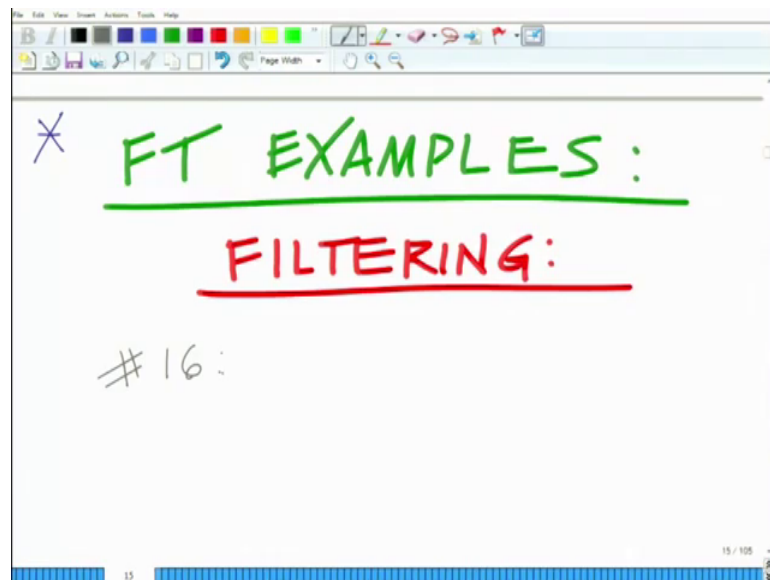


**Principles of Signals and Systems**  
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**Lecture - 50**  
**Fourier Transform Examples: Filtering – Ideal Low Pass Filter**

Hello welcome to another module in this massive open online course. So, we are looking at example problems in the Fourier transforms alright. So, let us continue our discussion and the completed discussion on the Hilbert transform let us start looking at another interesting problem that is to understand the process of filtering ok.

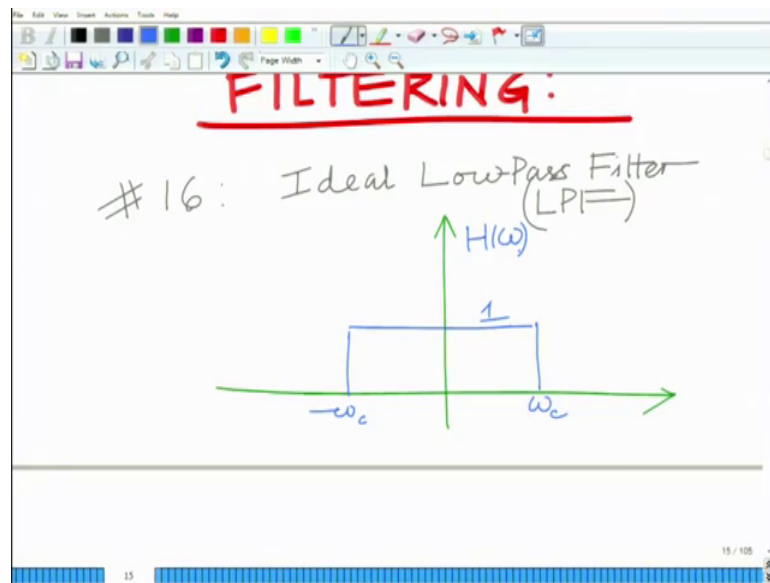
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So, looking at examples or a practical examples for the Fourier transform and in this particular module let us understand the process of filtering.

You will recall that we have discussed ideal filters high pass, low pass, band pass and band stop. So, we were going to look at an application on the theory of filtering ok. So, now, as you might already remember or recalls let us term this as process this is problem number 16.

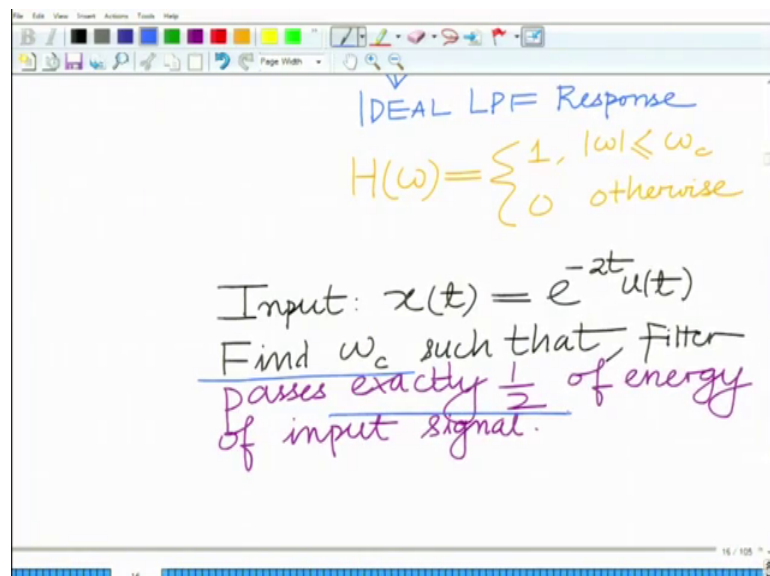
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So, we have an ideal low pass filter. So, consider an ideal low pass filter and in this ideal low pass filter if you might remember the ideal low pass filter the response looks something like this.

So, I have a cut off frequency  $\omega_c$  and the response magnitude of  $H(\omega)$  equals 1 or we can also call it  $H(\omega)$  this was just magnitude. So,  $H(\omega)$  equals 1 for  $\omega$  magnitude  $\omega < \omega_c$  and  $H(\omega)$  equal to 0 otherwise this is an ideal low pass filter ok.

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So, this is your ideal LPF response and this can be characterized as  $H$  of the response of the LTI system  $H$  of  $\omega$  equals 1 for magnitude of  $\omega$  less than or equal to  $\omega_c$  and this is 0 otherwise or magnitude of  $\omega$  greater than  $\omega_c$  this is 0 ok.

Now, what we want to do is for this LPF we want to consider an input signal. So, our input signal to the LPF input equals the input signal equals  $x$  of  $t$  given as the input is  $x$  of  $t$  equals  $e^{-2t} u(t)$  this is our input signal. Now what we want to do is we want to design a filter. So, this problem is with respect to filter design. So, we want to design a filter which means we want to design or choose a cutoff frequency  $\omega_c$  such that it passes a certain fraction or a certain desired component of the signal.

Now, what is the desired component of the signal? So, what we want to do is we want to find  $\omega_c$  of the low pass filters such that find  $\omega_c$  such that the filter passes exactly half of energy of the of the given input signal ok. So, the point is we want to find  $\omega_c$  such that the LPF that is your ideal LPS passes exactly half or allows exactly there is a energy of the output signal should be half of the energy of the input signal that is  $e^{-2t} u(t)$  ok. So, this is our design problem filter design problem and we can approach this problem as follows.

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The image shows a whiteboard with handwritten mathematical equations. The equations are:

$$x(t) = e^{-2t} u(t)$$

$$\Rightarrow X(\omega) = \frac{1}{j\omega + 2}$$

$$Y(\omega) = X(\omega) \cdot H(\omega)$$

$$= \begin{cases} \frac{1}{j\omega + 2}, & |\omega| \leq \omega_c \\ 0, & \text{otherwise} \end{cases}$$

The whiteboard also shows a toolbar at the top and a page number '17 / 105' at the bottom right.

Now, first let us use the Fourier transform approach. So, first note that we are given this signal  $x$  of  $t$  equals  $e^{-2t} u(t)$  which implies now taking the Fourier transform no  $X$  of  $\omega$  of this signal is  $1$  over  $j\omega$  plus  $2$ . Now, therefore, we

know from the theory of the Fourier transform that the output Fourier transform by  $\omega$  is Fourier transform the input signal  $X(\omega)$  times Fourier transform of the filter response that is  $H(\omega)$ . So,  $Y(\omega)$  is  $X(\omega)$  times  $H(\omega)$  which is now remember  $H(\omega)$  is 1 only for magnitude of  $\omega$  less than  $\omega_c$ .

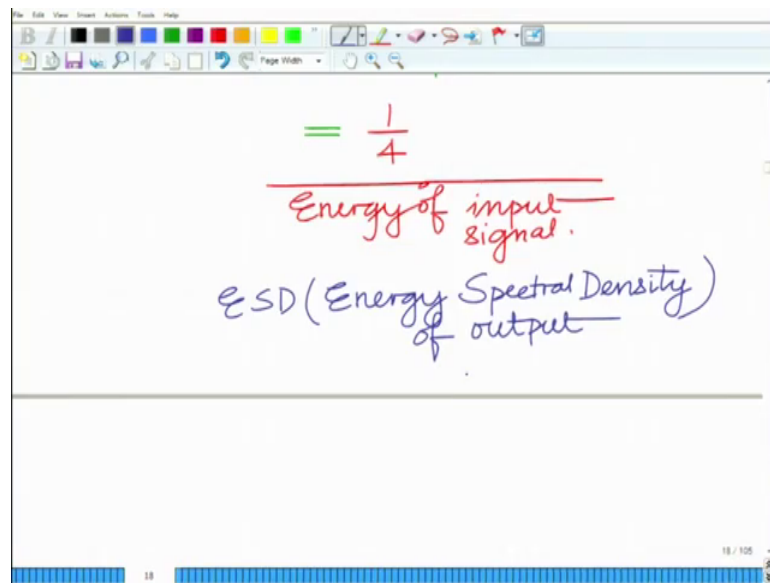
So, it allows only the signal component or the frequency components of the signal in this minus  $\omega_c$  to  $\omega_c$  because the pass through and it suppresses because its response is 0 outside of this band. So, it suppresses all the frequency components which are outside this band. So, what we have is this is basically  $1$  over  $j\omega$  over  $2$  form or  $\omega$  less than or equal to  $\omega_c$  and this is 0 this is 0.

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$$\begin{aligned} \text{Energy of signal} &= \int_{-\infty}^{\infty} |x(t)|^2 dt \\ &= \int_0^{\infty} e^{-4t} dt \\ &= -\frac{1}{4} e^{-4t} \Big|_0^{\infty} \end{aligned}$$

Otherwise now, the energy of the signal this is equal to now first let us find the energy of the input signal that is minus infinity to infinity magnitude  $x(t)$  square  $dt$  which is minus infinity to infinity  $e^{-4t}$   $dt$  which is minus one by 4  $e^{-4t}$  between the limits 0 to infinity which evaluates to basically 1 over 4 this is the energy of this is the energy of the input signal.

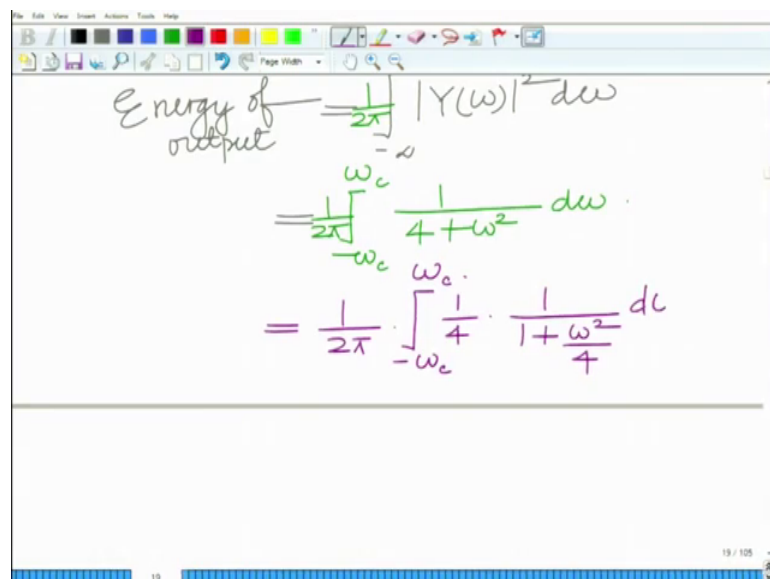
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The slide shows a handwritten equation  $= \frac{1}{4}$  in red. Below it, the text "Energy of input signal." is written in red. Underneath that, "ESD (Energy Spectral Density) of output" is written in blue. The slide is part of a presentation with a toolbar at the top and a footer showing "18 / 105".

Now, we want to lose the concept of what is known as the energy spectral density remember energy spectral density gives us the distribution of energy of the input signal over the frequency spectrum. So, this is a very good example to illustrate the illustrate a practical application of this concept of energy spectral density ok. So, now, what we want to do is we want to consider the ESD over the energy spectral density of output.

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The slide shows a handwritten derivation for the energy of output. It starts with "Energy of output" on the left. The first equation is  $= \frac{1}{2\pi} \int_{-\infty}^{\infty} |Y(\omega)|^2 d\omega$ . The second equation is  $= \frac{1}{2\pi} \int_{-\omega_c}^{\omega_c} \frac{1}{4 + \omega^2} d\omega$ . The third equation is  $= \frac{1}{2\pi} \int_{-\omega_c}^{\omega_c} \frac{1}{4} \cdot \frac{1}{1 + \frac{\omega^2}{4}} d\omega$ . The slide is part of a presentation with a toolbar at the top and a footer showing "19 / 105".

Now, remember the energy spectral density of the output that is magnitude Y of omega square remember we have seen what is Y of omega; we get Y of omega from this

expression. So, magnitude  $|Y(\omega)|^2$  is basically  $\frac{1}{4 + \omega^2}$  for magnitude  $\omega$  less than or equal to  $\omega_c$  and 0 otherwise. So, this is the energy spectral density of the output signal. So, this is your this is the ESD the energy spectral density of the output signal, this is  $\frac{1}{4 + \omega^2}$  correct for  $\omega$  the frequencies that lie in the band  $-\omega_c$  to  $\omega_c$  ok.

And therefore, the energy of this output signal is nothing, but the integral of the energy spectral density over the entire frequency band that is from minus infinity to infinity, but. So, to be nonzero from minus  $\omega_c$  to  $\omega_c$  therefore, it is the integral of the energy spectral density from minus  $\omega_c$  to  $\omega_c$ . So, therefore, energy of output now we have a very interesting application of the energy spectral density infinity to infinity magnitude  $|Y(\omega)|^2$  of  $\omega$  which is minus  $\omega_c$  to  $\omega_c$ .

. In fact, this is  $\frac{1}{2\pi}$  I have to have a factor of  $\frac{1}{2\pi}$  this is a constant factor scaling factor  $\frac{1}{2\pi}$  times  $\frac{1}{4 + \omega^2}$   $d\omega$  which is minus  $\omega_c$  to  $\omega_c$   $\frac{1}{4 + \omega^2}$  now I am going to simplify this integral  $\frac{1}{4 + \omega^2}$  by  $4$   $d\omega$ .

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The image shows a whiteboard with handwritten mathematical steps. At the top, there is a toolbar with various drawing tools. The main content consists of three lines of equations:

$$= \frac{1}{2\pi} \cdot \frac{1}{4} \cdot \tan^{-1} \frac{\omega}{2} \Big|_{-\omega_c}^{\omega_c} \cdot 2$$

$$= \frac{1}{4\pi} \times 2 \tan^{-1} \frac{\omega_c}{2}$$

The final result is enclosed in a green box:

$$E_y \text{ Energy output} = \frac{1}{2\pi} \tan^{-1} \frac{\omega_c}{2}$$

At the bottom right of the whiteboard, there is a small text "20 / 108".

Now, if you look at this is nothing, but one over  $2\pi$  into  $\frac{1}{4}$  into  $\tan^{-1} \frac{\omega_c}{2}$  evaluated between the limits minus  $\omega_c$  to  $\omega_c$  times 2. So, this is basically you have  $\frac{1}{4\pi}$   $\tan^{-1} \frac{\omega_c}{2}$  or  $\frac{1}{4\pi}$  into twice  $\tan^{-1} \frac{\omega_c}{2}$ .

$\omega_c$  by 2 which is equal to now you can see this is  $\frac{1}{2\pi} \tan^{-1} \omega_c$  by 2. So, this is the energy output.

You can also call this as  $E_Y$  this is the energy of the this is the energy of the output signal this is  $\frac{1}{2\pi} \tan^{-1} \omega_c$  over 2 this is a function of this is naturally going to be a function of the cutoff frequency  $\omega_c$  of the ideal low pass filter ok. And now all we have to do is basically equate this to half of the input. So, we know that we want to design the filter with a cut off frequency  $\omega_c$  such that the output energy is basically half of the input energy and the input energy is  $\frac{1}{4}$ . So, half of the input energy is  $\frac{1}{8}$ .

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The image shows a whiteboard with handwritten mathematical equations. The equations are as follows:

$$E_Y = \frac{1}{2} \cdot E_X$$

$$\Rightarrow \frac{1}{2\pi} \cdot \tan^{-1} \frac{\omega_c}{2} = \frac{1}{2} \cdot \frac{1}{4}$$


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$$\Rightarrow \tan^{-1} \frac{\omega_c}{2} = \frac{\pi}{4}$$

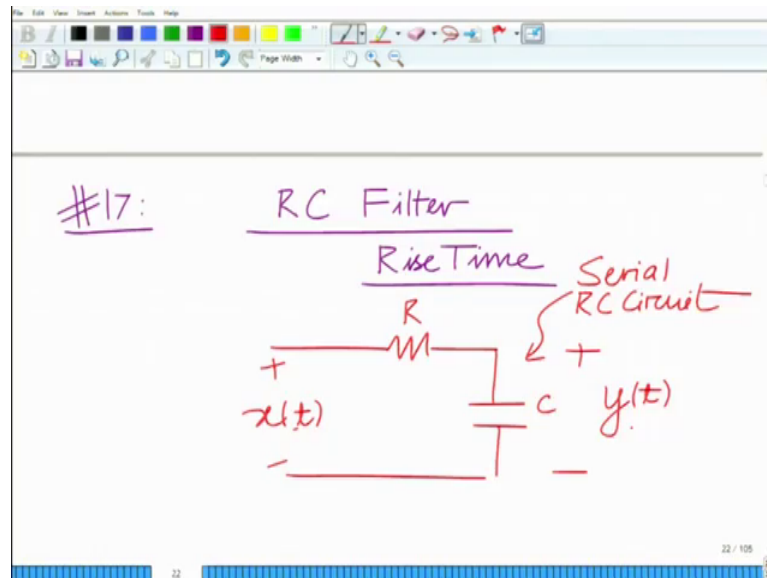
$$\Rightarrow \frac{\omega_c}{2} = 1$$

$$\Rightarrow \boxed{\omega_c = 2 \text{ Rad/s.}}$$

So, basically what we have is  $E_Y$  equals half of  $E_X$  which is input energy which means  $\frac{1}{2\pi} \tan^{-1} \omega_c$  over 2, this is equal to half into  $\frac{1}{4}$  which implies basically  $\tan^{-1} \omega_c$  by 2 equals  $\frac{\pi}{4}$  which means  $\omega_c$  by 2 equals  $\tan$  of  $\frac{\pi}{4}$  which is 1 which means  $\omega_c$  equals 2 radians. So, that is 2 radians per second  $\omega_c$  equals to radians per second.

So, that is basically. So, basically this gives us a filter. So, this gives us a filter such that input energy alright since the energy of the output signal corresponding to the input signal  $e^{-2t}$  there is exponential signal the output energy is basically half the energy of the inputs ok. So, the cutoff frequency  $\omega_c$  is basically 2 radians per second alright.

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So, let us proceed to the next problem that is problem number 17 and this is with respect to an RC filter and this blocks talks about the rise time of an RC filter. And this deals with the concept of the rise time of an RC filter and the problem is as follows. So, let us say we have a serial RC circuit; we have a serial RC circuit, the output across the capacitor the input is the signal  $x(t)$  and the output across the capacitor the output voltage across the capacitor is  $y(t)$ .

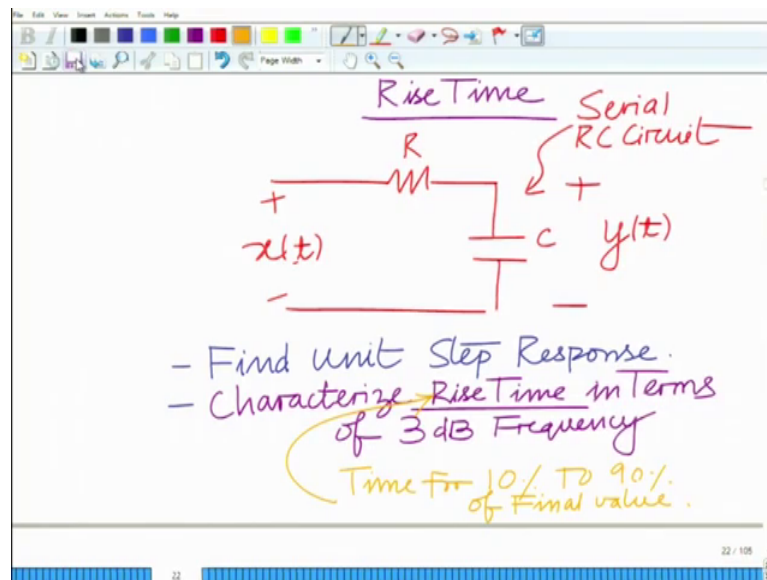
So, this is your serial RC circuit and now the problem is to find the unit step response and explicitly find the rise time that is the time that takes from the step response to go from 10 percent to 90 percent of its final value characterize the rise time. So, for a unit step response we have an output for this RC circuit ok.

Now what we want to do is we want to characterize the rise time what is the relationship of the rise to specifically what is the relationship of the rise time of this RC circuit there is a time it takes to rise from 10 percent to 90 percent of the final value alright in terms of the 3 dB frequency of this RC circuit ok. So, that is what you want to know.

So, we want to characterize the unit step response. So, want to find the unit step response that is the first step.



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And then we want to characterize the rise time in terms of 3 dB; now rise time is basically time taken to go from 10 percent to 90 percent. So, time taken to go from 200 to from the  $k$  by time taken for the capacitor output to go from 10 percent to 90 percent of its final value that is termed as a rise type of this serial RC circuit ok.

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The diagram shows the differential equation for the input/output relation of an RC circuit:

$$x(t) = y(t) + RC \frac{dy(t)}{dt}$$

This is labeled as the "DE for input/output Relation of RC circuit". Below it, the Fourier Transform (FT) is applied:

$$\Rightarrow X(\omega) = Y(\omega) + RC j\omega Y(\omega)$$

The diagram also shows a red arrow pointing from the differential equation to the Fourier Transform equation, and another red arrow pointing to the right.

So, now let us approach this problem now we have seen this several times before that is the input voltage  $x(t)$  is the voltage across the resistance is a voltage across the capacitor plus the voltage across the resistance which is  $I$  times  $R$   $R$  times  $I$ , but  $I$  is  $C \frac{dv}{dt}$

where  $v$  is the voltage across the capacitor. So, this is  $C \, dy$  by  $dt$  this is the differential equation that this is basically differential equation for input slash output relation of RC circuit ok.

And therefore, this implies that  $X$  of  $\omega$  now taking the Fourier transform once you take the Fourier transform we have  $X$  of  $\omega$  equals  $Y$  of  $\omega$  plus  $RC \, dy \, t$  by  $dt$  as  $\omega$  a Fourier transform  $j \, \omega$   $y \, \omega$  because if the Fourier transform of  $y \, t$  is  $Y \, \omega$  the Fourier transform which the derivative is  $j \, \omega$  times  $y \, \omega$ . Now we have a simple equation in terms of the Fourier transform which we can solve to obtain the transfer function.

So, this implies that basically what we have is  $Y \, \omega$  divided by  $j \, \omega$ .

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DE for input/output Relation of RC circuit  
 FT  
 $\Rightarrow X(\omega) = Y(\omega) + RC j\omega Y(\omega)$   
 $\Rightarrow \frac{Y(\omega)}{X(\omega)} = \frac{1}{1 + j\omega RC}$   
 Unit Step Response:  $= H(\omega) = \text{Transfer Function}$

Or  $Y \, \omega$  divided by  $X \, \omega$  this is basically  $1$  over  $1 + j \, \omega$   $RC$  this is  $1$  over  $1 + j \, \omega$   $RC$ . Now the unit step response can be found as follows now remember this is equal to  $H$  of  $\omega$  this is the transfer function this is the transfer function and now unit step response.

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DE for input/output  
Relation of RC circuit

FT

$$\Rightarrow X(\omega) = Y(\omega) + RC j\omega Y(\omega)$$
$$\Rightarrow \frac{Y(\omega)}{X(\omega)} = \frac{1}{1 + j\omega RC}$$

Unit Step Response:  $= H(\omega) = \text{Transfer Function}$

Now, consider the unit step function  $u(t)$  which is equal to 1  $t \geq 0$  and 0 otherwise this is your unit step function or this is a unit step signal. And if you take the Fourier transform of this  $U(\omega)$  we already know this is  $\pi \delta(\omega) + \frac{1}{j\omega}$  over  $j\omega$  there is a unit step response ok.

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$$U(t) = \begin{cases} 1 & t \geq 0 \\ 0 & \text{otherwise} \end{cases}$$
$$\downarrow$$
$$U(\omega) = \pi \delta(\omega) + \frac{1}{j\omega}$$
$$Y(\omega) = U(\omega) H(\omega)$$
$$= \left( \pi \delta(\omega) + \frac{1}{j\omega} \right) \cdot \frac{1}{1 + j\omega RC}$$

And therefore, we have  $Y(\omega)$  the output corresponding to unit the unit step response is basically the Fourier transform the unit step response there is  $U(\omega)$  times the transfer function  $H(\omega)$  that gives us the unit step response that is the output of this



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$$= \pi \delta(\omega) + \frac{1}{j\omega} - \frac{RC}{1+j\omega RC}$$

$$= \pi \delta(\omega) + \frac{1}{j\omega} - \frac{1}{j\omega + \frac{1}{RC}}$$

$$\begin{matrix} \text{IFT} \\ y(t) = u(t) - e^{-t/RC} u(t) \end{matrix}$$

$$y(t) = (1 - e^{-t/RC}) u(t)$$

Plus  $j\omega$  plus  $RC$  which is basically  $\pi$  of delta  $\omega$  plus  $1$  over  $j\omega$  minus  $1$  over  $1 + j\omega RC$ . Now I will bring the  $RC$  in the numerator to the denominator that will give me  $1$  plus  $j\omega$  divided by  $RC$  ok.

Now, I can now also write this quantity as  $1$  over  $1 + j\omega$  divided by  $\omega$  naught I am going to explain this in a little bit. So,  $\omega$  naught equals  $1$  over  $R$   $1$  over  $j\omega$  over  $j\omega$  over this is  $j\omega RC$   $j\omega$   $j\omega RC$  sorry this seems to be some mistake this is  $j\omega RC$ ,  $RC$  over  $RC$  over  $1 + j\omega RC$   $1 + RC$  over  $1 + j\omega RC$   $1$  over  $j\omega$  plus  $1$  over  $RC$   $j\omega$  plus  $1$  over  $RC$   $j\omega$  plus  $1$  over ok.

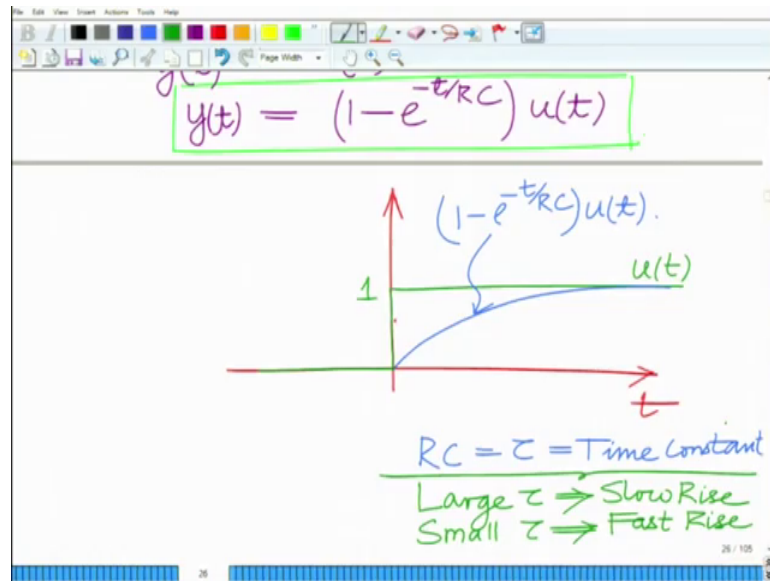
Let me just keep this as it is for a moment. So, this is  $1$  over  $j\omega$  plus  $1$  over  $RC$  now what this is now if you look at this now if you take the inverse Fourier transform; now look at this is nothing, but your signal the unit step  $u(t)$  this is  $\pi$  delta  $\omega$  plus  $1$  over  $j\omega$   $u(t)$ . Now this is  $1$  over this is of the form  $1$  over  $1 + j\omega$  plus  $a$ . So, the inverse Fourier transform of this is  $e^{-at} u(t)$  where  $a$  is this constant  $1$  over  $RC$  ok.

So, the inverse Fourier transform of this is  $e^{-t/RC} u(t)$  and therefore, the net taking the inverse Fourier transform. So, that you take the inverse Fourier transform and what you have is the output  $y(t)$  equals  $u(t)$  minus  $e^{-t/RC} u(t)$

over RC u t which is 1 minus e raised to minus t over RC ut e raised to minus t over RC ut ok. So, this is what we have.

And if you plot it it is going to look something like this with something you must have seen before.

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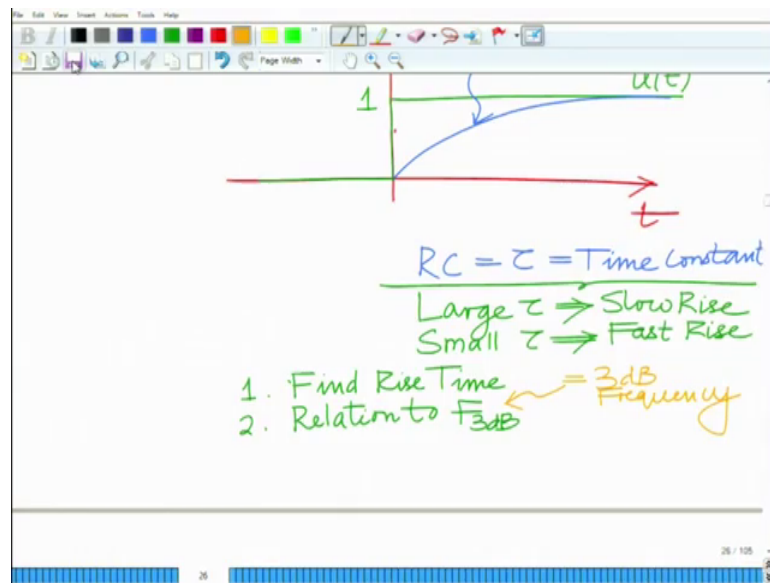
So, I have the time axis this is the unit response, this is the unit step the  $u(t)$  and what happens is if you look at the response of the RC circuit it starts from 0 its 1 minus e raised to minus t over RC. So, at t equal to 0 this is 1 minus 1 that is 0 at t equal to infinity this is e raised to minus t over RC at t equal to infinity e raised to minus t or RC 0. So, 1 minus e raised to minus t over RC is 1.

So, it starts from 0 and at t equal to infinity approaches one and ok. So, this is basically your 1 minus e raised to minus t over RC into  $u(t)$  ok. So, and this is known as the time constant this RC is known as the time constant larger the time constant implies slower the rise ok.

If the time constant is larger it means the rise is more sluggish ok. So, all these things I think are fairly large time constant and so, large time constant implies slow rise small time constant. So, very small time constant implies fast rise. So, for a large time constant it implies very slow rise ok. So, the rise is very sluggish alright and alright.

So, the time constant is and now what we want to find is we want to find the rise time.

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And find its relation to the 2 dB frequency. So, what we want to do is in and we will do this in the next module find rise time. So, we need to do two things find the rise time 2; relation to the 3 dB frequency where  $F_{3dB}$ ; this is the find its relation to basically the 3 dB frequency.

So, we want to find the rise time and find its relation to the 3 dB frequency of the circuit alright. So, we will stop this module here and look at the other look at other aspects in the subsequent modules.

Thank you very much.