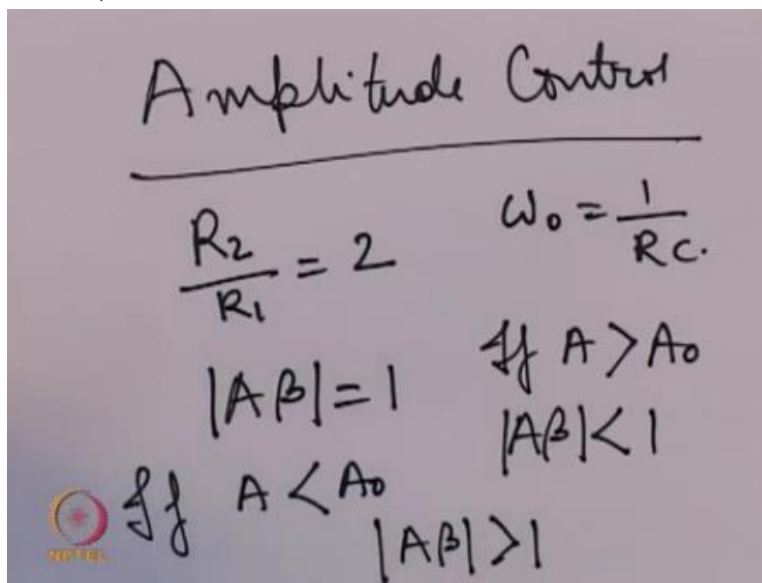


Analog Circuits
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Week 07
Module 02
Oscillator Amplitude Control, Quadrature Oscillator

Hello, welcome to another module of this course analog circuits, so in the past module we had talked about you know the oscillatory circuit design using opamps and one of the oscillator topologies that we had discussed was the Wien bridge oscillator, but we did not discuss about amplitude control we had obtained certain conditions that satisfy the Barkhausen criteria but then those conditions are just the conditions that need to be satisfied for successful oscillation they do not specify what the final amplitude will be.

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The image shows handwritten notes on a slide titled "Amplitude Control". The notes are as follows:

$$\frac{R_2}{R_1} = 2 \quad \omega_0 = \frac{1}{RC}$$
$$|A\beta| = 1$$

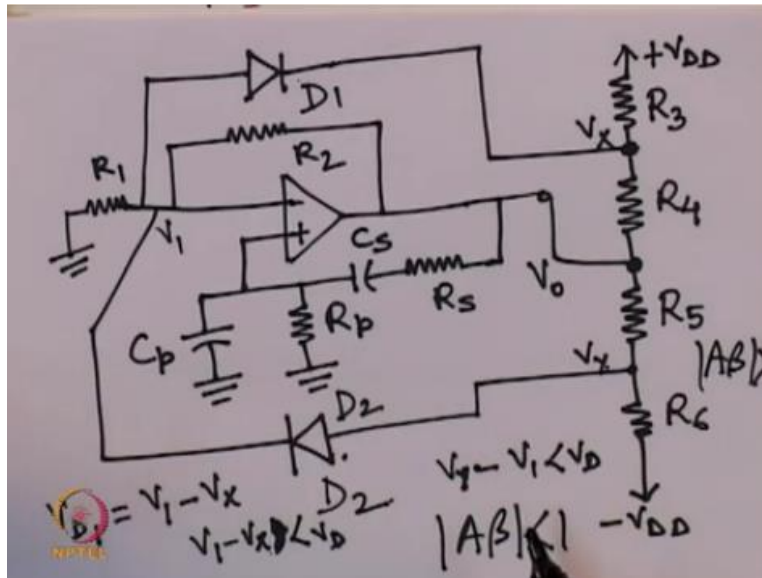
Below the main equations, there are two sets of conditions:

- For $A > A_0$, $|A\beta| < 1$
- For $A < A_0$, $|A\beta| > 1$

So in this module we will be discussing techniques to control the amplitude of that same oscillator, so in the last module amplitude control so for the Wien bridge oscillator we had seen that R_2 upon R_1 should be = 2 and the frequency of oscillation was given by RC if this condition in these 2 conditions are satisfied then the frequency of oscillation is determined but not the amplitude so for amplitude control we call that we needed to have 2 conditions that is at the point of oscillation $A\beta$ should be = 1.

However if A is greater than A0 the steady state amplitude then A beta should be lesser than 1 similarly if A is lesser than the steady state amplitude then A beta has to be greater than 1 so these how to achieve this so let us go back to our Wien bridge oscillator once again.

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This was our Wien bridge oscillator, now to this we if we add the limiter circuit which we had discussed a few module back then the circuit that we get is something like this so that limiter had 4 resistances on this end the supply voltage was - VDD on this end the supply voltage was + VDD so this is my V0 output amplitude comes stabbed from here this is diode D2 this is diode D1.

Now for you know for amplitude control we have already discussed the following conditions right that if A is greater than A0 the steady state amplitude then A beta should be lesser than 1 if A is lesser than A0 then A beta should be greater than 1 that is if the amplitude is lesser than the steady state amplitude or the desired amplitude then the feedback should be positive in or should be such that the amplitude is that a little instability is created and the output kind of goes a little higher similarly here also when the amplitude exceeds the desired value a similar instability is needed to be created.

So that amplitude comes back to its steady state value now how does this work (Refer Slide Time: 05:42), so in this circuit as we have seen that this voltage see that diode the voltage across diode D1 if I label this voltage as say V_1 then V_{D1} is = $V_1 -$ say I call is V_x and this I call V_y ,

V_x as long as V_x is greater than V_1 or $V_1 - V_x$ is greater or I should say is lesser than V_D as long as $V_1 - V_x$ is lesser than V_D this diode will be cut off similarly as long as $V_1 -$ or $V_y - V_1$ is lesser than V_D this diode D_2 will also be cut off.

Now suppose the voltage at V_0 exceeds the steady state value then these R_3, R_4, R_5, R_6 are so adjusted that when V_0 exceeds that value V_y will also exceed $V_y - V_1$ will now be greater than V_D and that will cause this D_2 to conduct once D_2 starts conducting let me write it nicely this is D_2 once D_2 starts conducting R_5 will come in shunt with R_2 and so the net opamp gain will reduce because of this shunt combination because in the feedback path we now have a shunt combination of R_5 and R_2 similarly when say V_0 becomes lesser than certain value ok.

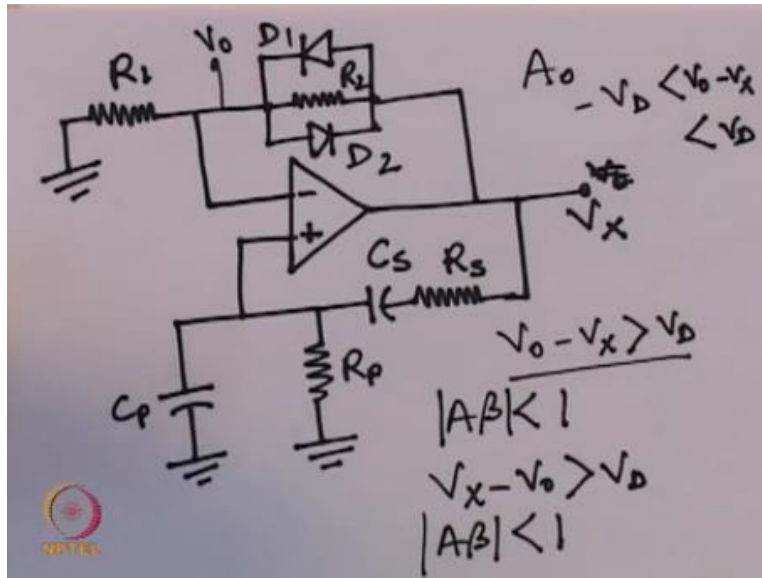
So this happens when V_0 exceeds in the positive sense that is when V_0 amplitude is more positive than the desired amplitude well on the other hand say V_0 amplitude is more negative than the desired value that is on the negative half cycle it becomes its magnitude is much higher then what happens V_x goes down when V_x goes down there is a particular point when V_{D1} given by $V_1 - V_x$.

Now becomes greater than V_D and therefore D_1 starts conducting once D_1 starts conducting an effect similar to that D_2 started conducting happens that is R_4 will be now in shunt with R_2 and because of the shunt combination of R_2 and R_4 that total gain of this opamp will reduce so that is how it happens okay so once when the amplitude exceeds the desired value 1 of R_4 or R_6 will come in shunt with R_2 and cause decrease in the gain that way we ensure that the condition of A beta lesser than 1 is satisfied.

What happens when V_0 for some reason becomes very low when V_0 becomes very low R_2 and R_1 are so adjusted that actually A beta is always greater than 1 for when D_1 and D_2 both are not conducting then this combination R_1 and R_2 provides again such that A beta is greater than 1, so A beta greater than 1 means that when D_1 or D_2 are not conducting the tendency of this circuit will always be to keep the amplitude going higher.

However the moment the amplitude crosses the desired limit one of V_A either V_x will become more negative or V_y will become more positive cause 1 of D_1 or D_2 to conduct and thereby bringing down the amplitude early so as a result of which the amplitude at this point remains at the desired value A_0 so this is at a dynamic balance we can have an alternate implementation of this circuit as well.

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Consider this circuit, this is V_x and this circuit see this if we ignore this D_1 and D_2 then the circuit is exactly like the Wien bridge oscillator that we have discussed earlier the purpose of keeping these 2 diodes D_1 and D_2 is to provide a control on this output voltage V_0 now how this output voltage works is like this so when say D_1 and D_2 both are not conducting then of course it will be a normal oscillator with a and suppose R_1 and R_2 are so adjusted that when D_1 and D_2 are not conducting the output is A_0 .

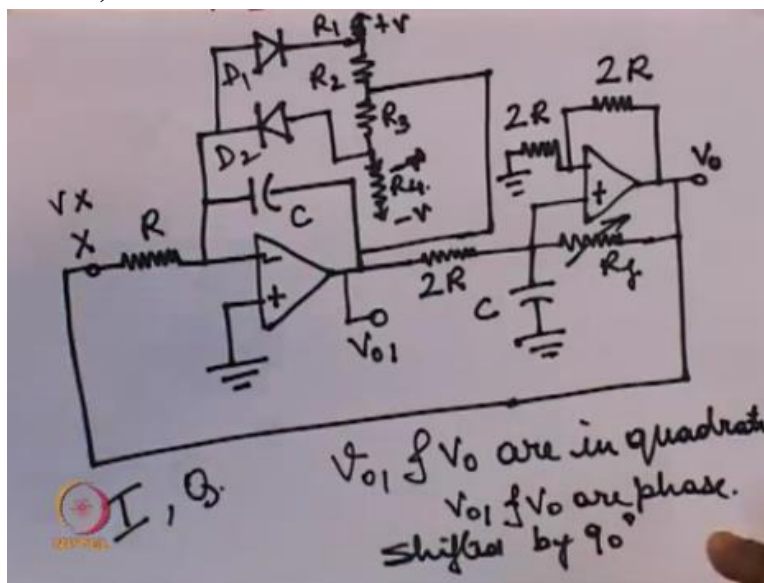
Now say for some reason V_0 goes high it goes high such that $V_0 - V_x$ is greater than V_D the threshold voltage of diode D_2 when this happens D_2 starts conducting once D_2 starts conducting so this resistance R_2 will be shorted by this diode D_2 so once this resistance R_2 is shorten the gain in the feedback loop provided by the feedback loop will be 0 and therefore $A\beta$ will become lesser than 0 and so V_0 will again fall back.

If on the other hand V_0 falls very low such that $V_x - V_0$ is greater than V_D then diode D_1 will start conducting and again a similar event will happen or I should say you know if suppose V_0

becomes more negative than such that $V_x - V_0$ is greater than V_D then also we will have A beta lesser than 1 when V_0 is between these 2.

So when $-V_D$ when $V_0 - V_x$ is within this range then however our circuit will oscillate our diodes D_1 and D_2 will not conduct and our amplitude will be maintained at the desired value so this is also another method to control the amplitude okay so now we have obtained you know the solutions for oscillator for 2 different ways to control the amplitude of the oscillator let us now move to another type of oscillator which know as the Quadrature oscillator.

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The circuit for this Quadrature oscillator is like this, let me use a fresh page so you know the reason it is called a Quadrature oscillator is because V_{01} there are 2 outputs here one is this V_{01} and the other is V_0 so in Quadrature means V_{01} and V_0 are phase shifted by 90 degrees in many applications such oscillator come in handy for example in communication you need to generate a I & Q signal which have to be phase shifted by 90 degree so this is an example of that there are of course many other topologies using MOSFET's, BJT's but using opamps this is one of the topologies for this Quadrature oscillator.

Now here note that this combination that you see here is just an amplitude control mechanism like the one circuit that we discussed previously so overall actually if you see then your V_{01} if suppose our output amplitude is kept within control then my V_{01} will simply be $= -$ upon RCS times V_x .

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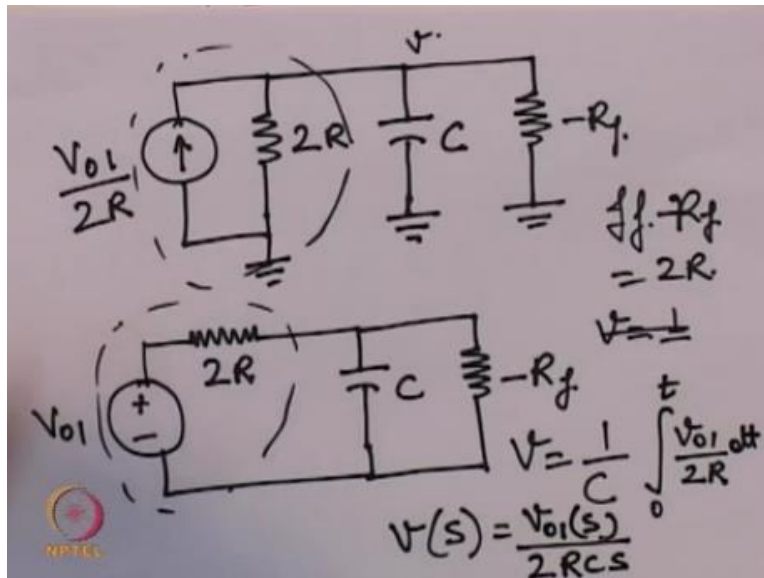
$$V_{01} = -\frac{1}{RCS} V_x$$
$$V_0 = \left(1 + \frac{2R}{2R}\right) V$$
$$= 2V$$

So on that and also so this is the relationship between V_{01} and V_x and what is the relationship between V_0 and V V_0 and V_{01} so to understand the relationship between V_0 and V_{01} or say in order to understand the relationship between V_0 and V_{01} let us label the voltage at this point as V so then your V_0 will be $= V$ times $1 + 2R$ upon $2R$ times V and this is written V twice and this is simply $= 2V$.

So V_0 is $= 2$ times V always so then the current that is flowing through this R_F see the voltage here is V and the voltage here is $2V$ this voltage is at a higher value provided of course V is positive so we can say that current is flowing through R_F in this direction and the value of the current that is flowing is $2V - V$ upon R_F which is $= V$ upon R_F .

So what is happening actually is that even though voltage from V_{01} is appearing at V but current through R_F is flowing in this direction, so we can say that this R_F act as a negative resistance isn't it, you usually current from V if I increase V by increasing V_{01} then current should flow in this direction but instead what I find is a current the current through R_F is $-$ of V upon R_F if I consider current flowing in this direction so then my equivalent circuit for just this part can be written something like this.

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I have a current source V_{01} upon $2R$ with a resistance $2R$ like this followed by a capacitance C and a negative resistance R_f just to clarify how we are getting this circuit see this is a voltage source okay V_{01} with a $2R$ resistance in series, so I might as well have written this circuit like this structure that we this circuit that we obtained is the Norton equivalent of this structure that is it otherwise the rest of the thing just follow.

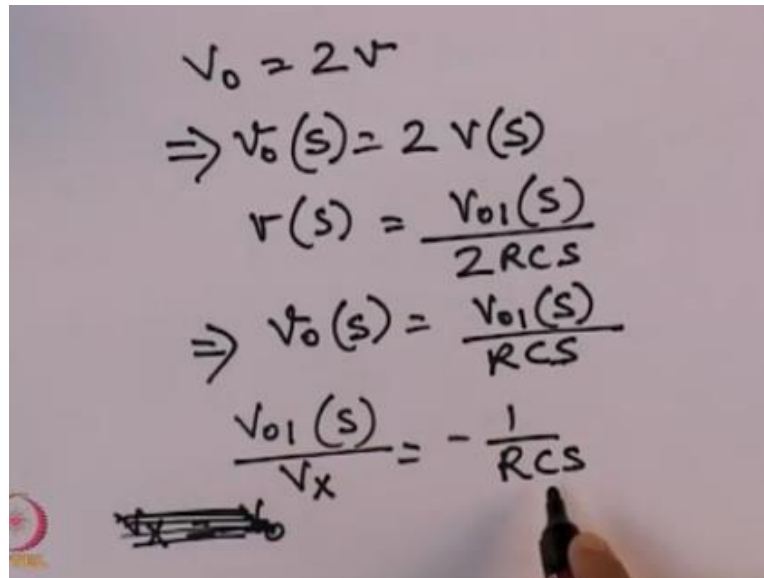
There is a C following this V_0 and $2R$ combination and this R_f which actually acts as a negative resistance having value $-R_f$ with the other end grounded okay now if this R_f is $= 2R$ so see we have obtained this as the equivalent circuit if $-R_f$ is $= 2R$ then what will happen so then this resistance that appears across this capacitance vanishes and so that is the condition of oscillation.

So this R_f if we can make it oscillatory that is the resistance the shunt resistance across the capacitance becomes vanishes then the system will oscillate isn't it then there are no losses happening and any signal that is present across any sinusoidal signal that is present across the capacitance will continue oscillate the rest of the thing that we need to provide is the Quadrature nature of the oscillator.

So for that we find that this V the voltage across this capacitance is given by V and this V is nothing but the voltage drop across this capacitance due to this current source we do not take into account this $2R$ or $-R_f$ because they have already been neutralized so or what is the voltage drop across the capacitor that is given by let me write it here $V = \frac{1}{C} \int_0^t \frac{V_{01}}{2R} dt$ the current V_{01} on

2R dt so in Laplace domain V of S will be given by V01 of S upon 2RCS so we have now obtained a relationship between V and V01.

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The image shows a whiteboard with handwritten mathematical equations. The equations are:

$$V_o = 2V$$
$$\Rightarrow V_o(s) = 2V(s)$$
$$V(s) = \frac{V_{o1}(s)}{2RCS}$$
$$\Rightarrow V_o(s) = \frac{V_{o1}(s)}{RCS}$$
$$\frac{V_{o1}(s)}{V_x} = -\frac{1}{RCS}$$

There is a small scribble at the bottom left of the whiteboard, possibly a crossed-out equation or a drawing.

We know what is the relationship between V and Vo, we saw that Vo is = twice of V so this implies in the Laplace domain V0s is = twice of VS and since VS we just saw is = V01 of S upon 2RCS therefore this implies V0S is = V01 of S upon RCS, now what is remaining is the relationship between V01 and Vx that is so we have found a relationship between this voltage and this voltage what was the relationship between this voltage and this voltage that I had mentioned that this is just a voltage control mechanism so V01S upon Vx is nothing but 1 upon RCS and note that Vx is we have V01 upon Vx given like this okay.

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$$\begin{aligned}
 V_o(s) &= 2V(s) \\
 V_o(s) &= 2 \times \frac{V_{o1}(s)}{2RCs} \\
 &= \frac{V_{o1}(s)}{RCs} \quad \text{--- (1)} \\
 \frac{V_{o1}(s)}{V_x(s)} &= -\frac{1}{RCs} \quad \text{--- (2)} \\
 \frac{V_o(s)}{V_x(s)} &= -\frac{1}{R^2C^2s^2} = 1 \quad s = j\omega_0
 \end{aligned}$$

V_s is given in terms of V_{O1} of S like this therefore so the relationship between V_o and V we already know is given like this from which we can say that that V of o S is = twice into V_{O1} of S upon $2RCs$ which is = V_{O1} of S upon RCs so this is one relationship which we got between V_{O1} and V_{O2} now coming to the other relationship that is between V_{O1} and V_x so we see that the relationship between V_{O1} and V_x is nothing but that of an integrator because this diode circuit base circuit is just for voltage control.

So V_{O1} of S upon V of x S is = - 1 upon RCs so then from these 2 equations from equation 1 and equation 2 we can write V_O of S upon V_x of S is = - 1 upon $R^2C^2S^2$ of S now for oscillation as you see for satisfying the Barkhouse criteria V_O should be = V_x so this should be = 1 so then from there we can see that if this relationship has to be satisfied then by substituting $S = j\omega_0$ where ω_0 is the frequency of oscillation we get.

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$$\frac{-1}{RCs^2} = 1$$

$$s = j\omega_0$$

$$\Rightarrow \frac{1}{RC\omega_0^2} = 1$$

$$\Rightarrow \omega_0 = \frac{1}{RC}$$

$$\frac{V_o(s)}{V_{o1}(s)} = \frac{1}{RCs} \quad \text{Substituting } s = j\omega$$

$$\Rightarrow \frac{V_o(s)}{V_{o1}(s)} = \frac{1}{RCj\omega}$$

So starting from -1 upon $RCs^2 = 1$ substituting $s = j\omega_0$ this implies 1 upon $RC\omega_0^2 = 1$ which implies $\omega_0 = \frac{1}{RC}$ so the frequency of oscillation of this oscillator is given by $\omega_0 = \frac{1}{RC}$.

Now did we establish the condition of Quadrature that V_{o1} and V_o are indeed in quadrature? Yes, how did we do that because V_{o1} we call this relationship that we just rewrite V_o upon V_{o1} of s is given by $\frac{1}{RCs}$ substituting $s = j\omega$ this implies V_o upon V_{o1} of s is $\frac{1}{RCj\omega}$.

So this relation clearly shows that the phase difference between V_o and V_{o1} is indeed 90 degree as seen by this j the imaginary quantity j which is = the square root of -1 because of the presence of this j in the denominator the phase shift will indeed be 90 degree and we have already established the way the amplitude control takes place by this diode circuit.

If say for some reason the voltage V_{o1} exceeds the stable value then the diode D_2 will start conducting and this capacitor will be shorted if on the other hand V_{o1} is much lower or becomes more negative than the desired value then this diode D_1 will start conducting and so the feedback part will be short circuited and once the feedback circuit is short circuited the this amplifies with lose its gain.

So I hope it was clear, so in this module you know we discussed a 2 different oscillator topologies the first one we had already started in the previous module in this module will be discussed about the amplitude control mechanism and then we saw for the same Wien bridge oscillator another way of controlling the amplitude and finally we saw a Quadrature oscillator were not just 1 output was produced but 2 outputs were produced and these 2 outputs were phase shifted by 90 degree or in Quadrature, thank you very much.