

Analog Electronic Circuits
Prof. Pradip Mandal
Department of Electronics and Electrical Communication Engineering
Indian Institute of Technology, Kharagpur

Lecture – 61
Multi-Transistor Amplifiers: Cascode Amplifier (Part A)

Dear, students welcome back to our NPTEL online certification course on Analog Electronic Circuits, myself Pradip Mandal from E and ECE department of IIT Kharagpur. And today's topic of discussion, it is Multi - Transistor Amplifiers in fact, this is continuation of our previous discussion.

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Flow of Discussion (Bottom-up) – Building blocks

- **System/ Sub-systems** (for specific application)
 - **Modules** (performing specific tasks)
 - **Building blocks** (having specific characteristics)
 - Components (devices/circuit elements)
- **Week 6:**
 - Multi transistor Amplifiers (operation and analysis):
 - CE-CC; CS-CD; CC-CC; Darlington pair etc.
 - ✓ **Cascode amplifiers**
 - CE-CB and CS-CG *CE - CB* *CS - CG*
 - Amplifier with active load.

Now the plan overall plan if you see according to our weekly plan so far we have covered CE – CC; CS - CD and CC; CC; Darlington pair etcetera both theory as well as numerical

examples. And we are going to discuss about Cascode Amplifiers which are essentially I should say CE this should be CE, CE followed by CB and CS followed by CG.

So, I should say this is combination of common emitter amplifier with common base. So, this is BJT version and this one is a MOS version common source followed by common gate.

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CONCEPTS COVERED

Concepts Covered:

- Continuing multi-configuration amplifiers:
 - CE-CB ✓
 - Cascode amplifier using BJTs ✓
 - CS-CG ✓
 - Cascode amplifier using MOSFETs ✓

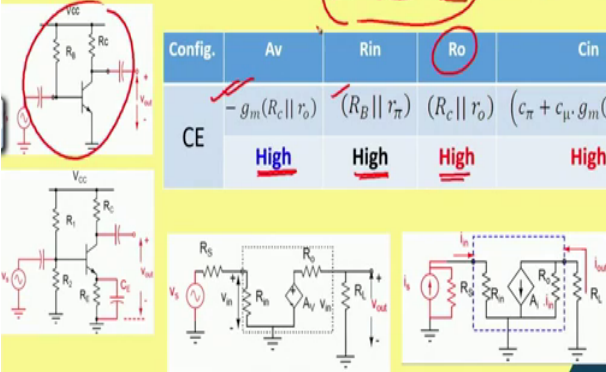
So, the concepts we will be covering in this lecture is the following. So, we shall start with CE followed by CB and in fact, with appropriate modification. It gives us a relatively simple circuit configuration which is commonly known as cascode amplifier so, that amplifier we will be discussing in depth. And then this is a course with using BJT. So, likewise we do have cascode amplifier using MOSFET transistor and, but prior to that since it is essentially coming from a common source followed by common gate.

So, we shall start with common source followed by common gate configuration and then we will simplify to conclude to cascode amplifier using MOSFET. I like to say that you might have observed that if we consider simply common emitter amplifier, its gain is typically quite high more than 100. On the other hand if I consider common source amplifier its gain is not so high. So, we must be having some alternative for particularly for MOSFET version otherwise that circuit may not be really much of an use. And this cascode amplifier is one of the configuration in a MOSFET amplifiers which is essentially helping to get the higher gain.

So, may not be the cascode amplifier may not be very popular in in the domain of BJTs amplifiers, but it is quite popular in the community of MOSFET. So, anyway both the circuits we will be discussing. So, let us see first the CE and CE followed by CB and then cascode using BJT.

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Performance metrics of ~~CE~~ ~~CB~~ configurations



Config.	A_v	R_{in}	R_o	C_{in}	A_I
CE	$-g_m(R_c r_o)$ High	$(R_B r_\pi)$ High	$(R_c r_o)$ High	$(c_\pi + c_\mu \cdot g_m(R_c r_o))$ High	β High

The slide includes three circuit diagrams: a common emitter (CE) amplifier, a common emitter followed by common base (CE-CB) amplifier, and a cascode amplifier. The CE circuit shows a BJT with base biasing resistors R_1 and R_2 , a collector resistor R_C , and an emitter resistor R_E . The CE-CB circuit shows a CE stage followed by a CB stage. The cascode circuit shows a CE stage with a CB stage in parallel. A table summarizes the performance metrics for the CE configuration, with handwritten red circles around the R_o column and the CE row. The table indicates that for the CE configuration, A_v is $-g_m(R_c || r_o)$ (High), R_{in} is $(R_B || r_\pi)$ (High), R_o is $(R_c || r_o)$ (High), C_{in} is $(c_\pi + c_\mu \cdot g_m(R_c || r_o))$ (High), and A_I is β (High).

So, to start with you may recall we made a summary that a different performance matrices of CE amplifier. So this is the basic CE amplifier configuration and then we also have a different performance matrices and their expressions and qualitatively we said that some of them are high, some of them are not so high or whatever it is and in fact, even though R_o it is high it is not good for voltage amplifier. So, those kind of discussion we already made. So, likewise we also have discussion related to a common base, common collector, this part we already have discussed so we will not be covering now.

So, we need to basically revisit this important property of CE and CB to motivate ourselves that combining CE and CB it is giving us a better performance. So, this is what the performance summary of CE amplifier, likewise we do have the performance summary of a common base amplifier.

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Performance metrics of CE / CC / CB configurations

Config.	A_v	R_{in}	R_o	C_{in}	A_i
CB	$g_m(R_1 \parallel r_o)$	$r_\pi \parallel \frac{(R_1 + r_o)}{(g_m r_o + 1)}$	$R_1 \parallel (r_o + g_m r_o (R_s \parallel r_\pi \parallel R_2))$	C_π	α
	"High" with $R_s = 0$	V. Low	V. High	V. Low	V. Low

So, this is the corresponding circuit configuration common base circuit configuration and you may recall that its voltage gain is quite good, but we assume that the signal source resistance is 0 and then its main property here is that its input resistance is low, as a result its input port is not really good for voltage feeding. So, we will see that, but then of course, this property is helping to make the port suitable for current signal feeding. On the other hand the output resistance of the amplifier is very high so, that also makes the circuit suitable for current mode signal at the output port.

So, then also its input capacitance is a low namely only the [vocalized- noise] the C_{pi} and the current gain on the other hand it is not good. In fact, it is theoretically it is less than 1 though it is very close to 1. So, now, if we put say performances of CE and CB together to construct a new configuration called CE CB, then let us see what kind of performance we do expect yeah.

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Multi-configuration amplifiers: CE-CB

Config.	A_v	R_{in}	R_o	C_{in}	A_I	Remarks
CE	High	High	High	High	High	Good Voltage amp & Current amp but needs suitable buffers (for cascading)
CC	V. Low ≈ 1	V. High	V. Low	V. Low	High	Voltage mode buffer and Power amplifier
CB	"High" with $R_s = 0$	V. Low	V. High	V. Low	V. Low ≈ 1	Current mode buffer and voltage gain booster

Handwritten notes: CC is circled in red. A note says 'V. Low ≈ 1 '. Another note says 'High' with $R_s = 0$. A third note says 'V. Low ≈ 1 '.

So, this is the [vocalized- noise] summary and as I said that at present we are interested to focus on CE and CB, this we may not be concentrating. And our main purpose here is of course, CB can be utilized for current buffer, but today we are going to discuss more like application to boost the voltage gain. Before I go into that I must say one important point I missed it whenever we have discussed about the CC amplifier we have seen that its voltage gain it is slow in fact, it is very close to 1.

And whenever in CC stage whenever we have given the input at the base and we are observing the output here and we have seen that the gain it is close to 1 and the phase also it is a phase shift is also 0 degree. So whatever the input signal you are giving at the base in fact, almost to the same signal it was coming to the emitter. So, that is why this CC it is having other name

which is also quite popular it is referred as emitter follower. So, which means that emitter node it is following the base node.

So, the CC stage whenever we are using as a voltage buffer it may be referred as emitter follower. So, likewise when you talk about say common base configuration and their the current gain it is approximately 1. So, whatever the input current we give so, we do have the CB stage here, whatever the input current we give here almost the same current we do get at the output.

So, this circuit CB circuit it is the other name of CB circuit it is something called current conveyor. So, it conveys this current from emitter node to collector node almost with the same magnitude but the basic purpose here it is that impedance at this port at the emitter port it is quite low whereas, impedance at the collector port it is high. So, this current conveyor basic purpose of the current conveyor, it is taking the or rather taking the receiving the current at the low impedance port and it is delivering the current at the high impedance port.

On the other hand the complimentary things are happening for voltage follower or I should not say voltage follower emitter follower, the input voltage it is getting conveyed from the base terminal to the emitter terminal. And so, here it is while it is conveying it is input port resistance it is high and then it is delivering the signal at the emitter where the output port resistance it is quite low. So, these two configurations [vocalized- noise] common collector and common base they do have their dual property and they are essentially used as voltage mode and current mode buffer respectively ok.

So, now coming back to whatever we are about to say the application of the common base to enhance the circuit gain. So, we will be seeing that how this this will be enhancing the gain.

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Multi-configuration amplifiers: CE-CB

Config.	A_v	R_{in}	R_o	C_{in}	A_i	Remarks
CE	High	High	High	High	High	Good Voltage amp & Current amp but needs suitable buffers (for cascading)
CC	V. Low	V. High	V. Low	V. Low	High	Voltage mode buffer and Power amplifier
CB	"High" with $R_s = 0$	V. Low	V. High	V. Low	V. Low	Current mode buffer and voltage gain booster

So, we do have the CE stage here and then we do have the CB stage as the name suggests that the output of the CE stage we like to feed it here and if we are feeding the voltage here and there may be a different possibilities, we may remove the capacitors or at least we can say that we can keep only one capacitor. So, if I am putting one capacitor here, then the corresponding configuration becomes like this.

So the output of the CE stage namely collector or Q 1 it is and getting connected to the emitter of Q 2 through a DC blocking capacitor. So, that the operating point of the second stage it is it should not get affected by this circuit so that is the purpose. Now we will see that in fact, the condition of the [vocalized- noise] of the DC operating point of CE and the CB stage is in this connection they are remaining isolated, but then of course, the signal it is going from the first stage to the to the second stage at its input.

Now we can modify this this connection without really putting this capacitor here, but then of course, we should be having a meaningful connection. And in the next slide, we will be discussing about how we can cleverly directly couple these CE and CB together and that gives us the new configuration called cascode configuration.

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Multi-configuration amplifiers: CE-CB and Cascode amplifier

CE - CB

So, I should say that cascode circuit, it is essentially CE-CB, but I should say it is simplified or modified version. So, here we do have the [vocalized- noise] CE-CB amplifier whereas, if you see here this Q 1 in fact, whatever the DC voltage you do have here that may be useful, I should not say DC voltage rather I should say the current. So, if you see the Q 1, it requires it is collector current and that current it is getting supplied by this R 2 and on the other hand the emitter current, DC current of Q 2 need to be consumed by this circuit.

So, we can say that basic purpose of having this R_2 and this I whatever the I bias here maybe along with this R_4 , it is essentially to bias Q_1 and Q_2 respectively. Q_1 it demand some current to become entering to it is collector and Q_2 it is expecting it is emitter current need to be consumed by somebody else.

So, what you are doing here it is, if we remove say this part and if you remove this part and then if you remove the DC blocking capacitor also. Then what you can say that the emitter current of Q_2 can enter into Q_1 and; that means, support this bias requirement of Q_1 and that is what exactly it is happening here. So, the emitter current of Q_2 it is entering into Q_1 as its collector current. So if here at this node in fact, instead of blocking their DC current and [vocalized- noise] DC voltage we are directly rather utilizing the opportunity here. So, that we can get rid off the bias circuits here we can we can get rid of the capacitor, but then of course, you have to see whether everything is falling in place or not.

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Multi-configuration amplifiers: CE-CB and Cascode amplifier

The image shows two circuit diagrams of a cascode amplifier. The left diagram is a standard cascode configuration with two transistors, Q_1 and Q_2 , and resistors R_1 , R_2 , R_3 , and R_4 . The right diagram is a more detailed version with handwritten annotations in red, including labels for V_{dd} , V_{be} , g_m , and f_o .

So, what we said here it is DC current of Q_2 it is supplying require DC current of Q_1 , on the other hand we are feeding the signal at the base of Q_1 and we are expecting that this V in signal it will be producing V_{be} signal V_{be} that supposed to be producing a current here signal current and that is g_m into that V_{be} . So, along with the DC current here of course, we do have the signal and this this signal should be successfully reaching to the collector or transistor to which we call it is the primary output port.

So this current this current source of course, it is having it is own conductance called r_o and then this current supposed to be successfully entering into this circuit. So, we will be going through detailed analysis for that, but then just I like to say that instead of having this ideal bias here. Practically we do have a potential divider constructed by R_2 and R_4 from the main supply V_{dd} here, which generates a DC voltage. Now it is also having Thevenin equivalent

resistance which is R_2 and R_4 in parallel and we like to keep the base node of transistor 2 to AC ground and that is done by this capacitor.

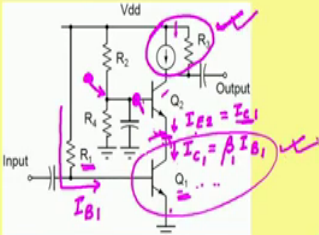
So, in summary we require the gate bias for Q 2, we require gate bias DC bias for Q 1, but then emitter bias of a transistor 2 and collector bias of transistor 1 they are eliminated by making them helping each other right. And of course, at the collector of Q 2 we do have the biasing arrangement I bias we do have maybe that bias circuit is having some finite conductance represented by R_3 there ok. So, that is how we got the cascode amplifier and as I said it is a special kind of amplifier and it is having higher gain and to appreciate or to really acknowledge that let we do the detail analysis of the cascode amplifier.

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Analysis of Cascode amplifier and comparison with CE amp.

✂️ **Biasing and operating point of BJTs**

- Small signal analysis
 - Voltage gain
 - Output impedance
 - Input impedance and
 - Input capacitance



Input

Output

Vdd

$I_{B1} = I_{E1}$

$I_{C1} = \beta I_{B1}$

$I_{E2} = I_{C1}$

Q1

Q2

R1

R2


R3

R4

R5

R6

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So, we do have the yeah. So, here we do have the cascode amplifier and let us see it is analysis, so, biasing and all we have discussed. So, let me yeah. So, we do have this biasing

and it is operating point of those BJTs it has been discussed. So, what we need to do here, it is the R_1 ; it is the value should be set such that the I_B of transistor 1 it is properly set here, which produces it is corresponding collector current I_{C1} which is beta times this I_B . And that is eventually gives us the emitter current I_E of transistor 2 which is I_{C1} .

Now this current of course, it should be consistent with whatever the current we do have. So, as long as we make sure that this current, it is consistent with I_{C1} then we do not have any problem. But, then if there is any mismatch then of course, the transistors maybe this transistor or this transistor they may be pushed into a saturated condition and that may create ill operation of the circuit. So, definitely while we are making this biasing, we need to be careful about that the current source here must be consistent with whatever the current we do have here which is set by this R_1 ok.

So, here we assume that this balancing of the current source and this current sink defined by Q_1 , they are consistent and hence rest of the things are it is I should say it is taken care. But of course, one minor thing that the base terminal here of Q_2 should be set at a voltage such that after deducting, it is V_{BE} namely around 0.6 whatever the voltage you do have that should not force Q_1 into saturation.

So I should say that it is collector current should be higher than $V_{CE\text{ sat}}$ and then plus 0.6. So, that is the required voltage here. So, the DC voltage here it should be at least 0.6 plus $V_{CE\text{ sat}}$ maybe whatever 0.3. So, now, this voltage if it is higher than the minimum required voltage, then we do not have any problem, this both the transistor particularly Q_1 it will be in active region of operation. So, maintaining this voltage on the other hand to ensure the consistency of the operation of the circuit is not so difficult. So, I think typically that is not the main concern; the main concern is that as I said that matching this current with this current is the main concern ok.

Now, coming to the small signal analysis so, now, let us see the small signal analysis and in in the small signal analysis we do have voltage gain and then output impedance, input impedance, input capacitances, those things we can compare with what are the corresponding performance

matrices coming out of simple CE amplifier. So, in the next slide we will be doing the analysis with a small signal equivalent circuit of the cascode amplifier.

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Analysis of Cascode amplifier and comparison with CE amp.

- Biasing and operating point of BJTs
- Small signal analysis
 - Voltage gain
 - Output impedance
 - Input impedance and
 - Input capacitance

Small Signal equiv. Ckt

So, I think you yourself can try out, but then I have done it for myself. So, here we do have the small signal equivalent circuit. So we do have the model small signal equivalent circuit for Q 1 and then we do have small signal model for Q 2. And the base node of Q 2 it is connected to a ground through this capacitor so, we are saying that this is AC ground. Then R 3 here it is connected to DC supply so that is also connected to ground and at the input you are feeding the signal maybe the signal source maybe having source resistance. So, we are feeding the signal here is V_{in} and the source is having source resistance of R_S . So, this is the corresponding model for that.

Now so, we can then of course, this is the primary output so, we will be observing the output here. So, to get the gain from this primary input to this output we need to analyze this circuit. So, either we can analyze this entire circuit or probably we can go little intuitive way to simplify the analysis.

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Analysis of Cascode amplifier and comparison with CE amp.

- Biasing and operating point of BJTs
- Small signal analysis
 - Voltage gain
 - Output impedance
 - Input impedance and
 - Input capacitance

So, let us see, what is the simplification we do have for the time being; let me assume that this R_s equals to it is very small. So, V_{in} it is directly coming here and that makes this V_{be} equals to V_{in} . So, the voltage dependent current source we do have g_{m1} into V_{in} here. So, this is g_{m1} into V_{in} so; that means, it is expecting that signal current it will be coming through this. In fact, this current partially it will be coming from upper side as well as it may be coming from this r_{o1} . So, when I say upper side it is primarily it is coming from $r_{\pi 2}$ as well as the combination of whatever the circuit we do have.

So either you can say that the current here it is signal current is flowing in this direction or you may say that the signal produced by this circuit it is getting injected here and then part of this is going here part of this is going here and the rest of the things it is going here and here. Now depending on the impedance offered by each of these paths, say this path, this path and this path this current it will be getting segregated.

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Analysis of Cascode amplifier and comparison with CE amp.

- Biasing and operating point of BJTs
- Small signal analysis
 - Voltage gain
 - Output impedance
 - Input impedance and
 - Input capacitance

$$R_3 \sim r_{o2}$$

$$V_o = -g_{m1} V_{in} R_3$$

$$R_{in,cb} = \frac{2r_{o2}}{g_{m2}r_{o2}} = \frac{2}{g_{m2}} \ll r_{\pi 2}$$

$$R_3 \sim r_{\pi 2} g_{m2} r_{o2}$$

$$R_{in,cb} = \frac{r_{\pi 2} g_{m2} r_{o2}}{g_{m2} r_{o2}} = r_{\pi 2}$$

$$V_o = -R_3 g_{m1} \frac{V_{in}}{2} = \frac{(r_{\pi 2} g_{m2} g_{m1} r_{o2} V_{in})}{2}$$

So, if you see the impedance. Now, if you look at the impedance of the main amplifier if you see this part. So, what is the impedance, impedance of this part it is R_3 plus r_{o2} divided by $g_{m2} r_{o2} + 1$, on the other hand this is straight forward this is $r_{\pi 2}$. So, if I say that this is the signal current it is entering and this is the resistance which is quite high compared to $r_{\pi 2}$ and maybe compared to this. So, we may ignore this path. So, we can say that $g_{m1} V_{be1}$ is essentially coming from these 2 paths.

So, then depending on this value of this resistance of course, there will be bifurcation. So, if I consider say R_3 in the order of say r_{o2} so, if I consider it is value it is in this order then this resistance; if I call R in of the common base. So with this R in CB it is say r_{o2} and in the denominator we may ignore this 1 and we can written only this part so, which is $g_{m2} r_{o2}$. So, this is becoming 1 2 by g_{m2} and we know that this is much smaller than $r_{\pi 2}$. So, as long as this R_3 it is maybe in this order. So, we can say that major part of the signal it is entering into this device and then it is whatever the things it will do we will see that part.

So, on the other hand if I say that R_3 it is in the order of $r_{\pi 2}$ and then let me call this is $r_{\pi 2}$ and then $g_{m2} r_{o2}$. So if I consider that R_3 it is in this order then corresponding R in of the common base circuit it is so, compared to r_{o2} this will be dominating because we do have this multiplication factor which is $r_{\pi 2}$ multiplied by g_{m2} that is nothing, but beta of the transistor so; obviously, that will be dominating. So, we can say that this is $r_{\pi 2} g_{m2} r_{o2}$ divided by $g_{m2} r_{o2}$ and that becomes $r_{\pi 2}$.

So, if R_3 it is in this order which is much higher than the previous case then we may say that half of the current it is flowing here and remaining half of the current it is entering there. But even then even then you may say that major part of the signal it is coming here and once or at least half of the signal it is coming there and once that current is flowing through this resistance it develops the corresponding voltage here. So, for the two cases if I consider say this case, then we can say that almost entire current is flowing here and the corresponding voltage getting developed here.

So, this gives us the output voltage which is R_3 multiplied by the signal current which is g_{m1} times V_{be1} which is V_{in} . So, we can say that of course, there will be a polarity difference. So, that gives us the voltage gain V_o divided by V_{in} equals to minus g_{m1} into R_3 . On the other hand so, you can say that if R_3 it is in the order of r_{o2} so, definitely this gain, it will be quite high depending on the value of this R_3 and the corresponding g_{m1} .

On the other hand if I consider the R_3 it is in this order and then only half of the current it is entering to this circuit and in this case the corresponding V_o it will be the minus R_3 into g_{m1} .

V_{in} by 2, why by 2 that is because half of the current it is entering into this $r_{\pi 2}$ which is wastage for us, but then the corresponding R_3 it is quite high. So, which is $r_{\pi 2} g_{m 2}$, then we do have $g_{m 1} r_{o 2}$ divided by 2 into V_{in} . So, that gives this V_o divided by V_{in} it is quite high.

In fact, if you see here this part it is beta so, we can say that the corresponding gain V_o divided by V_{in} and if I particularly keep the focus on gain magnitude, then this is beta of transistor 2 by 2 g_m into r_{naught} , which means that if I consider simple CE amplifier where the gain may be in this order where [vocalized- noise] this R_3 maybe in the order of r_o whereas, for this case the gain, it is higher than the CE amplifiers gain by a factor of beta 2. But then that can be obtained by considering a situation where R_3 it is much higher than a standard $r_o 2$.

So, we may require additional circuit we may require really a clever circuit here which offers high value of this R_3 . Assuming that it is possible to get that then we will be getting very good gain out of good voltage gain out of this one. So, that is the basis of this claim that the cascode amplifier, it provides higher gain much higher gain than the CE amplifier.

Now let us look into the output impedance.

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Analysis of Cascode amplifier and comparison with CE amp.

- Biasing and operating point of BJTs
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$R_o = R_3 \parallel ?$

$R_{eq} = r_{\pi 2} \parallel r_{o 1} + r_{o 2} + g_{m 2} r_{o 2} (r_{\pi 2} \parallel r_{o 1}) \approx g_{m 2} r_{o 2} (r_{\pi 2} \parallel r_{o 1})$

So, this is the output port and R_o which is R_3 coming in parallel with whatever the resistance coming out of this entire circuit. So, if I want to know what will be the resistance of this circuit the circle circuit what it can say that this $r_{\pi 2}$ and $r_{o 1}$, they are coming in parallel this one of course, I have to make the signal is equal to 0. So, that makes this is equal to 0. So, this part it is 0. So, we can ignore that part. So, to know this resistance what we can do? We can draw the rest of the circuit to get the equivalent resistance.

So, we do have $r_{o 2}$ and then we do have $g_{m 2} V_{be 2}$ and at this node at this node we do have $r_{\pi 2}$ connected to ground and also we do have $r_{o 1}$ connected to ground. So, we can say these two resistances they are coming in parallel and such kind of circuit, we have seen before the equivalent resistance of this circuit you may recall that $R_{equivalent}$ is equal to $r_{\pi 2}$ in parallel with $r_{o 1}$ plus $r_{o 2}$ plus $g_{m 2} r_{o 2}$ into $r_{\pi 2}$ in parallel with $r_{o 1}$.

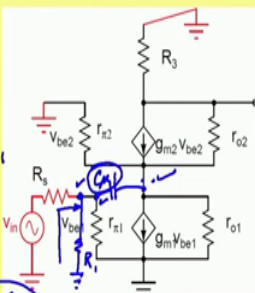
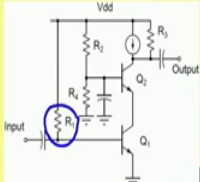
In fact if you see here compared to this part and this part; this is quite high. So, we can approximate that this is g_{m2} multiplied by r_{o2} multiplied by $r_{\pi 2}$ in parallel with r_{o1} , which means that the output resistance coming here it is quite big and its expression is given here. In fact, if you see these two transistors while these two transistors are connected in series and if the gate of the first transistor, it is connected to AC ground then it is not only it is r_{o1} and this r_{o1} coming in series in fact, we do have some nice amplification here ok.

So, this kind of tricks can be utilized to make the impedance here much higher than normal r_{o1} which is referred as cascode current source, later we will be talking about that in detail. So, while you are talking about cascode amplifier, this cascode terms [vocalized- noise] it may be coming while we will be you know designing this part to achieve high value of this impedance R_3 . So, anyway so, that is the output impedance we do have R_3 in parallel with this and then coming to the input impedance. Let me clear the board yeah.

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Analysis of Cascode amplifier and comparison with CE amp.

- Biasing and operating point of BJTs
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$R_{in} = r_{\pi 1} \parallel R_1 \approx r_{\pi 1}$
 $C_{in} = C_{\pi 1} + C_{\mu 1} (1 + A_{v1})$
 $\ll C_{in-CE} \ll \frac{g_{m1} r_{o1}}{\omega}$
 $\Rightarrow C_{\pi 1} + C_{\mu 1} (1 + A_{v-CE})$

So, the input impedance on the other hand so, if you see this is the input port input impedance is very straight forward. So, R_{in} in it is same as $r_{\pi 1}$, but then input capacitance. So, this is very important thing. So, input impedance wise if you see hardly there is no difference compared to input impedance of normal CE amplifier. In fact, we also need to consider R_1 in parallel with that, but. So, this R_1 in this model I have not drawn you can draw that also. So, typically this R_1 it is much higher than $r_{\pi 1}$.

So, you may consider this is approximately equal to $r_{\pi 1}$ which is same as the input resistance of normal CE amplifier. So, I should say there is no change in input impedance; however, in input capacitance if you see the C_{μ} this C_{μ} it is which is integral part of Q_1 which is breezing the base and collector terminals of Q_1 .

Now from this node to this node we claim that the gain of the circuit is not very high. So as a result the miller factor coming for this $C_{\mu 1}$ it may not be very high. So, of course, you will be getting $C_{\pi 1}$ and then $C_{\mu 1}$ multiplied by $1 + A_{V 1}$ gain and we claim that this $A_{V 1}$ gain, it is much lower than $g_{m 1} r_{o 1}$. So, if we agree with this that this is much lower than $g_{m 1}$ multiplied by $r_{o 1}$.

So, we can say that this capacitance is much smaller than C_{in} or a standard CE amplifier, where for standard CE amplifier the corresponding input capacitance is $C_{\pi 1}$ plus $C_{\mu 1}$ multiplied by $1 +$ the corresponding voltage gain of CE amplifier. Now to really acknowledge the improvement of this input capacitance namely reduction of the input capacitance, we need to establish that this gain the circuit gain here from this point to this point it is much lower than the [vocalized- noise] voltage gain of CE amplifier.

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Analysis of Cascode amplifier and comparison with CE amp.

- Biasing and operating point of BJTs
- Small signal analysis
 - Voltage gain
 - Output impedance
 - Input impedance and
 - Input capacitance

$$C_{in} = C_{\pi 1} + C_{\mu 1}(1 + |A_{V 1}|)$$

$$= C_{\pi 1} + 2C_{\mu 1}$$

$$A_{V 1} = -g_{m 1} \times (r_{o 1} \parallel \frac{1}{g_{m 2}})$$

$$\approx -\frac{g_{m 1}}{g_{m 2}}$$

$$\approx -1$$

So let us see how we establish that. So, if you see this circuit if you see this circuit and if you want to know what will be the gain from here to here, we need to know what is the corresponding impedance we do have here and we have seen that based on the value of this R_3 this impedance maybe in the order of you know $1/gm_2$.

So, the voltage gain from here to here it is I should say A_{V1} if I call it is A_{V1} minus gm_1 multiplied by r_{o1} coming in parallel with whatever the impedance. We are seeing here and that may be in the order of $1/gm_2$ ok. So, this is approximately gm_1 divided by gm_2 and since the current here and current here they are same, we can say that gm_1 and gm_2 they are same. So, further we can say that this is approximately minus 1. So, that makes the input capacitance of this circuit it is C_{pi} plus C_{mu1} into $1 + 1$ or to be more precise $C_{pi} (1 + 2)$ times or C_{mu1} .

Here of course, we have assumed that this [vocalized- noise] input impedance the input impedance of the cascode transistor this is referred as the cascode transistor so, it is in the order of $1/gm_2$, but we know that it depends on [vocalized- noise] it highly depends on the value of R_3 . So, if this R_3 on the other hand if it is very high that may increase the increase this resistance and the consequence here of course, then the voltage gain here it will increase. So, here to here the voltage gain if it is increasing, then this factor instead of one that will also increase.

So, but then typically this gain from this point to this point it is, it is quite fair to approximate that that is gain it will be around 1 or 2 depending on this corresponding load practical load here. Let me take a short break and I will come back after the break for the MOS circuit.