all are load

affected. So, where this R_{out} dashed R_{out} dashed it is the R_{out} here and if we have this R_{in} beta whatever the net output resistance we will be getting without considering this feedback network. So that is the R_{out} .

And if I consider this R_{out} dashed, it is essentially R_{out} coming in parallel with R_{in} beta and this is equal to 4 k in parallel with 0.2 k . So, this multiplied by 0.2 k divided by 4.2 k right. And again for this also, I have some calculation for you, I was having 190.47 ohms only. As you can see that this resistance it is quite small. So that is dominating and so, this resistance it is very small.

So, the β dashed and A_v dashed we already have calculated before. So A_v dashed it is 9.5238 and β dashed it is 0.095 by 2 and this factor it is 1.4 something right $4\ 5$. So that gives us R_{out} equals to 190.47 divided by 1.45238 . In fact, this is equal to around 131 ohms only. So similar to R_{in} for R_{out} also we do have alternate expression. So what is the corresponding expression? This R_{out} we can say this is R_{out} divided by $1 + \beta$ dashed, but A_v ok. So this is without considering this resistance.

Now all of a sudden if we say that this is appearing. So we need to consider then R_{in} beta in series but while you are doing this, you need to be careful that not only this R_{out} we are considering the inherent R_{out} there. But also this A_v it is not load affected ok. and in fact, it can be shown that this is this part it is coming 10.5 . So, this is R_{out} it is 4 k divided by this is 10.5 because the A_v it is 200 so that is why it is 10.5 . This is in parallel with 0.2 k and in fact, this is also becoming 131 ohms .

So we do have this equation, this equation as well as this equation. Again, I like to; I like to suggest you that these 2 expression difference are here we do have R_{out} dashed, but here we do not have any R_{out} dashed. Also here, we do have A_v dashed, but this A_v is not having any dashed this is R_{in} beta is already it has been captured here and here. So, we do not consider this R_{in} beta here, but in this case on the other hand R_{in} beta it was completely ignored, now we can incorporate that.

But while we are doing this exercise the beta however, it is remaining load affected. So when the conclusion is that whenever we are trying to see the output resistance, either we can incorporate this resistance as part integral part of the amplifier and accordingly, we modify this R_{out} to R_{out} dashed and also this A_v to A_v dashed and then you can use this equation. Or the alternate approach is that we can keep this part aside thinking that this resistance it is here and here the resistance it is infinite it has been shifted there.

And then we do calculate the whatever the resistance we do have by this formula where both R_{out} it is inherent R_{out} A_v it is also inherent A_v and then we consider this R_{in} beta into consideration by considering its parallel connection. So now we do have the value of this R_{out} if whether we do have this equation or this equation. In fact, if you consider this part this part without considering this we obtain.

So, we may say that this is also some form of the R_{out} f without considering R_{in} beta. So, as I was telling that A_v A_v f it is having two approaches one approach you already have discussed by considering this A_v dashed and beta dashed together. The second approach now we are going to talk it is the following.

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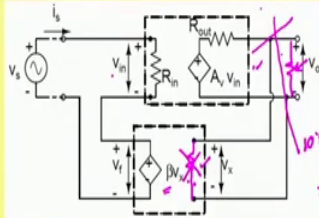
Numerical example on voltage amp. having Feedback
(Shunt-Series / Voltage-Series feedback system)

Given: $R_{in} = 1\text{ k}\Omega$, $R_{out} = 4\text{ k}\Omega$, $A_v = 200$ and $\beta = 0.095$, $V_s = 100\text{ mV}$

Find the values of $A_{v,f}$, $R_{in,f}$, $R_{out,f}$ and V_o

Case I: With Ideal feedback network ($R_{in,\beta} \rightarrow \infty$ and $R_{out,\beta} = 0$):

Case II: With Ideal feedback network ($R_{in,\beta} \rightarrow 200\Omega$ and $R_{out,\beta} = 1\text{ k}\Omega$)



$$A_{v,f} = \frac{A_v}{(1 + \beta A_v)} \times \frac{R_{in,\beta}}{(R_{out,f} + R_{in,\beta})}$$

$$= \frac{200}{(1 + \frac{0.095}{2} \times 200)} \times \frac{200}{\left\{ \frac{4\text{ k}}{(1 + \frac{0.095}{2} \times 200)} + 200 \right\}}$$

$$= \frac{200}{10^5} \times \frac{200}{\left[\frac{4000}{10^5} + 200 \right]} = 6.55\%$$

$R_{out,f} = \frac{R_{out}}{(1 + \beta A_v)}$

So, if we have say, we need to find what will be the $A_{v,f}$? What we can say that let we postpone the effect of R in beta. So this effect of this R in beta will be postponing. So instead of putting it here, if we connect it here and first we calculate what is the corresponding A_v here and then we can consider this part.

So to do. So the without considering this the A_v internal A_v it is or internal $A_{v,f}$ or intermediate $A_{v,f}$ it is A_v divided by $1 + \beta$ into β dashed into A_v multiplied by whatever the loading effect it will coming due to this β in R in beta sorry R in beta. So, that is that factor it is R in beta divided by R out of this intermediate resistance. So let me call this is say $R_{out,f}$ star plus R in beta where $R_{out,f}$ star is essentially R_{out} divided by $1 + \beta$ dashed into A_v .

So that means, the whatever the in output resistance we are having without considering this R in beta. And if you do the calculation here A_v of course, we do have 200 and this is 1 plus so, this is getting 0.095 by 2 into 200 . And then we do have this resistance it is 200 ohms divided by this resistance which is 4 k divided by 1 plus 0.9 0.095 by 2 into 200 right.

So this is this resistance plus R in beta that is 200 . In fact, this part it is 10.5 . So that gives us 200 here divided by 10.5 multiplied by 200 ohms here divided by 4 k 4000 divided by 10.5 plus 200 . In fact, this is also coming equal to 6.557 . In fact, this is same as whatever earlier we obtained the value of this A_v .

So, we do have alternate approaches to find this A_v . So either we consider this resistance as internal part of it or we can postpone its consideration. But of course, we have to keep in mind that beta we need to consider here. So that is how we can get the value of this the voltage gain input resistance output resistance and output voltage in terms of whatever the forward amplifier parameters and feedback networks parameters are given to you.

So similar kind of exercise you can do for other configurations. So right now it is voltage amplifier and the in the next slide we do have another numerical examples.

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Numerical example on Trans-conductance amp. having F.B.
 (Series-Series / Current-Series feedback system)

Given: $R_{in} = 1k\Omega$, $R_{out} = 4k\Omega$, $G_m = 100 \text{ mA/V}$ and $\beta = 90 \Omega$, $V_s = 100 \text{ mV}$

Find the values of G_{m-f} , R_{in-f} , R_{out-f} and I_o

Case I: With Ideal feedback network ($R_{in-\beta} = 0\Omega$ and $R_{out-\beta} = 0\Omega$):

Case II: With Ideal feedback network ($R_{in-\beta} \rightarrow 100\Omega$ and $R_{out-\beta} = 4k\Omega$):

Handwritten calculations:

$$G_{m-f} = \frac{G_m}{1 + \beta G_m} = \frac{100 \text{ mA/V}}{1 + \frac{90 \Omega \times 100 \text{ mA/V}}{1000 \Omega}} = 10 \text{ mA/V}$$

$$R_{in-f} = R_{in}(1 + \beta G_m) = 1k\Omega \times 10 = 10k\Omega$$

$$R_{out-f} = R_{out}(1 + \beta G_m) = 4k\Omega \times 10 = 40k\Omega$$

$$I_o = 100 \text{ mV} \times 10 \text{ mA/V} = 1 \text{ mA}$$

At the bottom right, a small video inset shows a man speaking.

It is very similar. However, in this case, the circuit is trans-conductance amplifier and so the signal here it is current. So, the sampler it is series and it is sampling current and the mixer it is series as the signal here it is voltage. So here again, the gain of this circuit it is G_m it is given to us which is 100 milli ampere per volt, input resistance remains 1 k output resistance here. Of course, this is in the form of conductance. So, that resistance it is coming it is 4 k. Beta on the other hand it is 90 ohms.

You might have observed that since this G_m its unit it is 1 by ohm the expected unit of beta it is it should be ohm and the value here it is 90, the input voltage we are feeding here it is 100 millivolt and you need to find what will be the output current? Also you need to find what will be the overall transfer function? Namely, overall Trans-conductance G_{m-f} of the feedback system G_{m-f} .

Then input resistance of this circuit and then the and the output resistance particularly, whatever the output conductance we will see. So whatever the output conductance we will see that is $1/R_{out}$. So that also you can find. Now, to start with, we can consider the ideal feedback network and then after that we can consider non-ideal situation. So in the ideal situation of course, it is pretty straight forward. So both A or I should say G_m and β they are not affected by load.

So to avoid the loading effect, we do have 0 load resistance. Here, the resistance is 0 and here the resistance 0 . So, there is no loading effect. So directly we can use this G_m and this β . So the desensitization factor it is equals to $1 + \beta$ into G_m and here it is $1 + G_m$, it is 100 and 100 milli.

So, I should say this divided by 1000 and β is 90 . So what we have here it is desensitization factor it is 10 . So for this case this case at least we can say. So, right now we are considering the first case G_m f. So, G_m f equals to this G_m divided by $1 + \beta$ into G_m . So that is equal to 10 milli ampere per volt. In fact, from that directly you can say that this i naught it will be 100 millivolt multiplied by 10 milli ampere per volt. So, that gives us 1000 micro or 1 milli ampere for this signal.

So likewise, we can calculate the input resistance. So, R_{in} f as you can anticipate the input resistance it will be increased. So, original input resistance R_{in} it is 1 k multiplied by the desensitization factor $1 + \beta$ into G_m .

So, this is we do have 1 k multiplied by 10 . So, that is equal to 10 kilo ohm. Similarly, if I consider output resistance R_{out} , here also since it is series connection. So we are expecting that R_{out} will also be getting increased by this desensitization factor namely, $1 + \beta$ into G_m .

So we do have original resistance for the forward amplifier it is 4 k multiplied by desensitization factor of 10 . So that gives us 40 kilo ohm. So, that is how we can calculate for the case 1. So likewise, you can make an attempt to consider the second part.

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Numerical example on Trans-conductance amp. having F.B.
 (Series-Series / Current-Series feedback system)

Given: $R_{in} = 1k\Omega$, $R_{out} = 4k\Omega$, $G_m = 100 \text{ mA/V}$ and $\beta = 90 \Omega$, $V_s = 100 \text{ mV}$

Find the values of G_m , R_{in} , R_{out} and I_o

Case I: With Ideal feedback network ($R_{in} = 0\Omega$ and $R_{out} = 0\Omega$):
 $R_{out}' = 4.1k\Omega$
 $R_{in}' = 1+4 = 5k\Omega$

Case II: With Ideal feedback network ($R_{in} = 100\Omega$ and $R_{out} = 4k\Omega$)

$G_m = 100 \times \frac{4}{4.1} = 97.56 \text{ mA/V}$

$\beta = \beta \cdot \frac{R_{in}}{R_{in} + R_{out} \cdot \beta} = 90 \times \frac{1}{5} = 18$

$G_m - I = \frac{G_m}{(1 + \beta' G_m)}$

$i_o = G_m \cdot V_{in} \times \frac{R_{out}}{R_{out} + R_{in} \cdot \beta} = G_m \cdot V_{in}$

$R_{in-f} = R_{in} (1 + \beta G_m)$
 $R_{out-f} = R_{out} (1 + \beta G_m)$

So, I may not be going all the solution for that, but I am going to give you hint for this non-ideal situation, where the input resistance it is 100 ohms and the output resistance of this circuit it is say 4 kilo ohm. So to start with, we need to find what is the corresponding G_m dashed and beta dashed.

So from that, probably we can get a hint of how to calculate G_m f. G_m whenever we are saying that G_m dashed which means that what may be the current in presence of this resistance? If this is having 0 resistance this entire current it was flowing through this circuit. So, the i_o it was simply G_m into V_{in} .

Now in presence of this resistance, this current it is getting segregated; 1 part it is flowing through this the other part it is flowing through this one and whatever the part it is flowing

through this that gives us this i_o . So to get this i_o in presence of this resistance, we need to consider this factor and that is R_{out} divided by $R_{out} + R_{in}$ of the beta network.

So, we can say this is the G_m dashed into v in where G_m dashed equals to G_m . G_m it is 100 milli into R_{out} it is 4 divided by 4.1. So, it is whatever the value it is coming. So, that is equal to 400 divided by 4.1. So, that 97.56 milli ampere per volt. So likewise, you can also calculate the corresponding beta dashed.

And this beta dashed it is of course, here it is the signal it is we are mixing in the form of voltage, and the beta dashed it is the original beta multiplied by whatever the potential division it is happening due to this 4 k resistance here along with this input resistance R_{in} and its expression it is R_{in} beta into R_{in} divided by $R_{in} + R_{out}$ of beta network.

So that is beta it is 90 and R_{in} it is 1 k and this is 4 k. So, this is 1 by 5. So, this is 1 k this is 4 k. So that gives us and this beta dashed it is equal to 18. So, that is how we can calculate G_m dashed and the beta dashed. So likewise, you can find what will be the R_{out} dashed; that means, the output resistance in presence of this 100 ohms.

So, definitely this resistance it is in fact, if you see here, this resistance it is coming in series. So, this will be 4.1 kilo ohm and likewise, R_{in} dashed we should consider. So in absence of this part R_{in} dashed it is 1 k plus 4 k that is the 5 k. So now we obtain the load affected, all these load affected parameters and from that you can calculate what will be the G_m f and then R_{in} f and R_{out} f and so and so on for this case.

So what is the G_m f? You may recall similar to whatever we have done for the previous case, it should be G_m dashed divided by 1 plus beta dashed into G_m dashed. We do have alternate expression also. But let we consider this. So likewise, when you consider R_{in} of the feedback circuit. So, what should we consider? We should consider R_{in} load affected and we know that input resistance it is getting increased by a factor of 1 plus beta dashed into G_m .

Sorry G_m dashed and likewise, whenever we are talking about R_{out} , R_{out} of the feedback system here the output resistance it is getting increased compared to its R_{out} dashed. R_{out}

dashed we already have 4.1 k multiplied by $1 + \beta$ dashed into G_m dashed and G_m dashed it is given here and β dashed it is 18 , so, we can find what will be the corresponding factor. So I think you yourself can calculate this one it is now it is a matter of using your calculator.

(Refer Slide Time: 48:07)

The slide is titled "Conclusion" in yellow text on a dark blue background. The main content is on a yellow background and includes a list of topics with checkboxes and handwritten notes:

- Basic concepts of a feedback system
- Basic types of feedback systems
 - Positive
 - Negative
- Transfer characteristic of a feedback system
- Four basic configurations of F.B. sys. and their characteristics
 - Shunt-series / Voltage-series
 - Series-shunt / Current-shunt
 - Shunt-shunt / Voltage-shunt
 - Series-series / Current-series
- Numerical examples

Handwritten notes include:
 $A_f = \frac{A}{1 + \beta A}$
 $L.G = -\beta A$
 $D = 1 + \beta A$
 A_f, R_{in-f}, R_{out-f}

So, to summarize all these 4 sub-lectures, what we have discussed in this topic of feedback system. So, far we have talked about basic concepts of the feedback system, there we have introduced how we define the feedback system and then we have talked about 2 basic types of feedback mechanism or feedback system namely, positive feedback type and negative feedback types feedback system.

And subsequent discussion it is mostly related to negative feedback system. So then, we have talked about transfer characteristic of feedback system namely, feedback system transfer

characteristic A_f is equal to 1 by sorry A divided by $1 + \beta$ into A . So also, we have talked about loop gain which is equal to β into A then, D sensitivity factor, D is equal to $1 + \beta$ into A .

Then we have talked about 4 basic configurations which normally it is common in electronic circuit and we have discussed about their characteristic. So these are the enlisted 4 basic configurations we have discussed about how the gain it is getting changed.

And also we have talked about how the input resistance and output resistance of the system it is getting changed by the desensitization factor. And then we have discussed about 2 numerical examples associated with 2 feedback configure different types of configuration starting with ideal situation and then also we have moved to non-ideal situation. I think that is all we need to cover.

Thank you for listening.