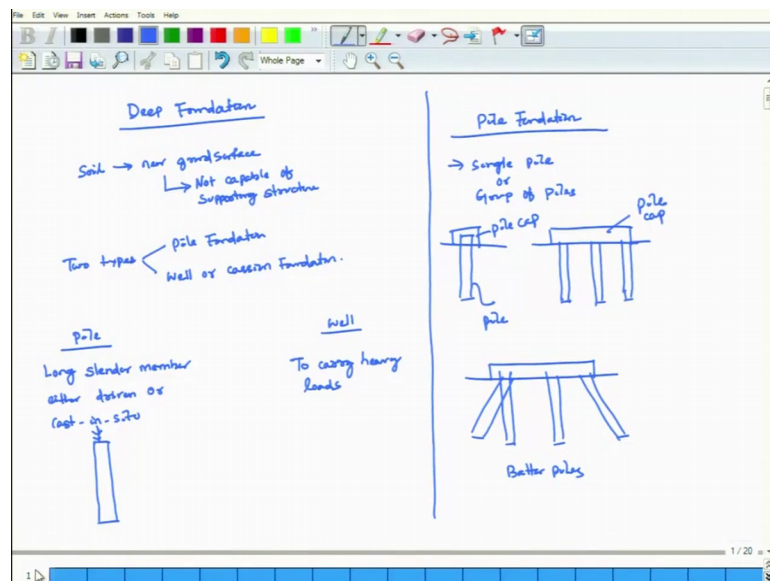


Foundation Design
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Lecture - 18C
Deep Foundation- Part 2

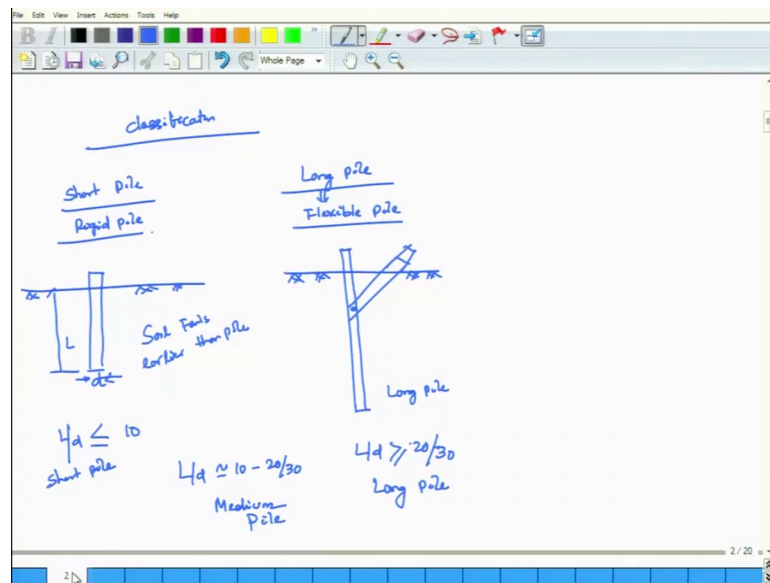
Last class I have started deep foundations, with this 2 types of deep foundation.

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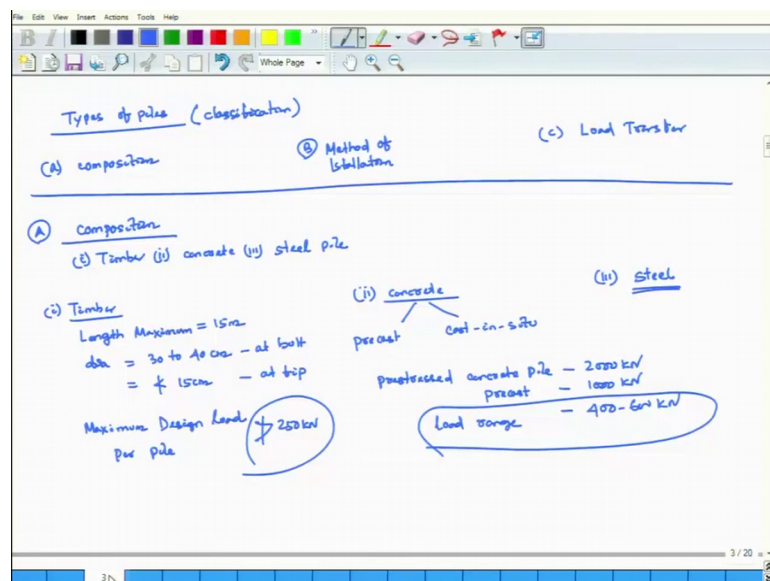
One is pile and well foundations. And pile foundation I discussed. It may be provided single group of pile or batter pile.

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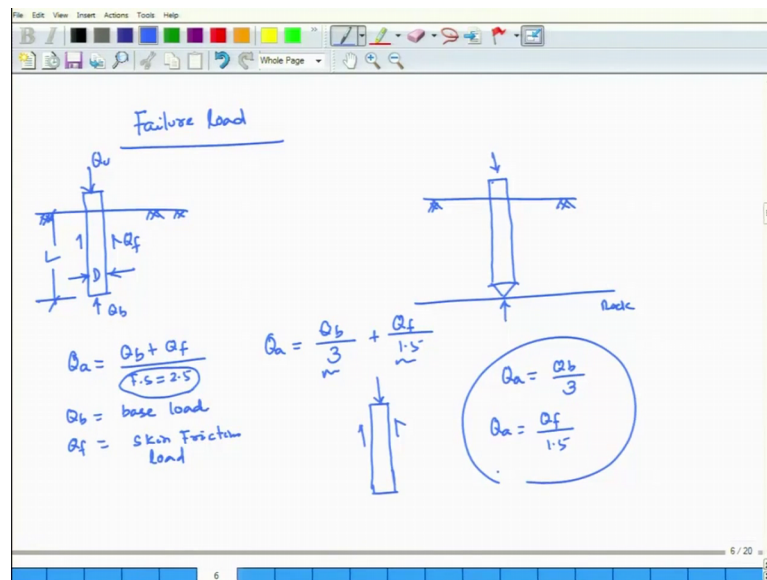
Then classification of piles also I have explained short, rigid, long, flexible.

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Then also is started I have finished types of piles, classification based on composition, method of installation and low transfer. Then let us start with this now Failure load.

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In failure load let us start with this. This is your Q_u . This is your embedded length, and this is your diameter D . And one is your point bearing, other is your sub friction.

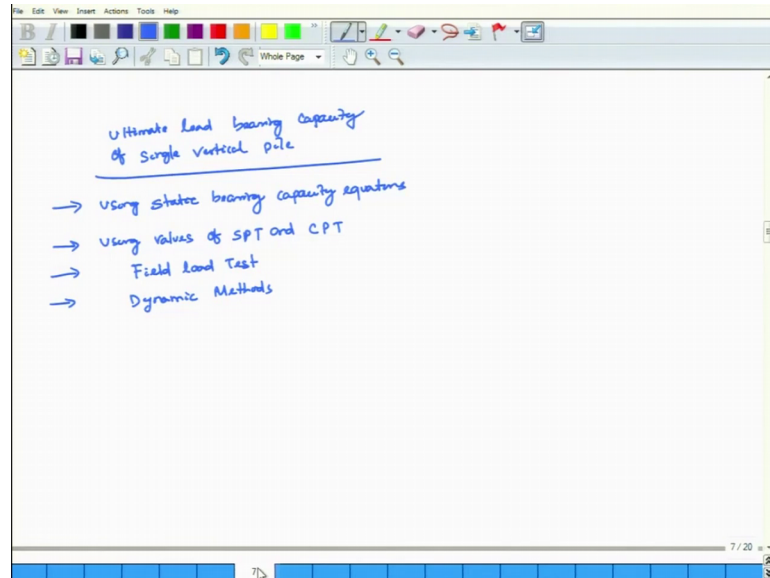
So, if I write it failure load Q_a , Q allowable, Q_a is equal to Q_b plus Q_f by factor of safety for pile foundation generally it is provided 2.5. So, Q_b is your base load and Q_f is your skin in friction, skin friction load. So, in case of the values of Q_b and Q_f can be Q allowable used. So, if I go by independently if I go by independently, you can write it Q_a is equal to Q_b by a factor of safety generally 3 plus Q_f by is your factor of safety generally 1.5. If you are going by this is a pile, in this pile we are considered both end bearing as well as frictions.

If only it is end bearing pile. For example, let us say this is the case as I have explained earlier, there is a load coming here. And here it is here it is So, Q_a is equal to Q_b by 3 and Q_f by 1.5. So, these are the 2 factor of safety independently if you are taking both friction as well as end bearing pile then in that case total factor of safety will be 2.5. Now in this case in this case if there is a case here than in this case there is a rock layer, what will happen? Load will be transferred by means of end bearing. Once it will be end bearing then in that case Q_a will be Q_b by factor of safety of 3. Now other case other case where load has been transferred by means of frictional resistance.

In this case Q_a is equal to frictional resistance by 1.5. So, that is why this is your allowable load. So now, method of finding out what are the different methods to find it

out ultimate load bearing capacity of a single vertical pile; ultimate load bearing capacity of single vertical pile.

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So, there are different ways. So, there are different methods, first one is your using static bearing capacity equations particularly bearing capacity equations, using static bearing capacity equations. Then use of values of or using values of SPT standard penetration test, and CPT. Cone penetration test, then by means of field load tests, and by means of your dynamic methods. What I have discussed earlier if this is allowable load, theoretically you have to find it out what is the end bearing capacity, what is the friction capacity.

So, to get that ultimate load bearing capacity of single vertical pile, first one is your using static bearing capacity equations using values of SPT and CPT. SPT is your standard penetration test and CPT is your cone penetration test. And third is your field load test fourth is your dynamic methods. Now let us consider first let me start with this using bearing capacity equations, bearing capacity questions first one.

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Bearing Capacity Equations

C-φ Soil

$$Q_b = [C N_c + q_0 N_q + 0.5 \gamma D N_\gamma] A_b$$

Ineffective and neglected for deep foundation.

N_c, N_q, N_γ = bearing capacity factors
 L = depth of embedment
 A_b = sectional area of pile at base level
 $q_0 = \gamma L$

For granular soil

$$Q_f = A_s f_s$$

↑
 shaft resistance
 A_s = shaft area
 f_s = unit shaft resistance.

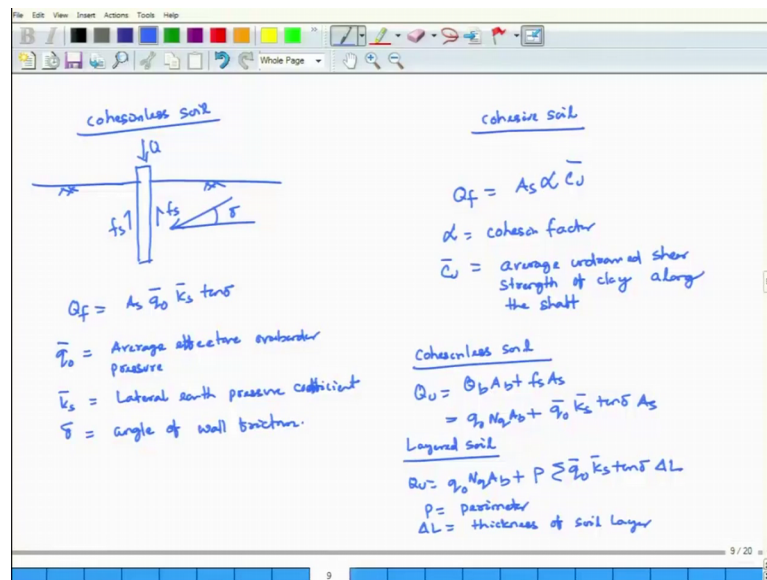
By using your bearing capacity equations; so for c phi soil, for c phi soil Q_b , because if this is my pile, this is your load this will be your frictional resistance Q_f and this is your Q_b base resistance.

So, Q_b if I write it there is again bearing capacity equations, it will be $c N_c$ plus $Q_0 N_q$ plus $0.5 \gamma D$ into $n \gamma$; γD into $n \gamma$ D is your capital D is your diameter of ϕ capital D is your diameter of ϕ , into because this is a capital Q , then area of your base area of your base. So, this generally has been neglected for deep foundations, it is ineffective and neglected for deep foundation, neglected for deep foundation.

So, $N_c N_q$ and $n \gamma N_c N_q$ and $n \gamma$ are bearing capacity bearing capacity factors. And if I write it, this is my L is your embedded length L is your embedded length or depth of embedment. A_b is your sectional area of ϕ at base level base level. And Q_0 is equal to Q_0 is equal to γ into L γ into L . γ is equal to effective unit weight of the soil. So, let me start with this for this Q_f for granular soil, for granular soil Q_f is equal to A_s into f_s . So, Q_f is your shaft resistance A_s is your shaft area f_s is your unit shaft resistance.

So, for cohesion less soil I am going to next page.

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For cohesion less soil, for cohesion less soil if I write it, let is take it a pile here. Then this is your f_s , this is your Q , which will be acted upon by this is your δ . If I write if I write Q_f Q_f is equal to $A_s Q_0 \text{ prime } K_s \text{ prime } \tan \delta$. So, in this case in this case $K_s \text{ prime } Q_0 \text{ prime}$ is your effective overburden. So, this will be your Q_0 this is your f_s and this is your δ . And K_s is your lateral earth pressure coefficient let me write it, $Q_0 \text{ prime}$ means average effective overburden pressure.

Average effective overburden pressure K_s is your lateral earth pressure coefficient, lateral earth pressure coefficient. Then δ is your angle of wall friction, similarly for cohesive soil, for cohesive soil cohesive soil Q_f is equal to Q_f is equal to $A_s \alpha C_u$. α is equal to this is your cohesion factor, and C_u is your C_u is your average undrained shear strength of clay, average undrained shear strength of clay along the shaft along the shaft.

So, let me write it let me write it for cohesion less soil all total how it is coming. So, total ultimate bearing capacity of single pile is your Q_b into A_b plus f_s into A_s which is equal to $Q_0 N_q A_b$ plus $Q_0 \text{ prime } K_s \text{ prime } \tan \delta A_s$. For layer soil what will happen for layer soil cohesion less soil, layer soil Q_u is equal to $Q_0 N_q A_b$ plus p is equal to perimeter summation of $Q_0 \text{ prime } K_s \text{ prime } \tan \delta$ into ΔL . So, p is equal to perimeter, ΔL is equal to ΔL is equal to thickness of soil layer.

So, all total if I start with this for particularly first one, this is your using static bearing capacity equation, then for see if I soil if I am considering your terzaghi is bearing capacity that is your $c N_c + q_0$ and q_0 plus $0.5 \gamma D_n$ gamma into A_b . So, that is your resistance of the base for deep foundations, deep foundations $0.5 \gamma D$ and gamma has been neglected to 0. A_b is your sectional area of pile at base level, q_0 is equal to γL , L is equal to depth of amendment. For granular soil q_f is equal to A_s into f_s .

Now, for base resist for cohesion less soil frictional resistance is your $A_s q_0' K_s \tan \delta$. q_0' is your average effective over burden pressure along the shaft length. K_s is your lateral earth pressure coefficient. δ is your angle of wall friction. For cohesive soil q_f is equal to $A_s \alpha C_u$. α is equal to cohesion factor. C_u is equal to average undrained shear strength of clay along this shaft. Now if I am writing altogether cohesion less soils.

So, Q_u is equal to $Q_b A_b + q_f A_s$. So, $Q_b A_b$ is equal to $Q_b A_b + f_s$, says if I write it $q_0' N_q$ into A_b plus $q_0' K_s \tan \delta$ into A_s for layer soil layer soil the $q_0' N_q A_b$ this is your base resistance. This will be fixed for particular layer for other part of this shaft. It is a summation of $q_0' K_s \tan \delta$ into ΔL ΔL is your thickness of yourself soil layer into is your perimeter.

So, next part is your how do I calculate, how do I calculate base resistance and what are the different factors affecting, I think I will I will stop it here. So, next class I will do other part.